

A GIS-BASED LID FRAMEWORK FOR
SUSTAINABLE URBAN RUNOFF
MANAGEMENT

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ABSTRACT

Low Impact Development (LID) is one of the most popular sustainable techniques for runoff reduction in urban areas. LID mimics nature by retaining or detaining the runoff at the source. Examples of LID include bioretention cells, green roofs, and porous pavements. While the primary purpose of LID is runoff reduction, several lateral benefits (environmental and socioeconomic) are accrued from LID.

Even though many studies have shown the effectiveness of LID on runoff reduction, investigation around many other aspects of LID has remained limited. Out of all these aspects, there is a significant lack of a systematic decision-making model to rank LID solutions (suggest where to implement LID and what type of LID to use) to maximize the LID benefits. The objective of this dissertation is to develop an innovative simplified geospatial model (referred to as LID-Solution Evaluation and Ranking Approach (SERAH)) to rank the LID solutions. SERAH develops a Hydrological-Hydraulic Index (HHI) and integrates it into a Multi Criteria Decision Making (MCDM) model considering the key criteria contributing to the ranking LID solutions.

In this research, the application and effectiveness of SERAH and its corresponding indices were examined under various case scenarios and case studies (e.g., City of Toronto as the study site). Also, SERAH was validated against physical models such as HEC-HMS and PCSWMM. Further, the HHI was used for modelling climate change and urbanization scenarios for three Canadian metropolitans (Toronto, Montreal, and Vancouver).

The results of this study show that, unlike the traditional methods which use stormwater modeling for ranking LID solutions, SERAH effectively ranks LID solutions

using geospatial analysis. SERAH and its corresponding indices are universally applicable since they have been deductively developed and like many similar methods are not induced and custom-built around a sample dataset. The results of this research lend themselves to the strategic planning of multifunctional sustainable infrastructures (LID); give a holistic insight about current and future demands for LID; integrate multiple disciplines (socioeconomic, environmental, geography, and hydrology) to find comprehensive sustainable solutions; and suggest a future need for similar multidisciplinary research by highlighting the gaps and limitations.

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ABBREVIATIONS

DEM	Digital Elevation Model
Dr	Depth to restrictive layer
Dg	Depth to groundwater
ENI	Environmental Index
GI	Green Infrastructure
GIS	Geographical Information System
HEC-HMS	Hydrologic Engineering Center- Hydrologic Modelling System
HHI	Hydrologic-Hydraulic Index
HHCI	Hydrologic-Hydraulic Cost Index
HSE	Hydrological-hydraulic Socioeconomic Environmental
IT	Infiltration Trench
K_s	Saturated hydraulic conductivity
LID	Low Impact Development
LIDDI	LID Demand Index
MADM	Multi Attribute Decision Making
MADA	Multi Attribute Decision Analysis
MCDM	Multi Criteria Decision Making
MCDA	Multi Criteria Decision Analysis
MODM	Multi Objective Decision Making
MODA	Multi Objective Decision Analysis
n	Soil porosity
PP	Porous Pavement
R	Rainfall intensity
RG	Rain Garden
S	Slope
SAW	Simple Additive Weighting
SERAH	LID-Solution Evaluation and Ranking Approach

SCN	Stormwater Collection Network
SEI	Socio Economic Index
PCSWMM	Personal Computer Stormwater Management Model
t_c	Time of concentration
TSS	Total Suspended Solid
TRCA	Toronto and Region Conservation Authority

CHAPTER 1: INTRODUCTION

1.1. BACKGROUND AND MOTIVATION

Climate change and urbanization are two key drivers increasing the surface runoff and consequently the risk of flood. Urbanization modifies the land terrain and replaces the natural soil and vegetation with impervious surfaces. Both cause a change in the hydrologic behaviour and response of catchments [1]. The extension of the impervious surfaces increases the surface runoff quantity [2]–[5] and deteriorates water quality in receiving water bodies [6], [7]. Urbanization also results in the centralization of assets and population, which aggravates the impact of the flood and causes more severe and costly consequences. It is being more exacerbated due to the historical and projected urban growth trends [8], [9]. In addition, climate change significantly impacts the intensity and frequency of runoff generation and resulting in flood occurrence and is increasing dramatically [9], [10]. As a result, the risk of the future flood (as a leading global concern) is being intensified by climate change and urbanization [9].

Like other natural hazards, floods have detrimental effects on the quality of life causing

casualties, financial losses, and deterioration of the ecological system [9]. During two studied decades (1995-2015), floods have caused the loss of 157,000 lives worldwide (about a quarter of all weather-related disasters). It has affected the life quality of 2.3 billion people (the highest share among weather-related disasters with a percentage of 56 %) [11]. During a studied period (2006 to 2016) the global flood losses were approximately 50 billion USD annually (the highest among natural disasters) [12].

In Canada, in 1948, the Fraser River flood (located in British Columbia) cost about 22 million CAD. Two years later in 1950 again Red River flood had a 25 million CAD cost, four years later in 1954 Hurricane Hazel in Ontario cost 25 million CAD. Since then, these costs have consistently grown. From 1948 to 2021, the Federal Government of Canada has expended about 714 million CAD for flood disaster compensation [13]. These are measurable reported losses resulted from floods whereas there are also significant immeasurable hardships such as mental health support or physical needs [14].

Urban sources of runoff alleviate the flood in the downstream receiving water bodies [15]. Urbanization changes the hydrological behaviour of catchments which is caused by several factors [16]. Some of these factors include removal or reduction of the tree and/or shrub canopy and root systems, developing new impervious surfaces, including streets, driveways, roofs, sidewalks, etc., as well as the direct connection of these surfaces to the stormwater systems [16]. Many studies have been focused on investigating the effect of urbanization on increasing the amount of surface runoff (e.g., [2]–[4], [17]) and exploring methods for its mitigation [5] (e.g., [18] [19] [20]).

An innovative solution for reducing the effect of urban surface runoff on the flood is a smart and sustainable urban development approach commonly known as Low Impact Development (LID) [21]–[23]. LID is also known with other terms such as SUDS (Sustainable

Urban Drainage Systems) [24], which is mostly used in the U.K.; WSUD (Water Sensitive Urban Design) [23], which began to be used in the 1990s in Australia [25], and sometimes Green Infrastructure (GI). Among mentioned terms, “LID” is used in this research as it is more common across the world, particularly in North America.

LID is one of the most popular solutions for urban runoff reduction [25]. LID utilizes hydrological approaches to mitigate the surface urban runoff. These approaches include increasing infiltration, maintaining t_c (time of concentration: the time needed for stormwater to flow from the furthest point in a catchment to the hydrological outlet [26]), retention (holding water with no surface release), detention (holding water with slower surface release) [27]. To practice LID, there are two main types of measures, conservation and construction [27]. The conservation measures aim for minimizing urbanization impacts to the extent practicable by conserving natural resources and ecosystems, reducing imperviousness, maintaining natural drainage courses, reducing the use of pipes, minimizing clearing and grading [28]. Construction measures follow the LID goals with the use of engineered structures [28]. Urban infrastructure such as porous pavements, green roofs, rain barrels, and bioretention cells [28] are some examples of these structures.

In addition to the runoff reduction benefit of LID [29], there are several lateral benefits associated with using some types of LID [30]. These lateral benefits include environmental [29], [31], [32] and socioeconomic [33], [34] benefits. Examples of environmental benefits are preserving the natural hydrological cycle [30] particularly recharging groundwaters [35], reduction in energy demands [36], [37], improving microclimates [38], mitigating urban heat island [39], [40], use of environmental friendly material [41], improved water quality [29], [31], [36], [42]–[46], decreased air pollution [32], [47]–[52] and enhanced biodiversity [32], [53]–[59]. Examples of socioeconomic benefits include access to amenities such as green spaces, easing the imbalance

between water supply and demand [30], [41], enhancing health [60]–[62], provisioning services [63], and improving educational results [64]. The types of LID which introduce the most lateral benefits are generally known as Green Infrastructure (GI). Examples of GI include bioretention cells, green roofs, and tree canopy [28], [65].

LID also assists the stormwater collection networks (SCN). SCNs are the conventional approach for managing surface runoff in urban areas. Runoff flows from surfaces into the SCN through inlets and pipelines. SCN rapidly transfers it to lower elevation areas (downstream) to a point of discharge which is typically natural water bodies (e.g., rivers, lakes, or ponds) [66]. SCNs are well-known and well-documented [67] but their evident problems have necessitated a demand for more novel approaches for urban flood management. SCNs are designed for a level of performance and have a maximum capacity. Thus, in the case of extreme rainfalls, the limited capacity of SCNs fails to manage these events. The severity of this problem is increasing due to climate change, urbanization, and the existing SCN ageing and performing at a lower capacity. The use of SCNs is criticized for providing long-term sustainability [68], and for collecting and transferring to water bodies the polluted runoff from surfaces (e.g., car oils from pavements), as well as sanitary sewage in combined sewers [69].

Despite the considerable benefits presented by LID, the progress toward more sustainable urban development using LID has been gradual [29]. Out of all drawbacks, this gradual progress has been due to the uncertainties associated with the unexplored aspects of LID [70]. Some of the common aspects which have been investigated in recent research include: improving the numerical modelling tools to enhance the physical simulation of LID processes [71]; improving the water quality modelling [46]; increasing the complexity of numerical modelling (e.g., 2D water quantity modelling [72]); cost-benefit analysis [73], [74]; designing geospatial planning systems [75], [76],

and investigating the effectiveness of LID under climate change [77], and decision support systems that facilitate optimal planning of LIDs incorporating modelling and optimization (e.g. SUSTAIN) [78].

LID is a novel concept and the majority of the focus of the literature has gone toward exploring the “hydrological-hydraulic benefit” of LID through the traditional stormwater modelling approach (e.g., [79]). In these approaches, some combinations of “LID types” (e.g., bioretention cell and green roof) at some “LID sites” (wherein LID will be implemented) are selected as scenarios. The scenarios are simulated using a hydrological model and based on the hydrological performance the best scenario is introduced as the priority “LID solution”. In this traditional trial and error process, the decision of selecting the combinations of “site” and “type” of LID is mainly based on the “intuitive criteria” and constraints of guidelines. This decision is not made through a knowledge-based model that systematically incorporates most of the key contributing criteria (e.g., LID cost, benefit, geospatial constraints). Out of all contributing criteria, lateral benefits of LID have been mainly overlooked in the traditional approaches.

The systematic decision making is conducted through Multi-Attribute Decision Models (MCDM). MCDM is the general class of the decision-making models and is further divided into Multi-Attribute Decision Making (MADM) (also known as Multi Attribute Decision Analysis (MADA)) and Multi-Objective Decision Making (MODM) (also known as Multi Objective Decision Analysis (MODA)). MADM copes with discrete problems whereas MODM focus is on continuous or stochastic problems [80], [81]. MCDM models use decision rules to determine the optimal decision. Decision rules are mathematical algorithms that integrate the criteria in a way that reflects the human decision-making process [81]. Some examples for the MODM models are multi-objectives programming algorithms, Heuristic search/evolutionary/genetic algorithms, and

Goal programming/reference point algorithms. Also, examples of these rules for MADM models are weighted sum, Boolean overlay, Ideal/reference point (TOPSIS, MOLA), Analytical Hierarchy Process (AHP), and Outranking methods (ELECTRE, PROMETHEE). Some intuitive or mathematical constraints can be incorporated into these rules to limit some possible decisions [80]. An example is assigning weights to the objectives which first has been suggested by Zionts and Wallenius (1976) [82].

Likewise, GIS-based multicriteria decision models (GIS-MCDM) have become popular for solving many geospatial decision problems [83]. The coupled capability of GIS and MCDM allows for the integration and processing of geographical data to make systematic judgments [81]. According to a survey (duration of the study was 1990-2004) by Malczewski (2006) [81], the number of studies using GIS-MCDM models for environmental studies has one of the largest shares among all fields of science. According to the same study, the most popular GIS-MCDM integration rule is the weighted sum model which was present in about 40% of studies [81]. Following with the Analytical Hierarchy Process (AHP) (GIS-AHP models) [81] as the second popular model. The popularity of these models is mainly due to their simplicity, being easy to understand, and their capability in reflecting human behaviour in the decision-making process [81]. To decrease the complexity of the decision-making model in this research we selected the weighted sum model in the GIS context to develop a simplified geospatial model to rank LID solutions.

There are previous decision-making models that have been developed to address this issue and vary in many different aspects such as their selected contributing criteria (e.g., LID cost, benefit, geospatial constraints) and decision-making models. However, there is still a remarkable gap for a model that integrates the key criteria in a geospatial context. Wu et al. (2020) has

identified such a significant gap for a comprehensive model that ranks LID solutions in a review research [84].

To cope with this, a knowledge-based and systematic model that incorporates multiple geospatial criteria to rank LID solutions (combination of LID type and sites) is required [85]. Such a model needs to account for the key criteria contributing to the rank of LID types and sites to meet the urban runoff management goals. Multi Criteria Decision Making (MCDM) [80] (also known as Multi Criteria Decision Analysis (MCDA) [81]) models are the systematic approach for decision-making where the decision-maker is facing multiple conflicting criteria and objectives [80]. MCDM has gained popularity in real-world decision-making problems where it used to be unknown or perceived as mathematic when it was suggested as a managerial decision-making solution [80].

1.2. RESEARCH OBJECTIVES

Based on the needs and gaps identified in the previous literature, the overall objective of this research has been determined as a GIS-based LID framework for sustainable urban runoff management. This objective was further divided into the following sub-objectives:

1.2.1. Developing a simplified geospatial index for ranking LID sites

The objective is to develop an innovative and simplified geospatial index for ranking “LID sites”. The traditional focus on “sites” usually goes toward identifying “feasible sites” (the locations that are suitable for implementing LID). Whether there is a need or “demand” for LID in a site has been less investigated in the previous research [86]. This “demand” is the need for

“primary (hydrological)” and “lateral benefits (environmental and socioeconomic)” of LID at each site. The high hydrological demand for LID highlights the potential of sites in runoff generation and the demand for LID at the site for runoff reduction, whereas the high environmental and socioeconomic is the demand of site for such benefits of LID (e.g., decreasing air pollution). Thus, the framework quantifies the demand for hydrological-hydraulic, environmental, and socioeconomic benefits of LID at each LID site and ranks the sites on this basis. The goal is to explore and establish a geospatial relationship between the key contributing criteria and the optimal sites for LID using the physics of runoff generation and MCDM models.

To meet this objective the “hydrological-hydraulic demand” needs to be quantified through developing a heuristic relationship between hydrological-hydraulic contributing criteria (e.g., rainfall, terrain slope, etc.) using geospatial analysis and considering the physical principles governing runoff generation phenomenon. High hydrologic-hydraulic demand at a site is associated with a high potential for runoff generation and high demand for capturing that runoff at the site (source control). Note that proposing such a heuristic relationship helps with highlighting the sites with high potential for runoff generation. Also, it facilitates the incorporation of runoff reduction benefits into lateral benefits of LID. The traditional method for quantifying the demand for LID is using the results of Storm Water Models (SWM), with which the flood-prone areas downstream are highlighted and demand for runoff reduction upstream is reported. Which sites upstream reduce the runoff more effectively and are a priority for implementing LID is a question that is answered in this research.

This priority will be also determined based on the demand for the lateral benefit of LID (“environmental demand” and “socioeconomic demand”). This demand will be quantified by identifying the key criteria and using them as an input of an MCDM model in a geospatial context

(GIS-MCDM model). The demand for lateral benefits of LID will be integrated into the demand for the primary benefit (hydrological-hydraulic demand) using a heuristic relationship. Note that the suggested model addresses the gap of an MCDM model that comprehensively establishes a geospatial relationship among the key contributing criteria; quantifies and integrates these key criteria; and ranks the sites for implementing LID. Such a model goes beyond accruing the primary benefit of LID and aims for implementing multifunctional LID that also maximizes lateral benefits simultaneously.

1.2.2. Applying the proposed index under climate change and urbanization

Using the results of the previous research, this objective investigates how the hydrological-hydraulic demand for LID will change under future scenarios. In this objective, 12 scenarios (combinations of future urbanization and climate change) for three cities in Canada (Toronto, Montreal, and Vancouver), 36 scenarios in all, will be developed. It will answer the question that under unplanned and unsustainable urbanization and future climate, how the demand for LID will change. Also, it will suggest the sole contribution of climate change and urbanization on LID demand. In addition, it will investigate how city characteristics (e.g., rainfall intensity or permeability) impact overall LID demand and modify it. Note that the quantification of LID demand (representing runoff generation potential) using GIS-based analysis, and under future scenarios is novel among similar studies. The results of this part of the dissertation will provide us with a comprehensive insight into the effect of climate and urbanization on the demand for LID. The outcome of the proposed index can be used for stormwater management, urban planning, and the sustainable development of cities. Also, this objective highlights the importance of sustainable

development using LID and the future need for such a development.

1.2.3. Developing a simplified geospatial model for ranking LID solutions

This objective is to innovatively rank the LID solutions (combination of LID type and site) based on the site demand and LID benefits (primary and lateral benefit and costs of LID types). The ranking will be through developing a novel simplified geospatial model (referred to as LID-Solution Evaluation and Ranking Approach (SERAH)) and using the results of objectives 1.2.1 and 1.2.2. SERAH will integrate key contributing criteria to comprehensively rank LID types as well as LID sites. Ranking LID types and sites enhance the performance of the stormwater network by introducing high rank and effective LID solutions.

To demonstrate the applicability of SERAH for a real set of data, it will be applied in an actual case study for a catchment in the City of Toronto. The prioritized LID solutions will be used to ameliorate the performance of the SCN in the catchment using a stormwater modelling process.

SERAH ranks the LID solutions through geospatial maximization of runoff reduction (primary benefit) integrated into the lateral LID benefits and minimization of cost. Note that the traditional method for ranking LID solutions is based on conventional stormwater modeling which ranks the LID solutions based on their hydrological or water quality performance. In such traditional methods, the solutions are mainly identified using intuitive judgment rather than relying on a systematic approach that quantifies the key contributing criteria and identifies the LID solution. In this objective, a simplified, systematic GIS-MCDM model will be developed. This model relates the demand for LID at each feasible site to the cost and benefit offered by each type of LID to rank LID types at each feasible site and rank feasible LID sites.

1.3. CONTRIBUTIONS

This dissertation will propose a simplified geospatial model for sustainable urban runoff management. The innovation and novel contributions of this research lie in proposing several innovative physics-based GIS-MCDM indices to rank LID sites and LID types. The proposed model integrates key contributing criteria including LID cost, LID benefits (the primary (hydrological-hydraulic) and lateral (environmental and socioeconomic) benefits), LID demand and feasibility of sites. The effectiveness and application of this ranking will be demonstrated by enhancing the performance of a stormwater network.

The objective of this research will be achieved through proposing novel indices (e.g., physics-based index, MCDM-based indices). The indices will establish heuristic geospatial relationships between the key contributing variables to rank LID solutions. The established relationships for the physics-based indices will be validated against physical models. A wide range of climate and urbanization scenarios as new datasets will be studied to demonstrate the applicability of the proposed indices.

1.4. DISSERTATION OUTLINE

This is a paper-based dissertation. Thus, each chapter includes its introduction, literature review, specific objectives, methods, results, and discussion. *Chapter 2* begins with the development of a simplified geospatial index (LID Demand Index (LIDDI)) generated using a systematic framework for ranking sites for LID. Following with an application of LIDDI for the City of Toronto as a case study, and validation of the hydrological-hydraulic component of the

framework against a stormwater model are presented. *Chapter 3* further uses the hydrological-hydraulic index (HHI) of Chapters 2 to explore the change in demand for LID under current and future urbanization and climate change scenarios. This demand is quantified, explored, and contrasted for three Canadian cities (Toronto, Montreal, and Vancouver). *Chapter 4* uses the framework used in Chapter 2 to suggest a novel simplified geospatial model (referred to as LID-Solution Evaluation and Ranking Approach (SERAH)) to rank the LID solutions (combination of LID type and sites). Using a stormwater model, the applicability of the proposed framework is examined in a catchment within the Don River watershed in the City of Toronto. *Chapter 5* presents information about the input data including the sources and the sensitivity analysis of the input data (parameters and weights). *Chapter 6* summarises the major conclusions from each chapter, discusses the limitation of the developed model, introduces the novel contributions of this dissertation, and recommendations for future research. Following Chapter 6 the *Bibliography* is presented. Then, Appendices include complementary information about the research. Appendices A to C presents the developed codes for Chapters 2 and 4. Following by Appendix D, which includes the proof of the concept tested by generating 100 scenarios for a synthetic catchment. Appendix E presents the code and input data used for the sensitivity analysis of Chapter 5. Lastly Appendix F presents the design parameters of the Chapter 4.

CHAPTER 2: THE LOW IMPACT DEVELOPMENT DEMAND INDEX: A NEW APPROACH TO IDENTIFY LOCATIONS FOR LID

2.1. PREFACE

This Chapter addresses the first sub-objective, which is developing a simplified geospatial index for ranking LID sites (referred to as LID Demand Index (LIDDI)). LIDDI is developed through a systematic framework and applied to the City of Toronto as a case study. The validation of the LIDDI and its sub-indices is discussed and demonstrated in this chapter. Particularly, the hydrological-hydraulic index of LIDDI (referred to as HHI) is compared against a stormwater model and its effectiveness is demonstrated.

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Contributions:

The contributions of authors in the current chapter are as follows, **Sarah Kaykhosravi** has conducted the literature review, performed the data collection and curation, developed the method, used the required software to perform the analysis and modelling, validated and visualized the results, and wrote the original manuscript of this publication. **Karen Abogadil** has contributed to the literature review, writing, reviewing, and editing the original draft. **Usman Khan** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript. **Mojgan A. Jadidi** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript.

2.2. ABSTRACT

The primary goal of Low Impact Development (LID) is to capture urban stormwater runoff; however, multiple indirect benefits (environmental and socioeconomic benefits) also exist (e.g., improvements to human health, and decreased air pollution). Identifying sites with the highest demand or need for LID ensures the maximization of all benefits. This is a spatial decision-making problem that has not been widely addressed in the literature and is the focus of this research. Previous research has focused on finding feasible site for installing LID, whilst only considering insufficient criteria which represent benefits of LID (either neglecting hydrological-

hydraulic benefit or indirect benefits). This research considers the hydrological, environmental and socioeconomic benefits of LID to identify sites with the highest demand for LID. Specifically, a geospatial framework is proposed that uses publicly available data, hydrological-hydraulic principles, and a Simple Additive Weighting (SAW) method within a hierarchical decision-making model. Three indices were developed to determine the LID demand: (1) hydrological and hydraulic index (HHI), (2) socioeconomic index (SEI), and (3) environmental index (ENI). The HHI was developed based on a heuristic model using hydrological-hydraulic principles and validated against the results of a physical model (HEC-HMS). The other two indices were generated using the SAW hierarchical model and then incorporated into the HHI index to generate the LID demand index (LIDDI). The framework was applied to the City of Toronto, yielding results that are validated against historical flooding records.

2.3. INTRODUCTION

Increased urbanization has led to a significant increase of impervious surfaces. This has led to higher levels of stormwater runoff, resulting in higher flood risk, overflowing sewer systems, and damage to existing stormwater infrastructure [87]. This situation is made worse by the impacts of climate change, causing more intense rainfall events and droughts, which threaten urban water security. Social implications suggest that these risks will disproportionately affect more vulnerable populations [88].

Low Impact Development (LID) has become one of the most popular methods for managing stormwater and mitigating floods [25], [89]. Examples of LID include bioretention cells, green roofs, detention tanks, and permeable pavement systems [28], [44], [65], [90]–[92]. From a

water and stormwater management perspective the main purpose of most types of LID is runoff mitigation [21], [25], [29], [57], [93], [94] multiple environmental and socioeconomic benefits of LID also exist [30]. Additional environmental benefits include improved water quality [29], [31], [42]–[45], decreased air pollution [32], [47]–[51], and enhanced biodiversity [32], [53]–[59]. Socioeconomic benefits [33], [34] include provisioning services [63], educational improvements [64], enhanced immune functioning [60]–[62] and aesthetics. Not all types of LID provide all additional benefits. The types which provide these additional benefits are generally known as Green Infrastructure (GI). Examples of GI include bioretention cells, green roofs, and tree canopy [28], [44], [65], [90]–[92]. Whereas other types of LID such as cisterns (or underground tanks) mostly provide hydrological (flood control and rainwater harvesting) benefits. Despite the fact that LID such as cisterns provide less environmental or socioeconomic benefits (compared with GI) and have maintenance issues [95] their high efficiency in runoff management preserves it as one of the LID types [96], [97].

During the strategic planning stage of stormwater or flood management projects, decision-makers select sites for LID under limited financial resources [98]. Since LID benefits are spatially dependent, maximizing these benefits requires careful planning when selecting sites for LID implementation [86], [99]. This can be done through the use of geospatial data such as topography, precipitation, land cover, and multiple physical phenomena (e.g., hydrological and hydraulic processes). Without a systematic geospatial framework, selecting sites that can maximize the benefits of LID (need or demand for LID) becomes difficult. Indeed, in a comprehensive review of spatial allocation of LID, Kuller et al. (2017) [100] determined that the lack of such a geospatial framework is one of the biggest gaps in this field.

2.3.1. Existing Geospatial Decision Models

Determining sites for LID has two sides of suitability: *feasibility*: referred to as LID needs site to be implemented, and *demand*: referred to as a site wherein the needs or demands for benefits of LID is high [86], [100]. In the literature, three types of LID geospatial decision-making models exist. The first prioritizes different hydraulic solution scenarios using stormwater models, which allows for modelling LID [101]. The second conducts geospatial analysis using geographical information systems (GIS). The third combines the use of both stormwater models and GIS.

The first type of decision-making models use stormwater modeling along with a multi-criteria decision analysis (MCDA), or multi-attribute decision-making (MADM) [102]. In these type of models MCDM or MADM are used to rank LID solutions in predetermined locations e.g. [103]–[107]. In these types of studies, the method for determining which LID sites or types are more effective to include are based solely on the results of the stormwater model and are not through geospatial analysis (e.g. Lee et al. (2012) [78] used a stormwater modeling to determine the best GI solution).

Models that conduct geospatial analysis through GIS have mostly focused on determining feasible sites, and outputting maps for each type of LID. The criteria used to determine feasibility are often based on specific technical guidelines (e.g., suitable slope or distance to existing infrastructure), and rarely concentrate on maximizing LID benefits (an example of this type of study is [108]). Another study by Kuller et al. (2019) [86] proposes a decision-making framework to determine the feasibility and demand for LID. For the demand, which is the focus of our research, they selected five criteria which were grouped in three categories, including: provisioning (proximity to water demand), regulating (heat vulnerability, connected impervious

area, floods), and cultural (visibility). However, their selected criteria for determining demand do not account for the hydrological-hydraulic demand for LID nor is this demand integrated with the other benefits (i.e., provisioning, regulating, and cultural) of LID. Thus, there is an opportunity to expand on a previously proposed framework (such as [46] or others highlighted below) to incorporate a physically based approach to capture the impacts of the hydrological-hydraulic demand of LID.

The third type of decision-making model combines both GIS and SWM. Models of this type identify sites based on feasibility and prioritize them according to either a specified decision-making system (MCDA model) or discrete prioritization (MADA model); the former may include geospatial analysis while the latter typically does not. Examples of criteria that have been used include slope, water table, hydrological soil group, and runoff volume [109]. Others also consider stakeholder opinion and technical experts [107]. For example, one study, [110], did consider three classes of benefits of LID (the environmental, economic and social benefits), though these were done independently (i.e., in isolation of each other) rather than using a holistic approach. With these three different classes of decision-making criteria, identical rankings of the sites were obtained [110]. Thus, as concluded by Kuller et al. (2017) [100], although a set of GIS-MCDA tools and frameworks have been developed, none of them are sufficient and comprehensive. In addition, in another review by Lerer et al. (2015) [111], they concluded that there is a lack for a comprehensive model that covers all physical-based aspects (referred to as “How Much models”), human aspects (referred to as “Where and Which” models).

2.3.2. Geospatial Physical-Based Framework

Among previous studies in this field the strategical allocation of LID and prioritizing sites on this basis, particularly through considering hydrological and hydraulic parameters is less frequently addressed. Of those that have addressed it, there remains multiple limitations that have significant environmental and socioeconomic impacts. One recent study by Martin-Mikleá et al. [112] used the concept of hydrologically sensitive areas (HSA) [60]. Since HSA was originally used for pollution transport risk [113], the HSA procedure and the criteria used do not match the physical processes that occur in LID. For example, in their study [112], the slope is considered to have an inverse impact on the priority of a site in terms of need for LID. Meaning that sites with higher slope has lower priority for installing LID (in their study includes rain-barrel, green roof, porous pavement, rain garden, vegetated swale, detention and retention pond, and riparian buffer). This is incorrect from a hydrological perspective. Sites with high slope generate lower time of concentration (t_c). Most LID types (such as grass swales) can be used to increase the t_c (and hence reduce runoff related issues). Though types of LID without out flow do not affect the t_c (e.g., drainage boxes), still capturing the runoff of a high slope site prevents joining a runoff with low t_c to the downstream runoff. Thus, steep sloped sites should have high priority (or high demand) for implementing LID for runoff management. Also, the method proposed by Martin-Mikleá et al. [112] does not consider the geospatial or temporal distribution of rainfall. In hydrological models the importance of spatial and temporal distribution of rainfall is noted by many researchers [114]. There are several studies (such as [115]) that present different methods for accurate modelling of rainfall distribution over watersheds. Thus, including the spatial rainfall distribution over the study area, particularly large-scale ones, is necessary. In addition, the geospatial distribution of land

cover and impervious area were also neglected in the Martin-Miklela et al. study [112] - in urban areas a significant portion of the natural land-cover is modified. This modification of the land-cover is important to be considered if the study area is under the influence of human activities and has experienced land-cover changes. Moreover, Martin-Miklela et al. [112] approach has multiple mathematical limitations. For example, in their study to avoid mathematical errors, sites where the hydraulic conductivity is zero, the calculated index has been reassigned somewhat arbitrarily to -3. This value of -3 is a number that is lower than the highest calculated index in the case study. Therefore, this number is a replacement for the actual calculations and depends on the case study and needs justification for each specific case. Finally, in the Martin-Miklela et al. [112] study, only the hydrological-hydraulic demand or need for LID is considered, whilst the environmental and socioeconomic benefits are largely ignored.

Overall, as demonstrated in previous studies, the strategic planning stage of LID projects significantly lack a comprehensive GIS-MCDA framework to determine where to install LID [100] based on the “demand” or “need” – including hydrological-hydraulic demand, and demand due to other indirect benefits. In previous studies, prioritizing sites based on their potential to generate stormwater runoff is one of the least addressed subjects. In addition, prior studies either overlook integrated hydrological-hydraulic benefit with other indirect benefits of LID (including socioeconomic or environmental status [116], use inadequate type and number of assessment criteria [86] (e.g. either hydrological- hydraulic benefit or indirect benefits of LID are overlooked). Also, many of previous studies are based on a stormwater models model. In these types of studies, the scale of the study area is limited to the stormwater models itself, which limits the extent of the study area. This restriction is due to the complexity (in terms of required input data) of developing SWMs for large-scale regions. Thus, as recommended by other studies such as [29], [111], [117],

[118], more investigation to address the indirect benefits of LID should be integrated into GIS-MCDA models for LID to identify the demand for LID that can include future climate, land-use and socioeconomic scenarios.

Therefore, the objective of our study was to develop a physical-based geospatial decision-making framework to answer the need for the strategical planning of the LID, through identifying the *demand* of sites for LID. This *demand* is comprehensively evaluated in our framework by integrating all main and indirect benefits of LID. In our framework we developed two heuristic geospatial relationships to incorporate all benefits of LID. The first heuristic relationship is based on hydrological- hydraulic principles (building on Martin-Miklela et al. (2015) [112] approach) and uses actual values of data in the overlaying process (data are not rescaled). As it represents the physical processes that occur within LID, we validated its results against a physical-based model. Using this relationship, we generated an index (HHI), which ranks the sites based on their potential in runoff generation. Also, using a GIS-MCDA model we developed two other indices (ENI and SEI) to rank the sites based on their *demand* for indirect benefits of LID. From the stormwater management perspective, we considered the runoff control as the direct benefit of LID. Thus, through an innovative heuristic relationship, the indirect benefits of LID (environmental and socioeconomic) are incorporated into the proposed framework as additive value. Meaning that if HHI is not zero (there is a hydrological- hydraulic demand) the indirect benefit adds a value to HHI value to estimate the demand for LID holistically. But, if HHI (direct benefit) is zero, even though indirect benefits are not zero, the demands for LID are estimated equal to zero.

In our proposed framework there is no mathematical limitations, and actual values of all parameters can be used as inputs. Finally, unlike models relying on the SWM, the proposed framework has no limits on the scale of the study area, since the number of input data is

independent from the scale of the area, and thus, the only cost is the computational time, which can increase based on the size of the area.

This paper is organized as follows: Section 2.4 presents the materials and methods including the case study, geospatial data, and the development of three new indices: the Hydraulic-Hydrologic Index (HHI), the Environmental Index (ENI), and the Socioeconomic Index (SEI), an approach to combine these indices into the proposed LID Demand Index (LIDDI). Section 2.5 includes the results and discussion including the generation of the HHI, ENI, and SEI maps for the case study and their validation as well as LIDDI map. Section 2.6 follows with conclusion.

2.4. MATERIALS AND METHODS

To address the inadequacies of existing approaches for the spatial allocation of LID, a geospatial physical-based framework is proposed which is then combined with a multi-criteria decision-making model. This framework was developed to identify sites with the greatest *demand* or *need* for LID, and to maximize both the direct and indirect benefits of LID.

To do this, three indices were developed to consider the direct (stormwater runoff reduction) and indirect (environmental and socioeconomic) benefits of LID. The first index, HHI was developed based on the physical principles governing stormwater runoff. HHI ranks the sites based on their potential for runoff generation. The second and third indices are ENI and SEI, respectively, which were generated using a SAW method within a hierarchical decision-making model. ENI and SEI identify sites with the highest demand of LID in terms of environmental and socioeconomic needs. Combining these three indices, the LID Demand Index (LIDDI) is then produced. The LIDDI ranks all sites within the study area based on their demand or need for LID

based on all hydraulic-hydrological, environmental, and socioeconomic benefits.

The conceptual framework of the method described above is presented in Figure 2.1. In this figure, the *variables* represent the physical-based parameters (for HHI) and geospatial criteria or indicators (for ENI and SEI). These variables, the secondary and primary indices are described in detail in the following sections.

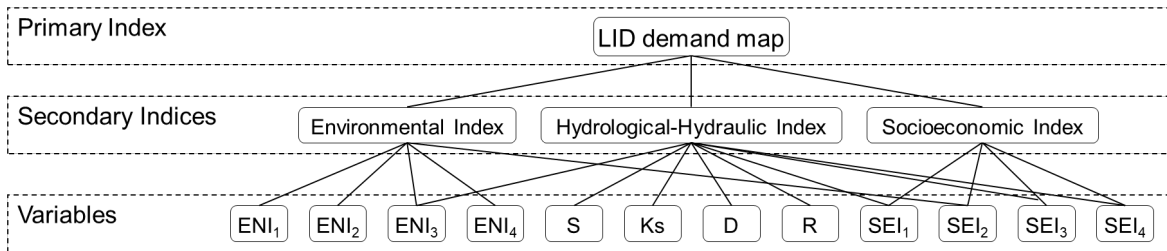


Figure 2.1 The schematic of the conceptual framework of LIDDI generation, where S is the slope (degree), K_s is saturated hydraulic conductivity (mm/hr), D is depth to restrictive layer (mm), and R is rainfall intensity mm/hr)

2.4.1. Study area

The utility of the proposed framework is demonstrated through case study: the study area used for this research is the City of Toronto which is located in Southern Ontario, Canada and covers an area of 630.2 km² with a population of approximately 2.73 million. The land-use varies from residential, commercial, and industrial to green spaces. Eleven major rivers pass through the city, dividing the city into eleven watersheds. Figure 2.2 presents the watersheds and their intersection with the administrative border of the City of Toronto. The use of LID has been growing in Toronto over the last several years [119]. Toronto is experiencing a transition period from grey (end of pipe methods) to green (using LID) infrastructure. This is done through developing and implementing a range of policy instruments, by-laws, and regulations, which

include developing and re-designing existing policies associated with land-use, environmental, water, infrastructure, and planning [94]. Some examples include the Green Roof By-law and Downspout Disconnection By-law [94].

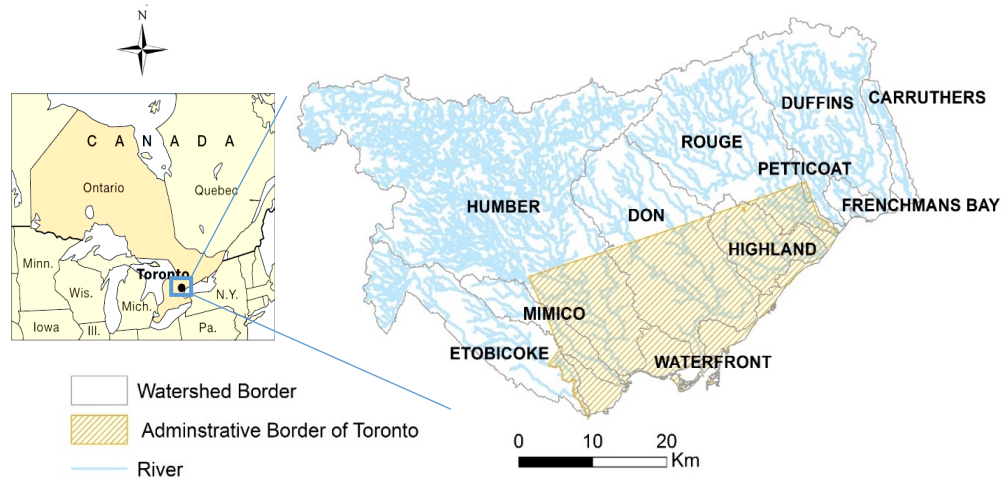


Figure 2.2 The extent of the study area (hatched in orange colour), which is the administrative boundary of the City of Toronto and its intersection with the eleven watersheds in Toronto

2.4.2. Geospatial data

In this study, data from open, publicly available sources were used and is listed in Table 2.1. This geospatial data was used to derive each of the parameters used for three indices; the rationale for selecting each data is discussed in detail below for each index. Each dataset was converted into raster format with a ground resolution of 5 m x 5 m (to align with the digital elevation model, DEM, resolution which was used as the reference resolution for this research). The framework was developed and implemented in ArcGIS.

The proposed framework, and specifically the application presented in this research, is restricted by the resolution of available data. Here, a raster resolution of 5 m x 5 m was used due

to the available DEM data. Higher or lower resolutions can be chosen, however this should be done with intent, as it can impact the accuracy and reliability of the results.

Table 2.1 The raw data downloaded from publicly available sources, including the structure/geometry of the data, and the source of the data.

ID	Data	Data structure/geometry	Data Source
1	Air pollution (TPM2.5)	Vector/point	Ministry of Environment, Conservation and Parks
2	Bedrock layer	Vector/polygon	Ministry of Northern Development and Mines
3	Census tract boundaries 2016	Vector/polygon	Statistics Canada
4	Demographics data - Census 2016	Tabular data	Statistics Canada
5	Digital elevation model (DEM)	Raster/5 mx 5 m	Ontario Ministry of Natural Resources and Forestry - Provincial Mapping Unit
6	Ecozones of Ontario	Vector/polygon	Scholars Geoportal
7	Groundwater table	Vector/point	Groundwater Information Network (GIN)
8	Land cover	Raster/0.6 m x 0.6 m	City of Toronto
9	Toronto rivers	Vector/polyline	Toronto and Region Conservation Authority (TRCA)
10	Surficial geology and saturated hydraulic conductivity (K_s)	Vector/polygon	Government of Canada open data website
11	Toronto precipitation data	Vector/point	Government of Canada open data website
12	Educational institute	Vector/point	City of Toronto
13	Hospital	Vector/point	Google Earth

Note: Missing data were ignored in the calculations.

2.4.3. Hydrological-hydraulic index (HHI) development

HHI ranks the cells (i.e., the pixels of the raster data) by their runoff or flood generation potential. Cells with higher HHI generate higher volume and peak runoff flow rate (referred to as High Runoff Cells). These cells should be the first target for implementing LID. However, wherein it is not feasible to implement LID, next target should be selected based on several parameters including the topography of the catchment amongst other parameters [104]. The selection of the

feasible sites is out of scope of this research and requires another investigation which incorporates results of this study (*demand*) to the feasibility.

To generate HHI, the geospatial variables that are representative of the runoff hydrograph were identified and quantified. Then, a geospatial overlaying heuristic relationship (Eq. 2.1) was developed according to the physical principles. The variables were then spatially overlaid based on the proposed relationship (Eq. 2.1).

To identify the variables, the runoff generation process, and the associated relationships (mathematical equations) were considered. Four variables were identified and quantified for HHI: rainfall intensity (R), hydraulic conductivity (K_s), water storage capacity of soil (D), and catchment slope (S).

Runoff is dependent on rainfall and infiltration. Rainfall intensity, denoted by R and measured in mm/hr, is especially important in large scale study areas where uneven spatial distribution of rainfall can be an important factor. By a simplification assumption we neglected the temporal distribution of R, and it was considered as constant. The value of R is obtained from the intensity-duration-frequency (IDF) curve for the City of Toronto and represents the extreme rainfall event. For this research, the intensity of the 100-yr 5-minute duration event was selected as R to represent extreme events. This rainfall is a sample of a low probability and intense rainfall event, though any other R value may be used since the focus is on the difference of R across the study area (rather than the magnitude itself).

Infiltration is a function of the soil moisture, porosity, hydraulic conductivity and water storage capacity of the soil. The Green-Ampt equation [120] demonstrates that if the antecedent soil moisture is saturated, the infiltration rate is equal to the saturated hydraulic conductivity (K_s). This allows to estimate the infiltration rate using K_s data: cells with higher K_s values have higher

infiltration rates, and consequently, generate less runoff. Note that urban areas contain significant impervious surfaces whose K_s is essentially zero, resulting in an infiltration rate that is also zero. Thus, the land-use data (specifically the impervious surface layer) was combined with the K_s of surficial geology data using the minimum geospatial operation tool in ArcGIS. With the minimum operation, in each cell the K_s of impervious surfaces (assumed to be 0 mm/hr) and the K_s of the surficial geology layer (which is greater than or equal to 0 mm/hr) is compared and the lower value is assigned to each cell. In addition, streams, rivers and other waterbodies within the study area were excluded from K_s layer and potential LID sites. Through geospatial subtraction operation, K_s values were subtracted from the rainfall intensity, R , resulting in an indicator for the runoff generation potential for each cell.

Infiltration volume is also dependent on the water storage capacity of the soil, which is further dependent on soil characteristics (e.g., soil porosity and moisture) and the thickness of the soil layers. Capacity, denoted by D , is quantified through three variables: the depth to groundwater table (D_g) and the depth to the first impermeable soil layer (bedrock) (D_r), and the soil porosity (n). The value of D takes the minimum of either D_g or D_r and represents the distance between the soil surface and the first restrictive layer. Capacity is then multiplied by the soil porosity, n , which quantifies the porous storage volume in the vertical direction. The calculated volume allows for additional quantification of runoff generation potential that considers both the infiltration rate and the water storage capacity. For instance, a cell with a high infiltration rate can be restricted by an impermeable soil layer, resulting in decreased infiltration.

The time of concentration (t_c) is another contributing variable to runoff generation; LID can be used to increase t_c in urban areas to reduce damage resulting from stormwater runoff. Two cells with the same values of K_s , R and D can generate the same runoff volume, however, the t_c

may be different. Using Kirpich's formula [121] t_c can be estimated using the catchment length and slope (S). When using cells with equal areas, the t_c is non-linear exponential function of the slope to the power of 0.385. To represent this nonlinear relationship of t_c and S, we generated the slope layer from the DEM data in ArcGIS and estimated the $S^{0.385}$ value using for each 5 x 5 m cell.

By identifying the contributing variables (R, K_s , D, and S), we developed a heuristic relationship (Eq. 2.1) to geospatially overlay the runoff contributing variables. Our relationship is developed based on the theoretical concepts of runoff generation. The validation of the relationship is presented in Section 2.5.4. Using this relationship, a value for each cell is calculated based on the potential of cells to generate runoff. The cells within the study area can then be compared in terms of their need or demand for LID. Cells with higher HHI have higher demand for LID; installing LID in a cell with a higher HHI captures more runoff or prevents the generation of runoff at that site, and attenuates t_c :

$$HHI_j = \begin{cases} [R_j - ((K_s)_j \cap (K_i)_j) \cap (n_j \times ((D_g)_j \cap (D_r)_j))] \times [1 + (\tan S)^{0.385}] & \text{for } R_j > K_{s_j} \\ 0 & \text{for } R_j \leq K_{s_j} \end{cases} \quad (\text{Eq. 2.1})$$

where j is the cell number, HHI_j is the HHI at cell j , R_j is rainfall intensity (mm/hr) at cell j , and $(K_s)_j$ is saturated hydraulic conductivity of surficial geology layer (mm/hr) at cell j , $(K_i)_j$ is the hydraulic conductivity of impervious areas (e.g. roads, parking lots and building roof tops) at cell j , set equal to zero for impervious cells, n_j is the soil porosity at cell j , $(D_g)_j$, $(D_r)_j$ are respectively, depth to groundwater (mm) and depth to the first restrictive soil layer (mm) at cell j , and S is the terrain slope (degrees) at cell j . Note that since physics-based variables were used to

formulate this heuristic relationship, dimensional consistency was ensured for all parameters considered. Also, in the lack of soil data still can be used. Whereas the data for K_s and D does not exist, there are two ways of using the relationship. Either K_s and D can be assumed based on known characteristics of the study area or assuming the worst-case scenario which is value of zero for these parameters ($K_s=0$ and $D=0$).

To generate the HHI map for the City of Toronto, the four variables in Eq. 2.1 (R , K_s , D , and S) were generated from the available raw data (Table 2.1) and converted to raster layers. Rainfall intensity, R , was derived from the IDF tables of three meteorological stations within the City of Toronto: Oshawa, Oakville Southeast, and Toronto Buttonville. The raster rainfall data for the study area were generated by geospatial interpolation using the point data from the three meteorological stations. The hydraulic conductivity, K_s , was derived from the surficial geology and land cover data as explained above (Table 2.1). To generate rainfall storage capacity of the soil (D), D_g was generated using groundwater level data of wells (in point data format). Using the geospatial interpolation within the study area and groundwater level data from the wells, the raster data layer of D_g was produced. D_r was generated from the bedrock data (in polygon data format). Using these two variables and a minimum geospatial operation tool in ArcGIS, the raster map of D was generated. The soil porosity (n) was assumed to be 0.5 for the entire study area due to the lack of available porosity data. According to Chow et al. [122], this is an average estimate of porosity for different soil types (sand, loam, silt, and clay). Terrain slope (S) was derived from DEM data using the slope tool in ArcGIS. In addition to these variables, a data layer consisting of the existing LID (using only existing tree canopy was considered which was derived from the land-cover data) was also generated in order to eliminate these sites as potential sites for implementing LID. Due to the lack of data of actual LID currently installed within the study area, other types of

LID such as green roofs, raingardens, etc. are neglected in this study. Due to this, the existing LID facilities are still considered as potential LID sites; however, if this data were available existing LID sites may be eliminated from the analysis if required.

2.4.4. Environmental index (ENI) development

The ENI quantifies the relative demand of cells for LID (specially GI) in terms of environmental needs. ENI is associated with mitigating or preventing environmental damage that result from anthropogenic sources such as urbanization. The environmental criteria were selected based on the DPSIR (Drivers, Pressures, State, Impact and Response) model developed by the European Environment Agency [123]. Based on DPSIR, urbanization is the “driving force” causes “pressures” that include pollution, and changes in land-use and habitat population. These “pressures” cause changes to the “state” of the environment (air quality, biodiversity, water quality and soil quality). These changes lead to negative “impacts” on public health and ecosystems, which can elicit a positive or negative response feeding back into the “driving forces” (or to the “impacts” and “states” directly). GI are considered as a “response” model of intervention to these “impacts”; other “responses” such as environmental laws can also be applied. The criteria for ENI represent the environmental “states”; the four sample environmental states used for this research are: air quality, bio-habitat, water quality, and soil quality. Specifically, the criteria include air pollution denoted by ENI₁, biodiversity denoted by ENI₂, water quality denoted by ENI₃, and soil contamination denoted by ENI₄ all of which are caused by urbanization and for which GI can be used as response to mitigate the impacts.

Higher ENI₁ values were assigned to sites with higher concentration of air pollution, as

they were considered to receive the greatest benefit from the GI in terms of air quality [32], [47]–[49]. In particular, LID (planted-based types) reduces the concentrations of a variety of air pollutants that are known to increase health risks, such as PM_{2.5} [124], [125]. In the proposed framework, PM_{2.5} concentration was chosen as the indicator of overall air pollution, as is often done in the literature.

Higher ENI₂ values were assigned to sites with higher biodiversity to ensure the existing bio-habitats are maintained. GI provides potential bio-habitat and consequently prevents the impact of urbanization on existing habitats [32], [53]–[59]. For example, previous studies have shown that green roofs can host diverse plants and animals, as well as function as stepping stones to other nearby habitats, particularly for immobile organisms [126]. In another study, this effect is highlighted when a 41 % increase in forest coverage led to an increase of 81 bird species – highlighting that tree-based LID or GI may have a positive impact on bird species [127]. Thus, the ecozones of Ontario (collected from the Scholars Geoportal website, <http://geo2.scholarsportal.info>) was used as an indicator of the biodiversity within the study region.

GI are intended to capture and treat stormwater at the source (often referred to as “source control”). In doing so, GI can effectively capture contaminants (e.g., sediment which themselves contain other chemicals such as metals) [36]. Previous research has shown that GI such as bioretention cells can treat stormwater through physical, chemical and biological processes. Specifically, they provide filtration, sedimentation, adsorption as well as plant and microbial uptake [128]. Through these processes, pollutant concentrations of metals (zinc and copper), total suspended solids, total phosphorus, and total nitrogen have been reduced by more than 90% [128]–[130]. Capturing these contaminants at the source (i.e. upstream of the drainage point or outlets to rivers) prevents the contaminants from flowing downstream and also reduces the spread of

contaminants within the watershed [131]–[133]. Thus, for this research, higher ENI₃ values were assigned to sites farthest from rivers as an indicator of “source control” to improve water quality in the rivers. Areas closer to the rivers were given lower priority (lower ENI₃), whereas areas farther upstream were given higher priority in terms of LID (specially GI) need or demand.

Sites with GI installed maintain neutral pH, increased metal retention, and reduced risk of diffusion, all of which are attributed to the enhancement of biochemical processes in the soil by GI [43], [134]–[136]. To prevent the contamination of soil, stormwater runoff and sites closest to pavements were assigned higher ENI₄ values (and thus higher priority). Roads and parking lots were considered to be the sources of the soil contamination yielding high concentrations of pollutants such as zinc, copper, lead and cadmium, most often found at inflow points [129].

For the City of Toronto, the ENI₁ values were derived from point data of eleven air quality monitoring stations from the Ministry of Environment, Conservation and Parks. The air quality data layer was interpolated and converted to raster layer using an Inverse-Distance-Weight method. The ENI₂ values were derived from the total population of terrestrial bird, mammal, reptile & amphibian, and tree species per unit area of the according ecozone (from the Ecozones of Ontario database). The ENI₃ were calculated using the Euclidean distance, river cells have distance equal to zero and cells farther from the river have higher Euclidean distance. For ENI₄ values, road and parking lot surfaces were extracted from the land cover map, assigned as sources, and distances from these sources were estimated using the Euclidean distance similar to the ENI₃ process.

All four selected criteria were standardized by applying the linear standardization method (Eq. 2.2).

$$SENC_{j,k} = \frac{ENC_{j,k}}{(ENC_k)_{\max}} \quad (\text{Eq. 2.2})$$

Where k is the total number of criteria (in this case, 4), j is the total number of cells in the study area, $SENC_{j,k}$ is the standardized environmental criteria k at cell j , $ENC_{j,k}$ is the actual value of environmental criteria k at cell j , and $(ENC_k)_{\max}$ is the greatest possible value of environmental criteria k within the study area. After standardization, the overall ENI for each cell was calculated by overlaying all four criteria, using the simple additive weighting (SAW) method (shown in Eq. 2.3).

$$ENI_j = \sum_1^k w_k \cdot FENC_{j,k} \quad (\text{Eq. 2.3})$$

where ENI_j is the value of ENI at cell j , $FENC_{j,k}$: is the finalized environmental criteria k at cell j , which can be derived from Eq. 2.4, and w_k is the weight of criteria k .

$$FENC_{j,k} = \begin{cases} SENC_{j,k} & , \text{for direct distance criteria} \\ 1 - SENC_{j,k} & , \text{for inverse distance criteria} \end{cases} \quad (\text{Eq. 2.4})$$

2.4.5. Socioeconomic index (SEI) development

The SEI quantifies the LID demand of each cell in terms of the socioeconomic benefits of LID (specially GI and planted-based LID). In addition to the hydrological and environmental benefits, GI also improves socioeconomic status in a variety of ways, including increasing access to green spaces, enhancing academic performance in schools, enhancing public health, and social

resilience [33], [34], [63], [137]–[141]. To address these benefits, priority was assigned to cells using four sample socioeconomic factors: population density (SEI_1), distance to green spaces (SEI_2), distance to educational centers (SEI_3), and distance to hospitals (SEI_4).

Higher SEI_1 were assigned to sites with a higher population density in order to serve a higher population to serve a serving higher population with indirect benefits of GI. The second criteria (SEI_2) prioritizes sites that are farthest from existing green spaces; this creates an even distribution of green spaces. Areas with sparse landscaping, more deprived neighborhoods, and low public transport availability are identified as having the greatest demand for the benefits associated with LID (specially GI types) [61], [139]–[141].

The third criteria (SEI_3) gives priority to sites closest to educational centers and schools. Studies have shown that LID and GI improve the educational performance, and socioemotional, behavioral and cognitive development of students [142], [143]. In particular, preschoolers at educational risk were found to have greater development of independence and social skills when enrolled to schools with higher levels of plant-based LID [142]. The fourth criteria (SEI_4) assigns priority to sites that are closer to hospitals to improve the health status of patients. Studies have shown that patients with green window views recovered significantly faster and required less medication compared to patients with urban views [144]. Indeed, green spaces are widely associated with enhanced immune functioning, and greater mental well-being [62], [141]. Furthermore, green spaces have been shown to lower fasting blood glucose levels in both adults and children, effectively lowering the risk of diabetes, which is now recognized as one of the leading causes of illness and death [140].

A fifth socioeconomic benefit is social resilience, which comes in the form of provisioning services. Provisioning services yield products such as firewood, medicinal plants, and wild foods.

Studies have shown that poor households and vulnerable populations highly rely on GI to support their daily livelihood needs. One study found that 57 % of households on average use GI as a coping strategy as a response to co-variate shocks such as floods [138]. This benefit is harder to quantify due to the lack of available data. Because of this, quantifications of socioeconomic benefits often underestimate the actual benefits that can be obtained. Nevertheless, social resilience is highlighted as a great benefit to particularly vulnerable populations and could be included in future studies if relevant data is available.

For the City of Toronto, SEI_1 was estimated based on the 2016 census data, by dividing the population with the area of the corresponding census tract. SEI_2 , the distance from existing green areas was estimated by the Euclidean distance; higher values were assigned to sites further away from existing green areas. The raster map of the third criteria (SEI_3) was also estimated by calculating the Euclidean distance, with the location of educational centers (in point data) assigned as sources. SEI_4 was also derived with the same process as SEI_2 and SEI_3 .

As with ENI, the variables were standardized by applying the linear standardization method using Eq. 2.5.

$$SSE_{j,m} = \frac{SEC_{j,m}}{(SEC_m)_{max}} \quad (\text{Eq. 2.5})$$

where, k is the total number of criteria (in our study case, 4), j is the total number of cells in the study area, $SSEC_{j,m}$ is the standardized socioeconomic criteria k at cell j , $SEC_{j,m}$: is the actual value of socioeconomic criteria k at cell j , $(SEC_m)_{max}$: is the greatest possible value of environmental criteria k within the study area. After standardization, the overall SEI for each cell was calculated by overlaying all four criteria, using the simple additive weighting (SAW) method (shown in Eq. 2.6).

$$SEI_j = \sum_1^m w_m \cdot FSEC_{j,m} \quad (\text{Eq. 2.6})$$

where, SEI_j : is the value of SEI at cell j , $FSEC_{j,m}$: is the finalized environmental criteria k at cell j , which is derived from Eq. 2.7, w_m is the weight of criteria k .

$$FSEC_{j,m} = \begin{cases} SSEC_{j,m} & , \text{ for direct distance criteria} \\ 1 - SSEC_{j,m} & , \text{ for inverse distance criteria} \end{cases} \quad (\text{Eq. 2.7})$$

2.4.6. LID demand index (LIDDI)

The LIDDI represents the sites ranked by their respective demand for LID, with the combined consideration of all hydrological and hydraulic, environmental, and socioeconomic variables. High LIDDI values represent sites with the highest demand or need for LID. To generate the LIDDI, the SEI and ENI were first geospatially overlaid using SAW method to generate SEENI (Eq. 2.8). The relationship between the weights of the method is shown in the Eq. 2.9. In this equation W_{EN} is the sum of w_k and W_{SE} is the sum of w_m .

$$SEENI_j = w_{EN}ENI_j + w_{SE}SEI_j \quad (\text{Eq. 2.8})$$

$$W_{EN} + W_{SE} = \sum_1^k w_k + \sum_1^m w_m = 1 \quad (\text{Eq. 2.9})$$

where, $SEENI_j$ is the environmental-socioeconomic index at cell j , ENI_j is the environmental index at cell j , SEI_j is the socioeconomic index at cell j , w_{EN} is the corresponding weight of ENI, and w_{SE} is the corresponding weight of SEI. As demonstrated in Equations 3.2-8, the proposed framework to generate SEENI is not restricted by the number of environmental and socioeconomic criteria selected nor the assigned weight to each criterion. The number of criteria is considered, and the weights assigned to each criterion can be customized based on an end-user's needs, data availability, or other requirements. Thus, this framework has been developed in a way to be customizable to determine the need or demand for LID based on which benefits need to be considered or incorporated into the framework.

The resulting SEENI is proposed as an *additive value*, where it can be overlaid onto the HHI through a mathematical multiplication operation to generate the LIDDI, the overall demand for LID (Eq. 2.10).

$$LIDDI_j = HHI_j \times (1 + SEENI_j) \quad (\text{Eq. 2.10})$$

where $LIDDI_j$ is the demand of cell j for LID.

SEENI was considered as an *additive value* due to the multiple advantages it provides. First, two cells with identical HHI but differing SEENI values can be ranked distinctly based on their environmental and socioeconomic demand for LID. This allows the main objective of this framework to be achieved: spatial allocation of LID with the combined considerations of hydrological and hydraulic, environmental, and socioeconomic factors. Table 2.2 shows a simple example to illustrate these concepts: the effect of SEENI on the HHI and final LID demand Rank of the three sample cells. Two areas with equal HHI but unequal SEENI (Cells 1 and 2), will result

in different LIDDI, and the final rank is impacted by the cells with higher SEENI values. Secondly, since the primary goal of LID is stormwater runoff management, a site that does not generate runoff does not require LID (even if an environmental or socioeconomic demand for it exists, as shown in Table 2.2 Cell 3). In the framework, cells with HHI values equal to zero, but high SEENI values will result in LIDDI values of zero. This ensures that LID is not unnecessarily implemented in sites without a hydrological or hydraulic need.

Table 2.2 The effect of SEENI on the HHI in two sample cells

Cell #	HHI	SEENI	LIDDI	Rank
1	0.9	1	1.8	1 st
2	0.9	0	0.9	2 nd
3	0	1	0	3 rd

2.4.7. Adaptability of the proposed framework

The proposed framework can be adapted in various ways for the intended application, project requirements or stakeholder opinions.

Our proposed framework can be used for all types of LID, generally categorized as detention (such as tanks), planted infiltration (e.g., raingarden) and dry infiltration (e.g., infiltration trenches) types [145]. Note that for our case study, we only use planted infiltration or GI types of LID for Toronto to demonstrate the utility of the proposed approach. Accordingly, all the associated co-benefits are those benefits that correspond to GI or planted infiltration LID techniques. If a different subset of LID is used, using the proposed approach, the co-benefits should be selected to be compatible with the actual co-benefits of those LID.

To generate HHI we did not standardize the data and actual values with consistent dimensions were used. Regarding the SEI and ENI, we standardized all criteria using linear value

scaling method ranging between 0 and 1 (Eq. 2.2 and Eq. 2.5). This selection was based on several reasons: the exact correlation between each single criterion and result (the decision which is going to be made) is unknown. Despite that we know that each criterion has an increasing or decreasing influence on the results, but the exact linearity or nonlinearity of this change is not clearly proven. However, our framework allows the end-user to select among other standardization methods such as score range, value function, utility function, probabilistic and fuzzy. This selection, though should be based on the expert judgment (as it was performed in e.g., [86]), which is recommended and performed in literature such as [146], [147].

The weights used in the SAW hierarchical model for ENI and SEI in this research were chosen based on the particular study area, team judgement and expertise. However, these weights are adjustable, we suggest generating the weights through a systematic process such as Analytical Hierarchy Process (AHP) using weighting methods such as the Pairwise Comparison (PC) combined with a method like Delphi, which relies on a panel of experts.

Also, the four criteria used for ENI and SEI, respectively, are not restricted to the criteria we selected for this study: they can be customized according to the environmental and socioeconomic concerns of the study area, availability of data and be estimated and incorporated into HHI using Equations 3.2-8.

2.5. RESULTS AND DISCUSSION

To evaluate the effectiveness of the proposed framework, the three indices HHI, ENI and SEI were generated, followed by the SEENI and then the LIDDI for the City of Toronto. The resulting maps are color-coded to show the gradient from lowest (green) to highest (red) demand

of LID. Additionally, the HHI map was compared to the historical flood data and further validated against a physical-based hydrological model (HEC-HMS). The results are presented, analyzed and discussed in this section.

2.5.1. HHI map

The resulting HHI map is presented in Figure 3(f), along with the data layers of the required variables R , K_s , D , and S . The map of existing LID is included as well. Figure 3(a) shows that overall, the City of Toronto has a low K_s (and therefore a high LID demand) across the city, though there are some high K_s areas in the eastern and western parts of the city. Figure 2.3 (b) indicates a relatively low slope for the city, with higher slopes located along riverbanks. Sites with slopes greater than 45 degree were excluded as potential LID sites. This was due to two reasons: first, the maximum long-term stable cut slope is 45 degree [148], second, to cope with the DEM data error, in which the difference between the elevations of some new urban developments (such as bridges) and surrounding area were falsely estimated as a high slope. Figure 2.3 (c) shows that D is higher at the same regions with high K_s , except for northern part of the city. Figure 2.3 (d) shows a 20 mm/hr difference in average rainfall intensity across the city. Figure 2.3 (e) shows the areas with existing tree canopies, which were eliminated from potential areas for LID implementation and excluded from further analysis. As described earlier, tree canopies were used as a proxy for existing GI due to the insufficient data available.

By geospatial overlaying of all variables using Eq. 2.1, the HHI map was generated, as presented in Figure 2.3 (f). Comparing the HHI map Figure 2.3 (f) with the input variable maps (Figure 2.3 (a) to (e)), high HHI areas are located in areas with low hydraulic conductivity (K_s),

high precipitation intensity (R), low depths to restrictive layers (D) and high terrain slopes (S).

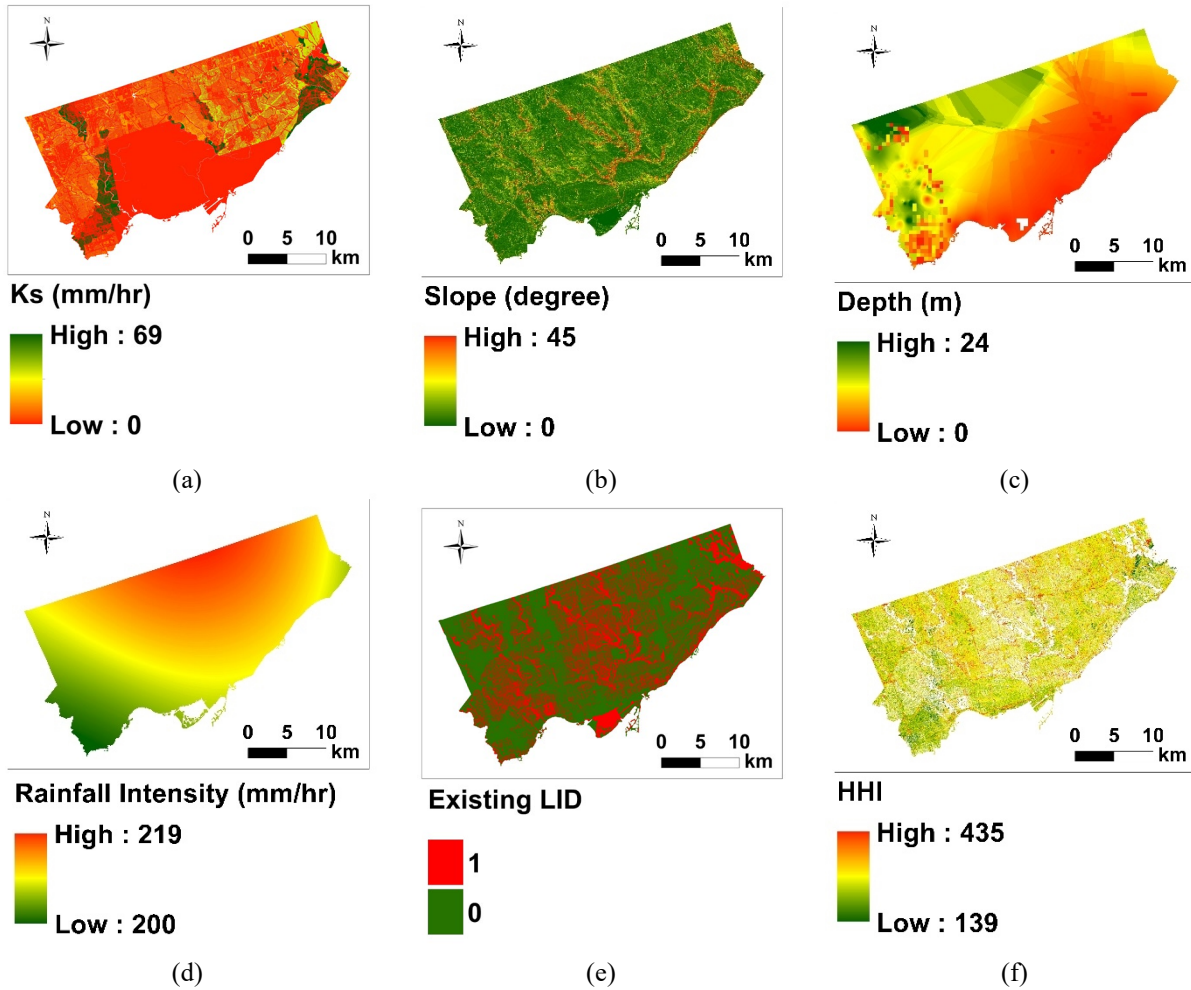


Figure 2.3 Input variables (a) hydraulic conductivity, K_s (b) terrain slope, S (c) depth to restrictive layer, D (d) rainfall intensity, R (e) existing LID, and (f) the generated HHI map (in all maps, red colour indicates high LID demand and green colour indicates low LID demand)

Assigning HHI values to an area allows filtering or ranking sites by their runoff generation potential. Identification of high HHI sites targets the main source of runoff generation for LID implementation, and thereby effectively maximizes runoff reduction. Furthermore, the HHI map can show the relationship between historically flood-prone areas and high HHI sites.

To demonstrate the application of filtering cells with high HHI, we considered the highest

2.3 % HHI (mean value plus two standard deviations of HHI) cells as the highest priority for LID implementation within the region. For Toronto, these are sites with HHI values of 0.56 or greater (if we linearly rescale HHI in range 0 and 1). Figure 4 presents the map of these highest 2.3 % HHI cells and also contains TRCA's data on historically flood-vulnerable areas [149], shown in dashed circles. The impact of upstream flood sources (i.e., areas with high HHI) on downstream areas (the encircled flood-vulnerable areas) is evident, illustrating the usefulness and utility of the proposed HHI. This is especially critical since significant parts of the upstream Humber and Don Rivers are outside the study area, and the contribution of these areas on downstream flood generation must also be considered.

From Figure 4, areas upstream the flood-prone areas are often, though not always, associated with higher HHI. Downstream of the confluence of the Don River branches, Figure 2.4 areas (a) and (b) (East Don, West Don and Taylor/Massey Creek) are historically vulnerable to flood. HHI values suggest this vulnerability originates from the upstream East Don River and the main inlet of Taylor/Massey Creek. However, high HHI areas of the western branch of the Don are lower and are mostly concentrated on the central parts of the city and may be the origin of the flooding at Figure 2.4 areas (a) and (c). In addition, upstream of areas (d) and (e) shows a high concentration of high HHI values.

West of the Don watershed, the Humber watershed shows flood vulnerable areas along and slightly east of the Black Creek River. High HHI sites are also seen along this branch (upstream of areas (f), (g) and (h)), decreasing downstream towards the confluence with Albion Creek (between areas (h) and (i)). This is in contrast to the lower HHI areas along Albion Creek (downstream of the area (k)), though there is a concentration of high HHI cells at the upstream and near (k).

On the eastern part of the city, the Highland watershed, also has flood vulnerable areas located along all four branches of the main river (Malvern, Bendale, Dorset Park, Centennial Creek), as marked by (l), (m), (n), (o), and (p) in Figure 4. HHI results shows that upstream of each of these four branches are areas with high values of HHI and therefore sources of runoff generation. The resulting HHI map combined with the historically flood vulnerable areas of the city demonstrates that the HHI can successfully identify areas with high runoff generation and its relationship to downstream flood-vulnerable clusters. Thus, the HHI is effective in correlating the geographical locations of potential sources of flood to observed flood locations.

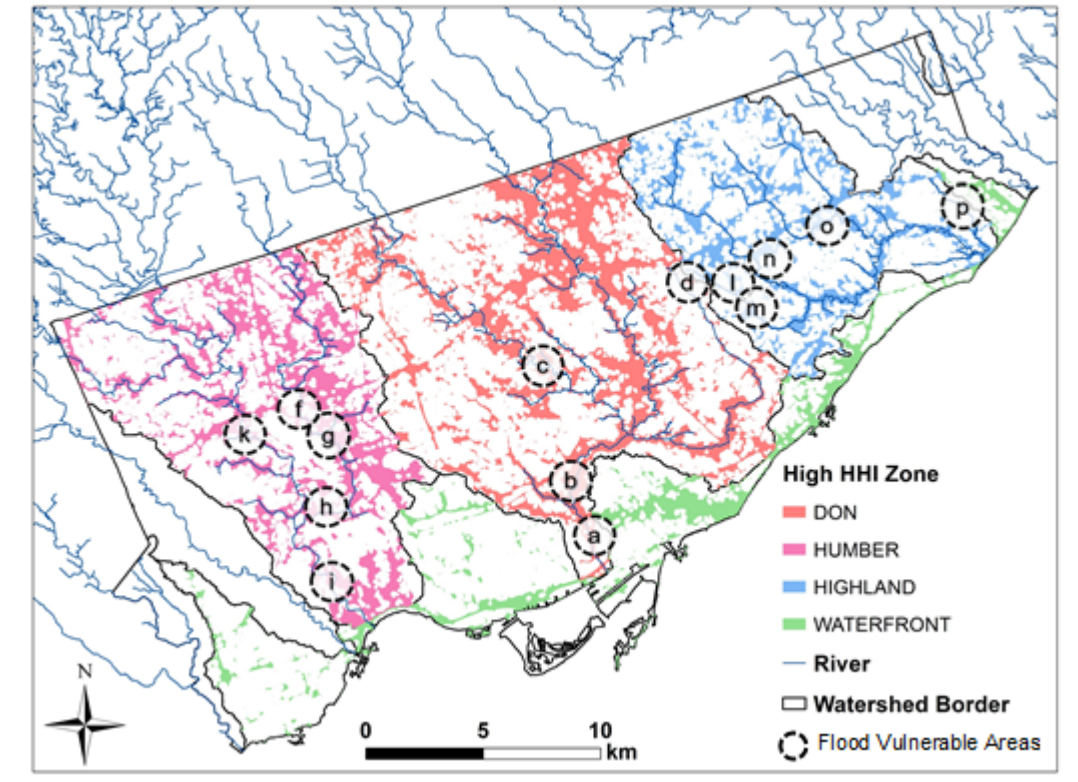


Figure 2.4 Top 2.3 percent ranked sites with a high standardized HHI of 0.56 and greater (these areas are presented for each watershed within the study area) and the location of historically flood vulnerable areas of the City of Toronto

The HHI results were then statistically analyzed for the entire study area and for each main watershed. Segmenting Toronto by cells (5 m by 5 m in size) resulted in 25.4 million cells. By extracting the cells without available data, water bodies and existing LID 17.9 million potential LID cells remain. The mean calculated standardized HHI (if linearly rescaled between 0 and 1, which is not necessary and we only performed it for comparison purposes) for all cells is 0.4 with a standard deviation of 0.079. Figure 5 shows a plot of the HHI values versus the normalized count of cells within the entire study area and each watershed. By investigating the watersheds individually, Figure 5 demonstrates that the Don has the highest mean HHI of 0.427, whereas Etobicoke has the lowest mean HHI of 0.374. Thus, in terms of runoff generation potential, the HHI values for each watershed can show the relative demand for LID in each watershed. In this case, the demand for LID in the Don (a highly urbanized watershed and centrally located within the city) is highest, and lowest in Etobicoke. Further validation and verification of the HHI is provided in the Section 2.5.4 that calculates the HHI for a site and directly compares it to runoff generation volumes from a hydrological model.

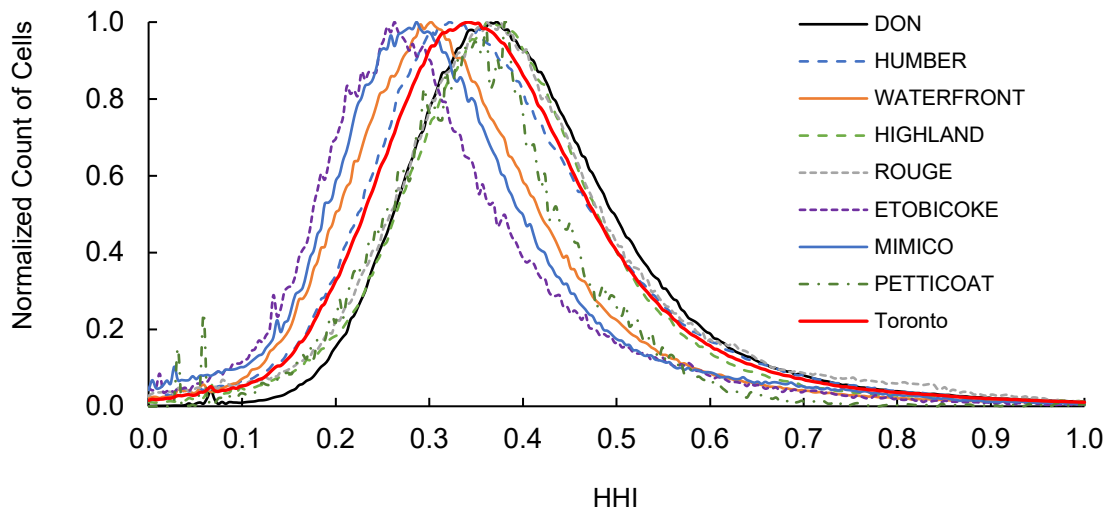


Figure 2.5 Normalized frequencies of HHI within 8 watersheds and City of Toronto.

Normalization of each watershed is performed by dividing the HHI frequency of each watershed by its maximum HHI frequency

The resulting HHI from geospatial analysis of physical-based processes is a quantification of the sources of runoff generation. This allows decisions to be made about micro-scale sites (25 m²) within a bigger macro-scale study area (630.2 km²). HHI highlights areas that contribute the most to flood, here high HHI areas are shown to produce flood vulnerable areas downstream. Selecting these sites for LID implementation improves the effectiveness of LID while efficiently allocating resources in stormwater management.

2.5.2. ENI map

To generate the ENI map for the City of Toronto, data for the four criteria (ENI1 to ENI4) were collected, converted to raster format (gridded cells) and standardized (using Eq. 2.2 and Eq. 2.3). The resultant maps are presented in Figure 2.6. Figure 2.6 (a) shows that the concentration of air pollution (ENI1) is located at the central areas of Toronto. ENI2 (Figure 2.6 (b)) indicates that Toronto contains four different ecozones with one being significantly more dominant, covering the majority of the city. ENI3 (Figure 2.6 (c)) shows the distance to rivers with river boundaries clearly noticeable. ENI4 (Figure 2.6 (d)) shows highly developed areas while less developed areas are around rivers and green spaces. All four layers (ENI1 to ENI4) were combined using the method described in Section 2.4.4 in order to generate the ENI map (Figure 6(e)). The resultant ENI map assigned higher priorities to areas farthest from the rivers, located in the central part of the city. The highest ENI are seen in the Waterfront, Humber, Don and western regions of the Highlands.

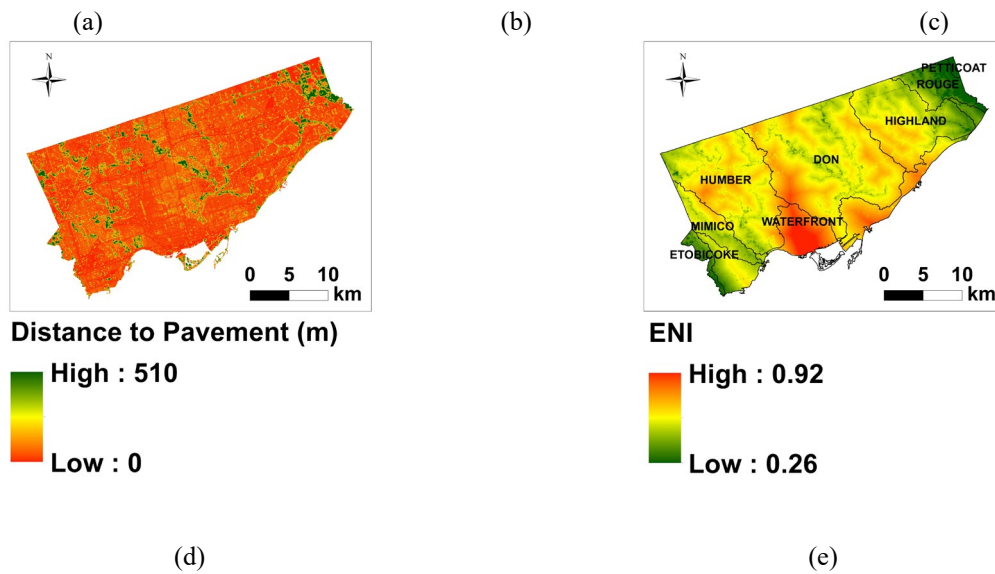
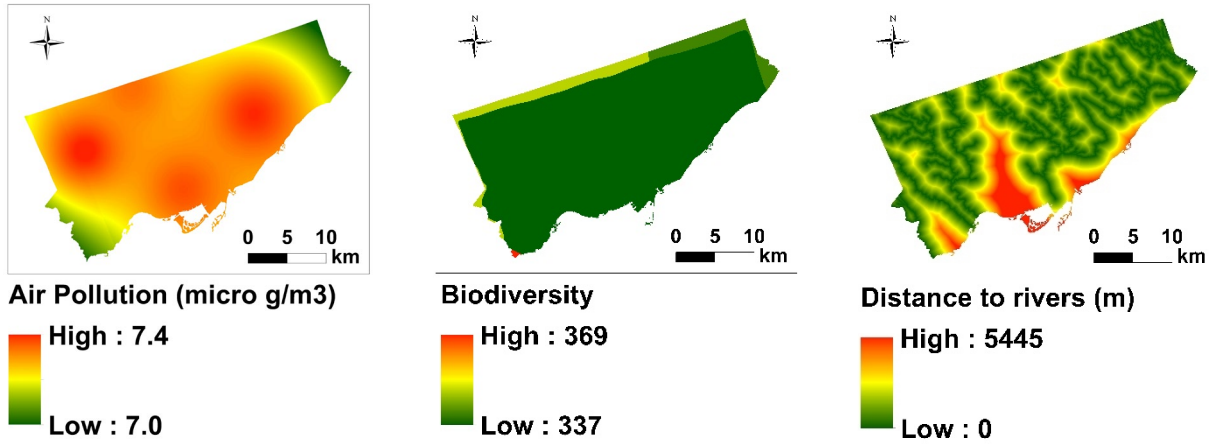


Figure 2.6 Input environmental variables (a) air pollution (ENI_1), (b) biodiversity (ENI_2), (c) distance to rivers (ENI_3), (d) distance to pavements (ENI_4), and (e) the generated ENI map of City of Toronto. In all maps, red color indicates high LID demand and green color indicates low LID demand.

2.5.3. SEI map

To generate SEI, all four criteria maps (SEI_1 to SEI_4) were created from the raw data, standardized and overlaid (Eq. 2.5 and Eq. 2.6). Each map is shown in Figure 2.7. SEI_1 (Figure 2.7 (a)) indicates that the highest populated areas are located in Downtown Toronto. Similarly,

multiple census tracts with high population densities are scattered across the city. SEI₂ (Figure 2.7 (b)) shows that the LID demand for green spaces is higher downtown. Other high priority areas that are scattered across the city shows impervious areas, some of which are used for industrial land. SEI₃ (Figure 2.7 (c)) shows a high and evenly distributed pattern of educational institutes throughout the city. SEI₃ (Figure 2.7 (d)) shows hospitals mostly concentrated on the south-western part of the city. All four generated maps were overlaid to generate the SEI map (Figure 2.7 (e)) with highly urbanized areas showing the greatest socioeconomic demand for LID.

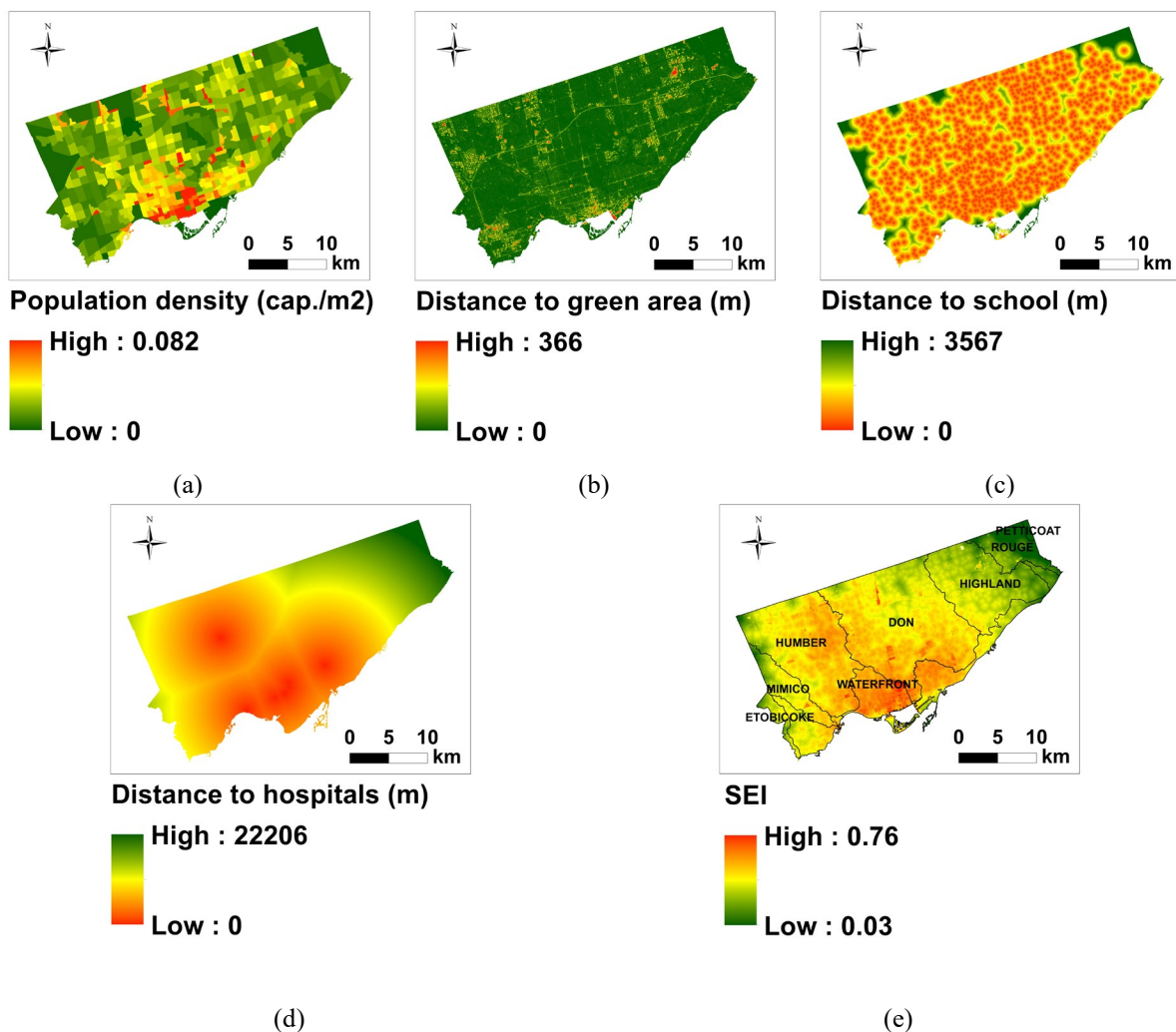


Figure 2.7 Socioeconomic variables (a) Population density, (b) Distance to green area, (c) distance to educational institutes, (d) distance to hospitals, and (e) the generated SEI. In all maps, red indicates high LID demand and green indicates low LID demand.

2.5.4. Validation

HHI validation

We developed the HHI heuristic relationship based on the hydrological-hydraulic principals. HHI is a GIS-based index representing the runoff generation potential of each cell. Thus, HHI should be able to rank various catchments with different hydrological-hydraulic characteristic (R, D, Ks, and S). To examine the HHI performance we validate the HHI against a physical-based model. The validation was done by comparing the results of HHI to a physical-based hydrological numerical model, the Hydrologic Modelling System (HEC-HMS) developed by the U.S. Army Corps of Engineers [150] – a commonly used hydrological model. A sensitivity analysis was conducted by calculating the HHI using extreme cases for each of the variable used to develop the HHI (which are listed in Table 2.3) and running the HEC-HMS model for the same values. A combinatorics approach was used to define 16 variants of catchments (or scenarios), and these are illustrated in Figure 2.8.

Table 2.3 Variable Values considered for 16 scenarios

	Low	High
R (mm/h)	50 ¹	220
D (mm)	0	24000 ²
Ks (mm/h)	0.3	117.8
S (m/m)	0.0001	0.15 ³

¹ Minimum R was not considered zero allowing for generating a low amount of runoff

² Maximum D layer is selected according to maximum D of the study area

³ Maximum S was considered to be 0.15 (= tan 9°), which is the greatest maximum proposed slope for all types of LID [109]

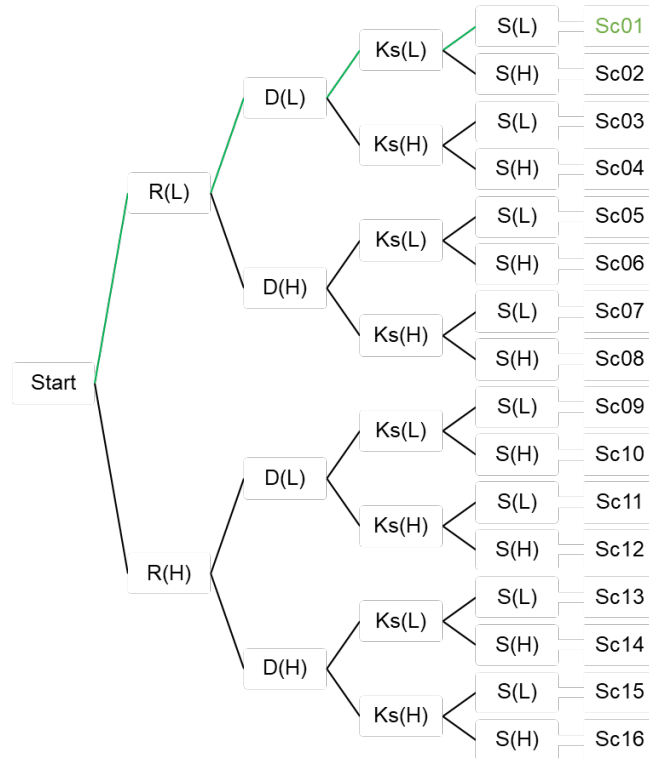


Figure 2.8 The 16 scenarios considered based on combinatorics concept

The resultant hydrographs from HEC-HMS for all 16 scenarios were created and normalized and each scenario was ranked based on the peak flow and flow volume. On the other hand, the HHI were calculated for all 16 scenarios as well, and subsequently these scenarios were ranked based on the HHI values. Results from both methods were compared and contrasted and are presented in Figure 2.9.

The methods show near identical results, with the exception of scenarios 9, 11, and 13. As expected, Sc10, Sc12 and Sc14 (High R and S, low K_s , or D) show the highest potential for runoff generation, whereas Sc07 and Sc08 (Low R and S, High K_s , and D) do not generate any runoff. HHI values are lower than the HEC-HMS values only for the flatter catchments, which is expected. Since HHI accounts for slope, runoff volume and peak flow, HHI of steep catchments are expected

to be higher than the HHI of catchments with low slop. Thus, the flat catchments should be considered lower priority than steeper catchments with other parameters being identical. This demonstrates how HHI incorporates the slope with the peak flow and runoff volume in order to rank each scenario.

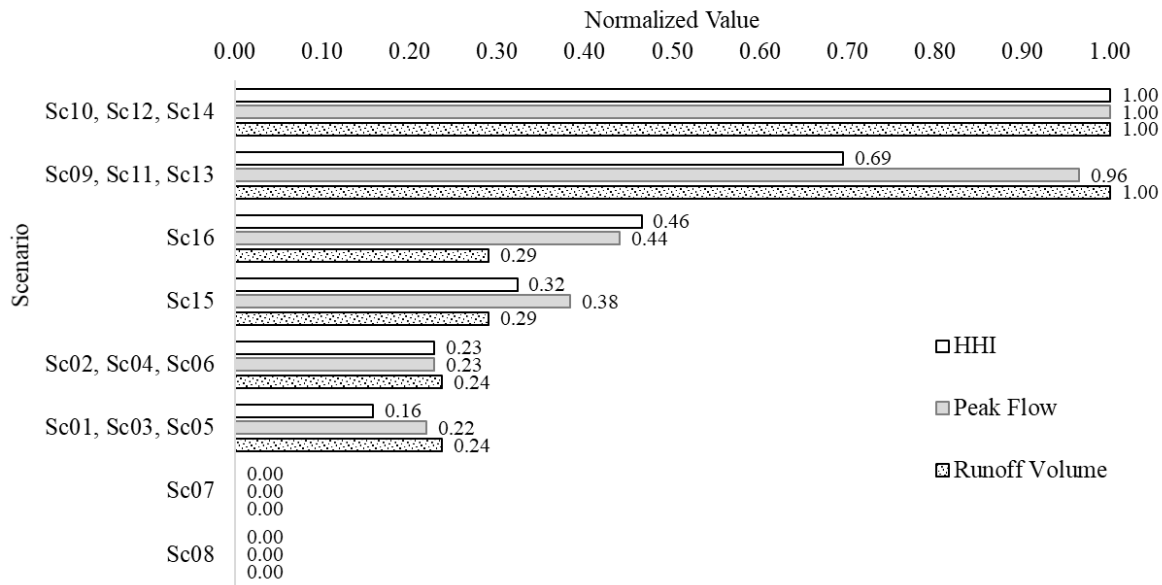


Figure 2.9 Comparison of HHI with HEC-HMS for 16 extreme scenarios

The hydrographs of each catchment were compared in the following criteria: peak flow, runoff volume, and time of concentration, as shown in Figure 2.10. From this figure, the normalized hydrographs show approximately three types of runoff volume: high, medium, and low peaks. The ranking obtained from Figure 2.10 are identical to the rankings obtained from HHI. The highest peaks are also the scenarios that obtained high HHI rankings. Within each grouping, the scenarios with the steeper slopes but similar other variables, are ranked higher than those with lower slopes. From the agreement between the HHI and HEC-HMS, HHI demonstrates its capability to rank scenarios based on the hydrological and hydraulic demands, using publicly

available geospatial data and geospatial analysis.

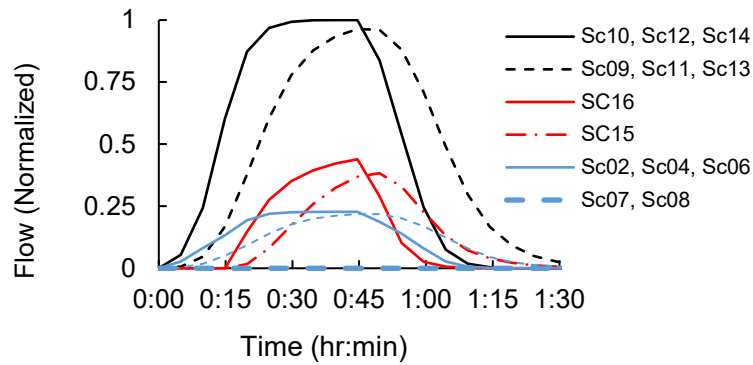


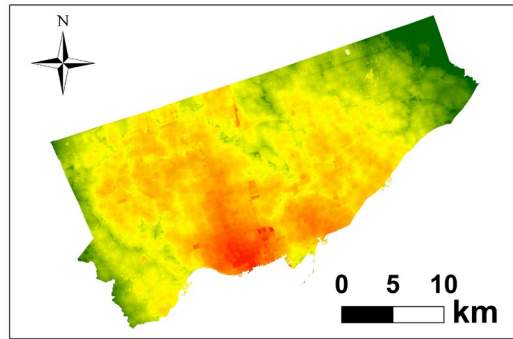
Figure 2.10 The normalized hydrograph of all 16 catchments resulted from modelling in the HEC-HMS

ENI and SEI validation

Validation of decision-making models is not practical since these models are not representing an actual phenomenon, which is extensively discussed in Kuller et al. (2019) [86].

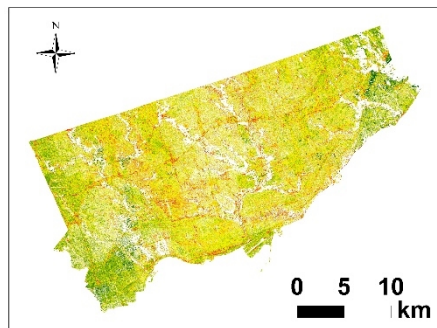
2.5.5. LIDDI map

To generate the LIDDI map, the SEENI was first calculated by combining SEI and ENI (Eq. 2.8), as presented in Figure 2.11. SEENI was then overlaid with HHI (Eq. 2.10) to generate the LIDDI map, presented in Figure 2.12 (a). Values of LIDDI range from 0 to 1.62, with a mean of 0.63 and standard deviation of 0.125. The top 2.3 % that represent sites with values greater than two standard deviations are those with an LIDDI value of 0.88 or greater as shown in Figure 2.12 (b).



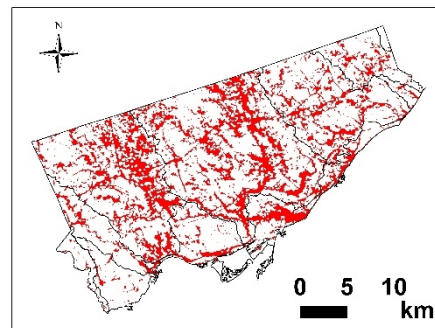
SEENI
 High : 0.75
 Low : 0.24

Figure 2.11 The generated SEENI map resulting from geospatial overlaying of ENI and SEI



LIDDI
 High : 1.62
 Low : 0

(a)



Top 2.3% LIDDI
Watershed Border

(b)

Figure 2.12 (a) LIDDI map generated from geospatial overlaying of SEENI, and HHI (b) top 2.3 percent sites ranked with the highest demand for LID

By comparing the map shown in Figure 2.12 (b) with the HHI map shown in Figure 2.4, the influence of SEENI on HHI can be observed. In particular, they show the sites that were excluded (or included) due to the lack of consideration for the socioeconomic and environmental

demands (i.e., the impact of SEI and ENI or overall LID demand) that would have otherwise been obtained from SEENI.

To clearly demonstrate this, two regions with low and high values of SEENI are shown in Figure 2.13. Figure 2.13 shows HHI overlaid with LIDDI. Figure 2.13(c) (area with high SEENI), the cells that were previously excluded as high priority under HHI, are now included as priority under LIDDI, as shown in red. In contrast, in the low SEENI regions (Figure 2.13 (b)), cells that were ranked as high priority under HHI are now excluded from high LIDDI, as shown in blue.

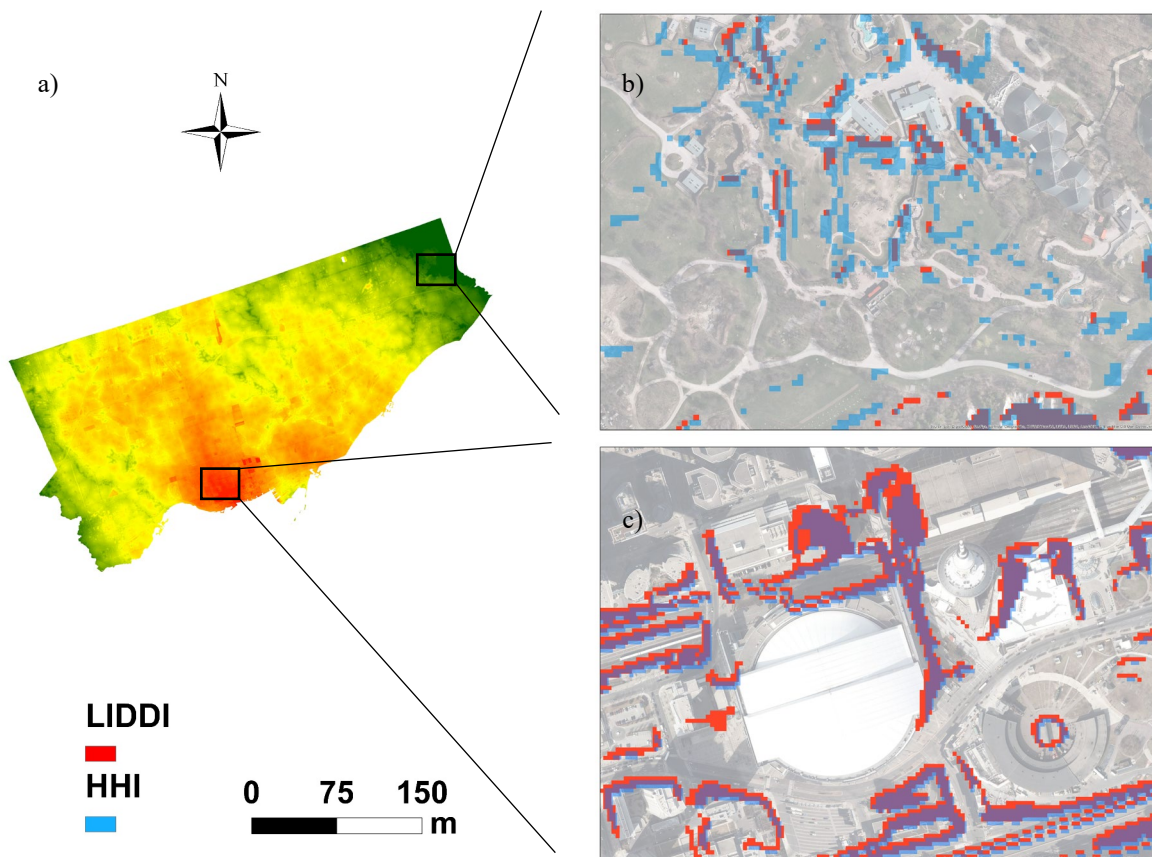


Figure 2.13 The effect of SEENI (a) on HHI and changing the priority of sites in LIDDI in two high and low SEENI areas, the area with low SEENI: Toronto Zoo area (b), area with high SEENI: the area around CN tower (c)

The LIDDI map allows visualization of the LID demand across a study area, which would otherwise be a complex geospatial problem. The results of this framework allow decision-makers to observe the main sources of flood with consideration of the socioeconomic and environmental factors using a physics based, robust, and easily implementable index, the HHI. The distribution of LIDDI across the study area helps visualize the need for LID in different regions in a large-scale study area. This visualization provides users with a simple expression of a complex and multi-criteria geospatial problem: it highlights the connections between the sources of runoff generation, flood prone areas, and areas that need higher socioeconomic and environmental benefits of LID. In addition, the LIDDI allows us to filter top ranked sites for implementing LID. Thus, with limited time and financial resources, presence of such a tool can save our resources while maximizing the earned benefits of LID.

2.6. CONCLUSIONS

In this research, a physical-based geospatial framework was developed to identify sites with the highest LID demand, in terms of their flood generation potential, along with socioeconomic and environmental factors. To develop this framework, hydrological-hydraulic, socioeconomic and environmental criteria were identified and generated using publicly available geospatial data. Through geospatial analysis and the SAW method within a hierarchical decision-making model, the variables were overlaid, resulting in three different indices: HHI, ENI and SEI. These indices rank the sites based on the demand or need for LID with respect to each index. By combining these indices, a LID demand index (LIDDI) was generated, which ranks the sites based on HHI, ENI and SEI and identifies locations where LID should be installed to meet the multiple

objectives (hydrological, environmental, and socioeconomic).

A heuristic equation was created to develop the hydrological-hydraulic index (HHI). To validate this equation and the generated HHI, we compared the results against a hydrological model (HEC-HMS) and historical flood-vulnerable locations within the study area.

The proposed framework was applied to the City of Toronto. The results showed that the framework for generating LIDDI has multiple advantages. It addresses the lack of a systematic geospatial allocation of LID methods and includes environmental and socioeconomic factors, in addition to the hydrological factors. This helps flood mitigation strategies in future land-use planning by allowing the decision-makers to rank the sites based on their demand for LID rather than using an ad hoc approach. Furthermore, this framework is specifically developed for LID objectives, unlike other existing models which are adapted from other objectives (e.g., water quality). Thus, many processes and benefits directly associated with LID are considered in the proposed framework. The three indices can also be used separately if only one aspect (hydrological, environmental, or socioeconomic) is needed. Moreover, publicly available data was used for the geospatial analysis, which allows for the wide use of our proposed framework. There is no limitation on the scale of the study area; modelling of a micro-scale, meso-scale and macro-scale study areas are all possible. Unlike previous studies where multiple mathematical limitations exist for the physical-based index (HHI), the proposed framework does not require modification or customization to use raw input data for this index. Thus, the actual values of all input data layers can be used as input data. Finally, the proposed framework is generalized to be applicable in any study area or region of interest. The proposed framework can be used to develop strategies for future flood risk attenuation, stormwater management, urban development and planning, retrofitting stormwater infrastructure, or to develop cost-effective development plans. In particular,

it supports spatial decision-making and flood risk reduction strategies and enhances the overall effectiveness of LID practices.

CHAPTER 3: THE EFFECT OF CLIMATE CHANGE AND URBANIZATION ON THE DEMAND FOR LOW IMPACT DEVELOPMENT FOR THREE CANADIAN CITIES

3.1. PREFACE

This chapter focuses on the second sub-objective, applying the hydrological-hydraulic index (HHI) proposed in Chapter 2 under climate change and urbanization. HHI is used to study the change in demand for LID under these future scenarios (12 combination of climate change and urbanization). The demand for LID is quantified, investigated, and contrasted for three Canadian cities (Toronto, Montreal, and Vancouver).

The content of this chapter was published in *Water*¹ in 2020 as follow:

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Contributions:

The contributions of authors in the current chapter are as follows, **Sarah Kaykhosravi**: has conducted the literature review, performed the data collection and curation, developed the method, used the required software to perform the analysis and modelling, validated and visualized the results, and have prepared and wrote the original manuscript of this publication. **Usman Khan** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript. **Mojgan A. Jadidi** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript.

3.2. ABSTRACT

Climate change and urbanization are increasing the intensity and frequency of floods in urban areas. Low Impact Development (LID) is a technique which attenuates runoff and manages urban flooding. However, the impact of climate change and urbanization on the demand or need for LID in cities for both current and future conditions is not known. The primary goal of this research was to evaluate the demand for LID under different climate change and urban growth scenarios based on a physical-based geospatial framework called the hydrological-hydraulic index (HHI). To do this, 12 scenarios considering four climate change and three urbanization conditions

were developed. The HHI for three cities in Canada (Toronto, Montreal, and Vancouver) were estimated, evaluated, and compared for these scenarios. The results show that both urbanization and climate change increase the demand for LID. The contribution of climate change and urbanization on LID demand, measured using HHI, varies for each city: in Toronto and Montreal, high rainfall intensity and low permeability mean that climate change is dominant, whereas, in Vancouver, both climate change and urbanization have a similar impact on LID demand. Toronto and Montreal also have a higher overall demand for LID and the rate of increase in demand is higher over the study period. The results of this study provide us with a comprehensive understanding of the effect of climate and urbanization on the demand for LID, which can be used for flood management, urban planning, and sustainable development of cities.

3.3. INTRODUCTION

Floods are a major growing natural hazard that causes the loss of human lives and properties. The proportion of flood occurrence was the highest of all types of natural disasters from 1995 to 2015 [11]. The frequency of flooding has increased during the last two decades (1995 to 2015) [9]. During the same period, floods caused 157,000 fatalities globally (accounting for 26 % of all weather-related disasters). In addition, it affected the quality of life of 2.3 billion people, which is the highest share (56 %) among weather-related disasters [11]. In terms of economic losses, based on UNISDR (2016), between 2006 and 2016, the average annual costs associated with flooding were about 50 billion USD. This ranks first among the natural disasters. These damages include all types of regions (i.e., land uses) including urban areas [12].

There exist several key drivers of urban flood risk such as urbanization, urban sprawl,

increasingly unresponsive engineering, global climate change, and fluvial and pluvial changes [151]. Urbanization causes changes to terrains, slopes, soil type, and vegetative cover, which result in a change in the hydrologic behaviour of urbanized areas [1]. Among these changes, the expansion of impervious surfaces dramatically increases the volume of surface runoff [2]–[5]. The expansion of impervious surfaces can occur in two contexts: (1) within a constant area (by an increase of the imperviousness densification within a fixed area); and (2) by increasing the area of the city (expansion of impervious area). However, in our research, we only considered the first context. On the other hand, due to a higher population density and valuable properties in urban areas, the influence of floods on these environments is intensive and excessively costly. Thus, urban areas are more vulnerable to the effect of floods, and, by the growth of the urban population, therefore, vulnerability and exposure are also significantly higher [9]. Climate change and the increase of rainfall intensity have also increased flood risk associated with the frequency of the occurrence of the flood [9], and this trend is expected to continue in many regions.

To cope with this, the traditional and most common approach is using a stormwater collection network (SCN). The objective of SCN is to collect and rapidly convey surface runoff to a predetermined outfall (e.g., receiving water bodies such as rivers, lakes, or ponds) [66]. However, several issues are associated with SCN. SCN is designed for a specific rainfall event; thus, there is an evident limitation of the capacity to manage extreme flood events which are likely due to climate change. This issue is exacerbated by the fact that existing SCNs are aging and performing at a lower capacity. Besides, SCN collects polluted runoff from urban surfaces, which causes environmental damages and financial losses. These losses are either due to contamination of receiving waters or treating the collected runoff at stormwater treatment plants. Even though using SCN is a well-known and well-documented method [67], [68], it has several issues, which

necessitate a different approach to managing runoff in urban areas.

The smart and sustainable urban growth approach commonly known as Low Impact Development (LID) is an innovative solution to complement SCN, which is increasingly being adopted in cities around the world [21], [22], [24], [25], [65]. LID can be incorporated with existing SCN to increase the capacity of the SCN and, thus, improve their performance. LID allows for reducing the risk of floods by reducing urban runoff [21], [25], [29], [57], [93], [94], [101]. This is achieved by reducing imperviousness, conserving natural resources and ecosystems, maintaining natural drainage courses, reducing the use of pipes, and minimizing clearing and grading during the development process. Structural techniques such as bioretention cells, rain gardens, green roofs, and permeable pavements are also used to increase infiltration, thereby decreasing the amount of runoff and delaying the time to peak [28], [65], [92].

Demand for LID in different locations varies based on different factors such as land cover type, topography, etc. [86], [100], [152]. From a hydrological-hydraulic point of view, this demand is associated with the extent of the runoff generated in each site. That is, the higher is the generated runoff, the higher is the demand for capturing the runoff at the source (the site) [101], [152]. The change in rainfall intensity and depth (caused by climate change) and land cover type (caused by urbanization) are the two main factors that affect the extent of this demand. In a specific site, if the rainfall or the land cover changes, the demand for LID will change accordingly [152]. This is due to the change in the volume of runoff generated at that site, which is a function of both climate and land cover.

At the city-scale additional complexity is introduced due to numerous LID sites, constant urban change (and growth), global climate change, and the non-uniform spatial distribution of land cover and rainfall [9], [153]–[157]. Thus, it is extremely important to be able to quantify this

complexity to attain insight into how changes in climate and urban land cover influence the demand for LID. Such information is useful for urban planning, designing multifunctional urban infrastructure, policymaking regarding urban growth, and the optimal assignment of financial resources for runoff and flood risk management. Therefore, the objective of our study was to investigate the effect of climate change and urbanization on the demand for LID.

The results of such an investigation will provide us with an insight into the effect of climate and urbanization on the demand for LID. This article holistically covers the scenarios under which either only one change takes place (i.e., climate or urbanization) or both (i.e., climate and urbanization), and discusses the causes and effects of the future demand for LID for three selected Canadian cities. It also discusses the contribution of climate change and urbanization factors on the change of hydrological and hydraulic processes. The manuscript is organized as follows. Section 3.4 presents the methods including the study area, the geospatial data, and the development of climate change and urban growth scenarios. Sections 3.5 and 3.6 include the results and discussion, respectively, followed with the conclusion in Section 3.7.

3.4. METHODS

In our study, we used a physical-based geospatial index called the hydrological-hydraulic index (HHI) [152]. We estimated HHI for three Canadian cities (Toronto, Montreal, and Vancouver) using the approach proposed Kaykhosravi et al. [25]. The HHI was generated for these cities under various climate and urbanization scenarios. For urbanization, we developed different land cover scenarios to represent different degrees of future urbanization, by modifying existing pervious areas to impervious areas. For the climate change scenarios, we created spatial rainfall

distribution maps based on the projected Intensity–Duration–Frequency (IDF) curves for each city. These maps included historical data as well as three future climate change scenarios. The urbanization and climate change scenarios were integrated and used to estimate, evaluate, and compare the HHI (a measure of LID demand [152]) for each city.

3.4.1. Description of the Three Canadian Cities

The study area in this research includes three metropolitan Canadian cities: Toronto, Montreal, and Vancouver. The location of all cities and their administrative border are presented in Figure 3.1. The figure illustrates the current status of land cover in all cities, categorized into three classes: impervious lands, pervious lands, and water bodies.

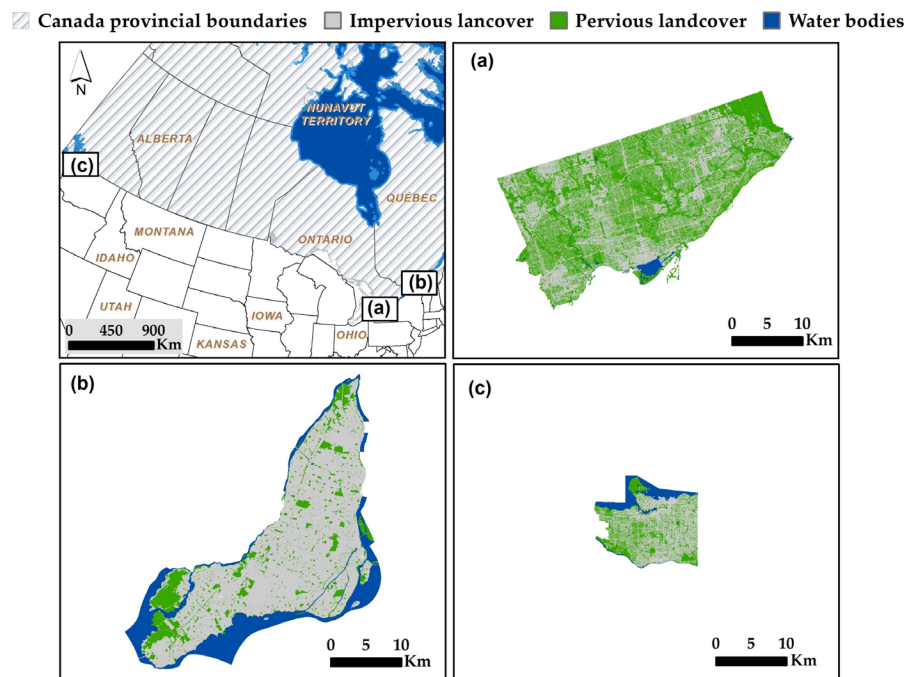


Figure 3.1 The location of the three case-study cities within Canada showing three land cover categories: (a) Toronto; (b) Montreal; and (c) Vancouver.

The area of Toronto is 633.5 km² and the population of the city in 2019 was 2.96 million [158]. The average annual precipitation of Toronto for the 1951–1980 period is 814 mm [159] which is the lowest precipitation among the three cities. The pervious to impervious ratio (PIR) (ratio of areas excluding water bodies) is about 1.17 based on the available land cover data (from 2007) meaning that land cover in Toronto is dominated by pervious land cover.

The area of Montreal is 624.4 km², slightly lower than Toronto, and the population of the city in 2016 (based on the most recent census data) is 1.96 million [160]. The average annual precipitation for the 1951–1980 period is 1028 mm [159], which is slightly higher than in Toronto. The PIR for Montreal is 0.21 which is the lowest among all three cities, meaning that the city is highly urbanized or, in other words, dominated by impervious land cover.

Vancouver area is 136.5 km² and the population of the city in 2016 (based on the most recent census year) is 2.55 million [161]. The average annual precipitation for the 1951–1980 period is 1569 mm [159], which shows the city has the highest precipitation depth among the three cities. The PIR for Vancouver according to the available land cover (from 2014) is 0.64, which is higher than Montreal but lower than Toronto. In addition, this indicates that the land cover of Vancouver is largely dominated by impervious land cover.

3.4.2. Geospatial Data Used for Generating the HHI

Our analysis in this study was conducted based on geospatial analysis. The HHI model was developed using Python and the ArcPy package was used to perform the analysis. The data used to estimate HHI included:

- Meteorological station data: To estimate rainfall intensity

- Surficial geology: To estimate the depth to restrictive layer and the hydraulic conductivity
- Groundwater tables: To estimate the depth to groundwater
- Digital Elevation Model (DEM) data: To estimate the slope

All geospatial data used in this study are publicly available and were downloaded from various open data sources [162]–[168]. All datasets were converted into raster format with a ground resolution of 5 m × 5 m (to align with the digital elevation model of Toronto). This resolution was used as the reference resolution for this research.

The raster maps that were derived from these data were overlaid using Equation 4.1 [152] to generate the HHI. HHI ranks the cells (i.e., the pixels of the raster data) by their runoff generation potential. Thus, cells with higher HHI generate higher volume and peak runoff flow rate. Ranking the cells based on HHI values highlights the cells that are the main source of runoff generation. On this basis, we can target the high HHI cells for LID implementation, and thereby effectively maximize runoff reduction [152]. Since the demand for implementation of LID corresponds to the HHI values, site with higher HHI values are considered as sites with higher demand for LID [152]. The HHI index accounts for seven variables, as presented in Eq. 3.1.

$$HHI_j = \begin{cases} \left[R_j - ((K_s)_j \cap (K_i)_j) \cap \left(n_j \times \frac{((D_g)_j \cap (D_r)_j)}{0} \right) \right] \times [1 + (\tan S)^{0.385}] & \text{for } R_j > K_s_j \\ 0 & \text{for } R_j \leq K_s_j \end{cases} \quad (\text{Eq. 3.1})$$

In Equation 4.1, j is the cell number; HHI_j is HHI at cell j ; R_j is rainfall intensity (mm/h) at cell j ; $(K_s)_j$ is saturated hydraulic conductivity of the surficial soil (mm/h) at cell j ; $(K_i)_j$ is the hydraulic conductivity of impervious areas (e.g., roads, parking lots, and building rooftops) at cell j , which is set equal to zero for impervious cells; n_j is the soil porosity at cell j ; $(D_g)_j$ and $(D_r)_j$ are,

respectively, depth to groundwater (mm) and depth to the first restrictive soil layer (mm) at cell j ; and S is the terrain slope (degrees) at cell j [152].

3.4.3. Developing Scenarios for Investigating the Integrated Effect of Climate Change and Urbanization

Climate Change Scenarios

The pattern of the effective rainfall (rainfall with losses deducted) can have a significant influence on the runoff hydrograph [169]. The pattern is typically determined by selecting the position of the maximum rainfall block (in the hyetograph) and rainfall duration [170]. For hydrological modelling of a catchment, it is important to determine the duration of the rainfall to which flood generation is assumed to occur [171]. Generally, for catchments above 40 km², the effective daily rainfall duration is in the order of 12 h (with the time of concentration between 4 and 12 h); for catchments larger than 500 km², or slow-reacting catchments, a sub-daily distribution is not needed. Smaller catchments are reactive to short but intensive rainfall events in producing their highest peaks [171]. For example, the recommended duration is 10 min inlet time for small (micro-scale) catchments, whereas the actual time of concentration should be used for larger-scale catchments, according to the Wet Weather Flow Management Guidelines for Toronto [172]. In this study, the catchments were generally small and, therefore, shorter durations (less than the time of concentration) were used for the analysis. However, due to the lack of such fine resolution data for all three cities, a duration of 60 min was used for effective rainfall for each city for the HHI analysis. In addition, a 10-year return period (RP) was selected because this is the most extreme scenario suggested by Canadian guidelines for the design of small wet weather

systems including LID. The RPs suggested by these guidelines include 2 [172]–[174], 5 [173], or 10-year [172], [175].

For the projected IDF data, we used the IDF_CC Tool 4.0 (Computerized Tool for the Development of Intensity-Duration-Frequency Curves under Climate Change—Version 4.0) [176]. The available range of IDF data available through this tool are the years 2006–2100. Generating IDF curves based on stationary historical data cannot capture the changing climate conditions; thus, this tool uses two other models: Global Climate Models (GCMs) and Regional Climate Models (RCMs) [177]. Both GCMs and RCMs need spatial and temporal downscaling, which relies on the historically observed data for the time-period of observations [177]. Downscaling links GCM/RCM grid scales and local study areas for the generation of IDF curves under changing climate conditions. For temporal downscaling of precipitation data, a modified version of the equidistant quantile-matching (EQM) method is used in this tool. For spatial downscaling, the tool utilizes a statistical downscaling method. The first future climate that this tool provides is for the period 2006–2036 (referred to as Scenario 2036 in this study), which was selected as our first future scenario [178]. In addition, projections for the period 2036–2066 (referred to as Scenario 2066 in this study) as the mid-term scenario and the period 2066–2096 (referred to as Scenario 2096 in this study) for the long-term period were also selected. Data from the Canadian Climate Model (CanESM 2) were selected from among several available climate models within the tool. The tool generates the IDF for three different values of the Representative Concentration Pathways (RCP) [179] including RCP2.6, RCP4.5, and RCP8.5. The comparison of IDF for these three RCPs for various RPs (2, 5, 10, 25, 50, and 100) provided by the tool shows that the lower the RP the smaller is the difference between IDFs with different RCPs [176]. Thus, for the RPs of 2–10 years, the difference between IDF for different RCPs is almost negligible.

Thus, we selected the 10-year RP and the highest RCP (8.5 W/m²) to derive the projected IDF values for the selected scenarios (2036, 2066, and 2096).

Following the derivation of rainfall intensity using the IDF_CC Tool 4.0 at each meteorological station within or near the cities, the geospatial distribution of rainfall across each city was estimated using the stations listed in Tables 4.1–3 for each city. This process was as follows: First, using the IDF tables, the rainfall intensities for the 10-year RP and 60 min duration were derived. Second, a geospatial analysis (using Inverse Distance Weighted method, IDW) was used to develop the distribution of the rainfall intensity across the study areas based on the location of the stations. This resulted in 12 different rainfall distribution maps (four for each city for the selected years including historical IDF and projected IDF for Scenarios 2036, 2066, and 2096).

Table 3.1 Projected rainfall intensity for Toronto for Scenarios 2036, 2066, and 2096 [176], [180], 60 min duration, and 10-year RP. The coordinates are in NAD_1983_UTM_Zone_17N.

ID	Station Name	Historical Data Range	Coordinates		Rainfall Intensity (mm/h)			
			X (m)	Y (m)	Historical	2036	2066	2096
1	Oshawa WPCP	1970–2006	674,358.9	4,859,722	32.17	35.00	35.45	42.12
2	Toronto City	1940–2007	628,988.2	4,836,464	39.12	43.54	43.59	49.43
3	Toronto-INTL A	1950–2017	610,427.6	4,837,243	38.12	42.06	42.99	47.39
4	Toronto Buttonville A	1986–2007	630,991.4	4,857,614	37.50	39.56	39.94	45.49
5	Oakville Southeast	1965–1976	610,793.8	4,815,031	32.33	35.70	36.48	40.10
6	Etobicoke	1964–1980	618,586.5	4,831,829	36.05	39.77	40.09	45.12
7	Toronto Met Res Stn	1966–1987	616,643.0	4,850,681	36.91	40.62	41.62	45.96

Table 3.2 Projected rainfall intensity for Montreal for Scenarios 2036, 2066, and 2096, 60 min duration [176] , and 10-year RP. The coordinates are in NAD_1983_UTM_Zone_18N.

ID	Station Name	Historical Data Range	Coordinates		Rainfall Intensity (mm/h)			
			X (m)	Y (m)	Historical	2036	2066	2096
1	McGill	1906–1992	609,377.	5,039,448	42.20	45.7	55.4	55.7
			3			0	5	0
2	Mirabel Int. A.	1976–2008	575,554.	5,057,840	32.41	33.7	40.9	41.5
			5			0	3	8
3	P. E. T. Int. A.	1943–2014	598,491.	5,035,934	34.90	36.6	45.3	45.6
			9			6	7	6
4	St Hubert A.	1956–1995	623,396.	5,041,931	34.60	36.4	44.9	44.8
			3			2	9	1
5	Jean Brebeuf	1969–1984	609,377.	5,039,448	32.50	33.9	41.7	42.1
			3			1	0	4
6	Lafontaine	1973–1991	609,338.	5,041,670	32.35	33.4	41.6	41.9
			6			6	3	9
7	Jar Bot	1977–1989	613,143.	5,047,295	39.35	39.5	50.8	49.6
			1			4	0	4
8	Valleyfield	1986–1998	570,587.	5,014,450	32.61	34.9	41.2	41.6
			7			9	0	2
9	L'Assomption	1963–2017	621,983.	5,074,136	36.28	38.2	47.4	47.4
			8			9	4	3

Table 3.3 Projected rainfall intensity for Vancouver for Scenarios 2036, 2066, and 2096 [176], [181], 60 min duration, and 10-year RP. The coordinates are in NAD_1983_UTM_Zone_10N.

ID	Station Name	Historical Data Range	Coordinates		Rainfall Intensity (mm/h)			
			X (m)	Y (m)	Historical	2036	2066	2096
1	UBC	1958–1990	481,806.1	5,455,27	14.35	14.9	15.6	16.8
			0	6		8	0	4
2	Lynn Creek	1964–1983	497,822.0	5,468,58	19.89	21.0	21.9	23.6
			0	7		5	4	5
3	Ladner Bchpa	1963–1978	503,651.3	5,436,34	11.02	11.6	11.9	13.0
			0	9		8	9	4
4	Surrey Kwantlen Park	1962–1999	510,200.9	5,448,58	15.79	16.5	17.2	18.5
			0	6		9	7	3
5	Buntzen Lake	1969–1983	509,436.0	5,469,70	21.30	22.3	23.4	25.0
			0	7		5	3	3

Urban Growth Scenarios

The projected land cover of each city was required to investigate the influence of future urbanization on runoff generation potential. To develop these projected scenarios, there were

several limitations due to inconsistent and/or complete lack of data for the study periods. To account for the inconsistencies in the land cover categories, we generalized the land covers into three categories: impervious (buildings, roads, parking lots, and other paved surfaces), pervious (tree canopies, parks, golfs, grass shrubs, bare earth, etc.), and water body (lakes, ponds, streams, etc.). For example, in Toronto, all trees (street, park, and forest trees) are considered as one category (tree canopy), whereas, in other two cities, trees are not distinguished from other green spaces, and are part of open spaces or park areas. Thus, due to this inconsistency, comparing the land covers directly for each city is not feasible. Tables 4.4–6 illustrate these differences for each city. These tables show 8 categories of land cover for Toronto and Montreal and 13 for Vancouver, each with a different taxonomy.

Another limitation was that the future urban growth data (which were used to estimate future urbanization) for the selected years were not available. To address this, we used a systematic urban growth model to generate this data. In the proposed model, we estimated the future state of cells (i.e., locations within each city). Our model is a grid-based discretization method [182] which is different from conventional urban growth models such as cellular automata (CA), land use/transportation (LUT), or agent-based (ABM) models [183]. The selection and priority of the “converted lands” were made based on a combination of three parameters including the hydrological state of the lands (pervious or impervious) considering the land cover (i.e., pervious lands such as bare earth were selected for conversion); the functional importance of the land cover (e.g., tree canopy had priority to bare earth for conversion to impervious cover); and finally the total geometrical area of the selected land cover (e.g., tree canopy in Toronto has a significant share in the area of the city which is greater than the area of all other pervious lands such as grass shrubs, bare earth, etc.). We divided the conversion process into two steps. In Step 1 (Scenario 1,

representing medium urbanization), a few land covers are converted to impervious surfaces, whereas in Step 2 (Scenario 2, representing high urbanization) more land covers follow (shown red colored text in Tables 4.4–6). Subsequently, the corresponding area of conversions is calculated, leading to different values for different cities. The PIR values for all three cities and scenarios are presented in Tables 4.4–6. Overall, as expected, PIR decreases with urbanization in all cities.

For Toronto, the impervious area increased by 28 % and 48 % for Scenarios 1 and 2, respectively. For Montreal, the impervious area increased by 5 % and 10 % for Scenarios 1 and 2, respectively. Lastly, for Vancouver, the impervious area increased by 19 % and 48 % for Scenarios 1 and 2, respectively. In each of these cases, the increase in impervious area is measured by comparison with the base scenario for each city. The difference among the “added impervious areas” of the cities for the same scenario is due to two reasons: (1) the limited capacity of the cities in terms of available pervious land cover; and (2) the inconsistency in the base maps in terms of the types of land cover (as described above). This limited the consistent conversion for the same scenario for all cities. For example, “grass shrub” in Toronto does not have a similar land cover type in Montreal (“Golf” can be considered a similar class), whereas “shrub”, “modified grass herb”, or “natural grass herb” can be considered as similar cover types in Vancouver.

In the highly urbanized state (Scenario 2), the PIR is 0.47, 0.10, and 0.11 for Toronto, Montreal, and Vancouver, respectively. These ratios reveal how far the cities are from the highly urbanized state. Both Montreal and Vancouver have similar PIR values for the most critical condition (i.e., Scenario 2) with the lowest pervious land cover, whereas Toronto has a significantly high proportion of pervious land cover. Overall, in Scenario 2, in all three cities, the area of impervious lands dominates the pervious area.

Table 3.4 Land cover data of Toronto at the year 2007 and its projected changes due to the urban growth for two scenarios.

ID	Land Cover	Area (km ²)	Base	Scenario 1	Scenario 2
1	Buildings	103	impervious	impervious	impervious
2	Roads	79.8	impervious	impervious	impervious
3	Paved surfaces	108	impervious	impervious	impervious
4	Tree canopy	179.2	pervious	pervious	impervious
5	Grass shrub	149.4	pervious	impervious	impervious
6	Agriculture	6.2	pervious	impervious	impervious
7	Bare earth	4.1	pervious	impervious	impervious
8	Water bodies	3.8	-	-	-
	Total	633.5			
	Added impervious		0	82.4 ¹	139 ¹
	Total impervious		290.7	373.1	429.7
	Total pervious		338.9	256.6	200.4
	PIR		1.17	0.69	0.47

¹ Pervious lands within a buffer of 500 m from the streams were not converted to impervious.

Table 3.5 Land cover data of Montreal at the year 2016 and its projected changes due to the urban growth for two scenarios.

ID	Land Cover	Area (ha)	Base	Scenario 1	Scenario 2
1	Buildings	264.6	impervious	impervious	impervious
2	Roads	103.5	impervious	impervious	impervious
3	Paved surfaces	47	impervious	impervious	impervious
4	Parks and open spaces	41.1	pervious	pervious	impervious
5	Golf	12.5	pervious	impervious	impervious
6	Agriculture	6.1	pervious	impervious	impervious
7	Bare earth	25.3	pervious	impervious	impervious
8	Water bodies	124.5	-	-	-
	Total	624.6			
	Added impervious		0	19.5 ¹	41.1 ¹
	Total impervious		415.1	434.6	456.2
	Total pervious		85.1	65.3	43.8
	PIR		0.21	0.15	0.10

¹ Pervious lands within a buffer of 500 m from the streams were not converted to impervious.

Table 3.6 Land cover data of Vancouver at the year 2014 [184] and its projected changes due to the urban growth for Scenario 1.

ID	Land Cover	Area (ha)	Base	Scenario 1	Scenario 2
1	Buildings	37.5	impervious	impervious	impervious
2	Other Built	0.1	impervious	impervious	impervious
3	Paved	33.3	impervious	impervious	impervious
4	Coniferous	6	pervious	pervious	impervious
5	Deciduous	21.8	pervious	pervious	impervious
6	Barren	1.9	pervious	pervious	impervious
7	Shrub	0.7	pervious	impervious	impervious
8	Shadow (considered as shrub)	1.5	pervious	pervious	impervious
9	Modified Grass-herb	13	pervious	impervious	impervious
10	Natural Grass-herb	0.2	pervious	impervious	impervious
11	Non-photosynthetic vegetation	0.1	pervious	pervious	impervious
12	Soil	0.3	pervious	pervious	impervious
13	Water	20.1	-	-	-
Total			136.5		
Added impervious			0	13.8	34.3 ¹
Total impervious			71	84.8	105.3
Total pervious			45.4	31.6	11.1
PIR			0.64	0.37	0.11

¹ Pervious lands within a buffer of 500 m from the streams were not converted to impervious.

To verify that the urban growth scenarios do not overestimate future urban areas, the computed scenarios described above were compared to a population-based metric. This metric denoted as the Additional Required Impervious Lands (ARIL) is presented in Eqs. 4.2 and 4.3. ARIL estimates how much impervious area is needed on top of the base land cover (i.e., current conditions) to accommodate the projected population in the future. To calculate ARIL, a linear relationship between population growth and impervious area (km²) was assumed using similar methods proposed in previous studies (e.g., [185], [186]). In addition, we assumed that the distribution of population over impervious lands is homogenous, the population density in the future remains the same, and the future area of impervious lands is a linear function of the current area and population density. In other words, future urbanization and urban growth will continue in the future as they are currently.

$$\text{PPI (capita/ha)} = P_{\text{base}} (\text{capita}) / A_{\text{ibase}} (\text{km}^2) \quad (\text{Eq. 3.2})$$

$$\text{ARIL} = (P_x - P_{\text{base}}) / \text{PPI} \quad (\text{Eq. 3.3})$$

where A_{ibase} is the area of impervious lands at the base year, P_x is the projected population at year x , P_{base} is the population at year b , and PPI is the population per impervious land (Eq. 3.2).

The projected populations for Toronto, Montreal, and Vancouver are needed to estimate the ARIL (Table 3.8). The available data for these projections for each city had several inconsistencies creating a challenge in data integration, particularly due to missing data for the three future periods. To overcome this, the missing data were estimated using a linear function to the available data (which included historical population data for each city as well as projected data for certain future years), for each city. The project data are specified in Table 3.7, which also identifies which data were estimated using the linear function.

Table 3.7 The projected population for Toronto, Montreal, and Vancouver scenarios 2036, 2066, and 2096 [158], [160], [161].

		Scenario			
		Base	2036	2066	2096
Population (million)	Toronto	2.40 ² (year 2007)	3.81 ¹	5.10 ²	6.47 ²
	Montreal	1.96 ³ (year 2016)	2.27 ¹	2.70 ²	3.14 ²
	Vancouver	2.42 ³ (year 2014)	3.40 ¹	4.35 ²	5.47 ²

¹ Based on projected data. ² Estimated using a linear function. ³ Based on available historical data.

Based on Equations 4.2 and 4.3, PPI in 2007 (the base year) for Toronto is estimated as 8255.9 capita/km². For Montreal, the PPI calculated in the year 2016, for which both population and land cover data are available, was estimated as 5159.8 capita/km². Vancouver had a PPI of 34,084.5 capita/km² in year 2016, for which both population and land cover data are available. Using PPI values, the ARIL of each city for all projected years were estimated and are presented

in Table 3.8. We compared the ARIL against the developed scenarios. This revealed that the added impervious lands (by converting pervious lands) in two scenarios are not adequate to accommodate the projected population with an assumption of constant PPI. In all cases, the ARILs in Scenarios 2066 and 2096 are larger than the added impervious area presented in Tables 4.4–6. From this, we learned that for the future land cover scenarios, only converting the pervious to impervious lands is not sufficient to accommodate such projected populations and the PPI needs to increase. In other words, the current lifestyles will need to be modified in each city to account for the increase in population, e.g., through the vertical development of buildings (i.e., densification) or an increase in population density.

Table 3.8 Land cover data of Toronto, Montreal, and Vancouver on the base year (2007, 2016, and 2014, respectively for each city) and its projected changes due to the urban growth in the years 2030, 2066, and 2096.

		Base	2036	2066	2096
Toronto	ARIL (km ²)	0.0	170.8	327.2	493.1
	Total impervious (km ²)	290.7	461.5	788.6	1281.7
	Total pervious area (km ²)	338.9	168.1	-159.0	-652.1
Montreal	ARIL (km ²)	0	60.08	143.61	228.89
	Total impervious (km ²)	379.8	439.94	583.55	812.44
	Total pervious area (km ²)	120.1	60	-84	-312
Vancouver	ARIL (km ²)	0	28.75	56.62	89.51
	Total impervious (km ²)	71	99.75	156.38	245.89
	Total pervious area (km ²)	45.4	17	-40	-129

Integrated Urban Growth and Climate Change Scenarios

We investigated all possible combinations of our selected urbanization and climate change scenarios. Using this, the influence of the sole change of any scenario as well as the combined change of any land cover and climate scenarios can be analyzed. The developed scenarios are

labeled and presented in Table 3.9.

Table 3.9 The 12 combinations of climate change and urbanization scenarios.

		Climate Change			
		Base Year	Sc 2036	Sc 2066	Sc 2096
Urbanization Scenarios	Sc00 (base land cover)	C-base-00	C-2036-00	C-2066-00	C-2096-00
	Sc01 (medium urbanized)	C-base-01	C-2036-01	C-2066-01	C-2096-01
	Sc02 (highly urbanized)	C-base-02	C-2036-02	C-2066-02	C-2096-02

3.5. RESULTS

A brief comparison of climate condition and urbanization under different scenarios is presented in Figure 3.2 and Figure 3.3. The mean rainfall intensity of the cities shows that the rainfall intensity of Toronto is slightly higher than that of Montreal and more than double the rainfall intensity of Vancouver. However, Vancouver has a maximum average annual rainfall of 1569 mm, about 90 % higher than Toronto and 50 % higher than Montreal. Overall, the trend of projected mean rainfall intensity presents an increase in the intensity of rainfall in the future for each city for each future period. However, there is an exception for Toronto in Scenario 2066, where the intensity is shown to remain almost constant compared to the previous scenario (2036). This is similar to Montreal for Scenario 2096 compared to the previous scenario (2066). Note that the variability of rainfall intensity is higher in Montreal compared to the other two cities.

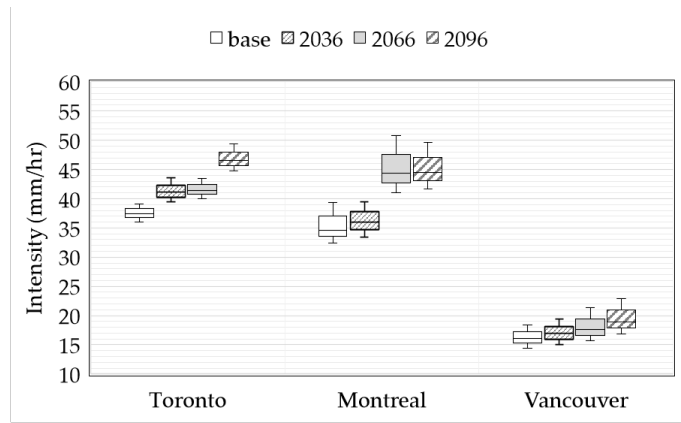


Figure 3.2 Comparison of rainfall intensity (for the 60 min duration and 10-year RP event) for the three cities in selected years.

Figure 3.3 presents an overall comparison of all urbanization scenarios for the three cities. If zero impervious surface is defined as the “green city”, Figure 3.3 shows that Toronto (for the base scenario) is the closest to the “green city” and Montreal is the most urbanized city (closest to 100 % impervious cover). As expected, the two projected scenarios (Sc1 and Sc2 representing medium and high urbanization) move each city further away from the “green city”.

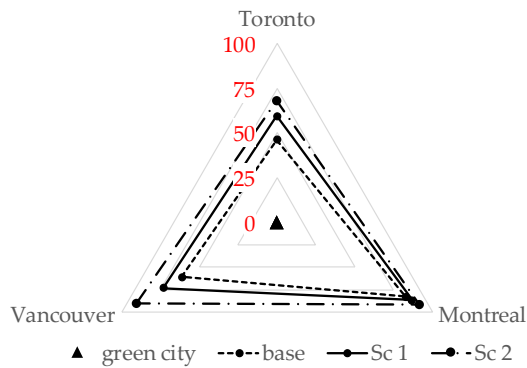


Figure 3.3 Normalized ratio of impervious area to the city area (water bodies excluded) for Toronto, Montreal, and Vancouver.

For the HHI, first, a general comparison of the three cities is presented in Figure 3.4 which

shows the current state (C-base-00, i.e., the base climate and the base urbanization scenarios) as well as the worst-case scenario (C-2096-02, i.e., Scenario 2096 climate and high urbanization, Scenario 2). Note that, as identified above, the C-base-00 comparison has some limitations: the base land cover for these cities is not for the same year, while the rainfall intensity is based on available historical data (which differs for each city).

This comparison was made based on the mean and frequency of HHI in each city. Figure 3.4 shows the normalized histogram of HHI for each city for the two scenarios listed above; a low HHI value represents a lower demand for LID, and a higher value represents a higher demand. Generally, there is a higher demand for LID in Montreal, with a slight difference compared to Toronto, and Vancouver has the lowest demand for LID. The mean HHI values for the C-base-00 and C-2096-02 scenarios range from 46.2 to 58.2 (a 26 % increase) for Toronto, from 44.0 to 56.4 (a 28.2 % increase) for Montreal, and from 21.3 to 25.1 (a 17.8 % increase) for Vancouver.

Toronto and Montreal present a similar pattern in response to climate change and urbanization. For example, in both cities, a significant proportion of the C-2096-02 histograms is higher than an HHI value of 50, which shows a higher demand for LID compared with the C-base-00 scenarios. In addition, there is a general change towards a higher frequency of HHI for the C-2096-02 from the C-base-00 scenario. In Vancouver, if an HHI value of 25 is used for comparison, the histogram does not show that the proportion of the C-2096-02 histogram for values greater than 25 has changed. Both the initial and final HHI values for Vancouver are much lower than both Toronto and Montreal. The C-2096-02 demand is higher, as expected, for Vancouver, but with lower variance than the C-base-00 scenario.

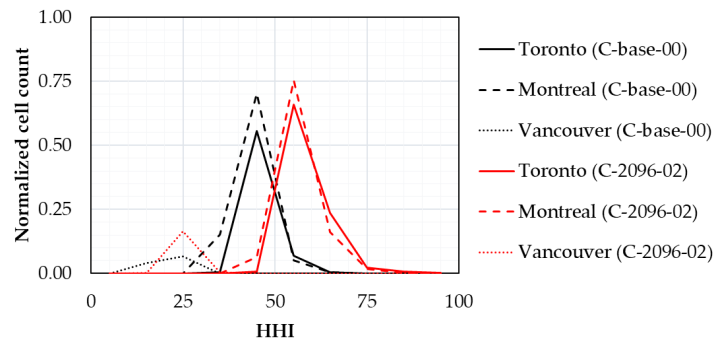


Figure 3.4 Normalized (to the maximum overall cell count of the three cities) histogram of HHI of comparing the current state (C-base-00) and the worst-case scenario (C-2096-02) among Toronto, Montreal, and Vancouver.

The HHI values for all three cities are visualized in maps presented in Figure 3.5–7. As expected, all scenario results indicate that climate change and urbanization increase the HHI and, thus, the runoff generation potential in each city, leading to a higher demand for LID for source control. Climate change also significantly impacts HHI more than urbanization in Toronto and Montreal. This can be due to two reasons: first, Montreal is already highly urbanized and, thus, the room for future change in land cover is limited; and, second, while Toronto has a high share of pervious land cover, most of the natural soil has low permeability (clayey silt till or silty clay to silt till [187]), thus increasing the HHI further. Therefore, considering the current state of the land cover of these cities, urbanization has a lower effect than the change in the magnitude of rainfall intensity. Vancouver (results are shown in Figure 3.7) responded to the integrated climate change and urbanization similarly to the other two cities (an increase of HHI), but with lower values of HHI overall. The difference between the sole effect of urbanization and climate change in this city was not as significant as the other two cities. This is because Vancouver has a lower rainfall intensity compared to the other two cities, so the HHI value is about half the values for Toronto

and Montreal, which decreases the effect of climate change. Note that Vancouver is more pervious compared to the other two cities, thus it has more room for urbanization (Figure 3.3).

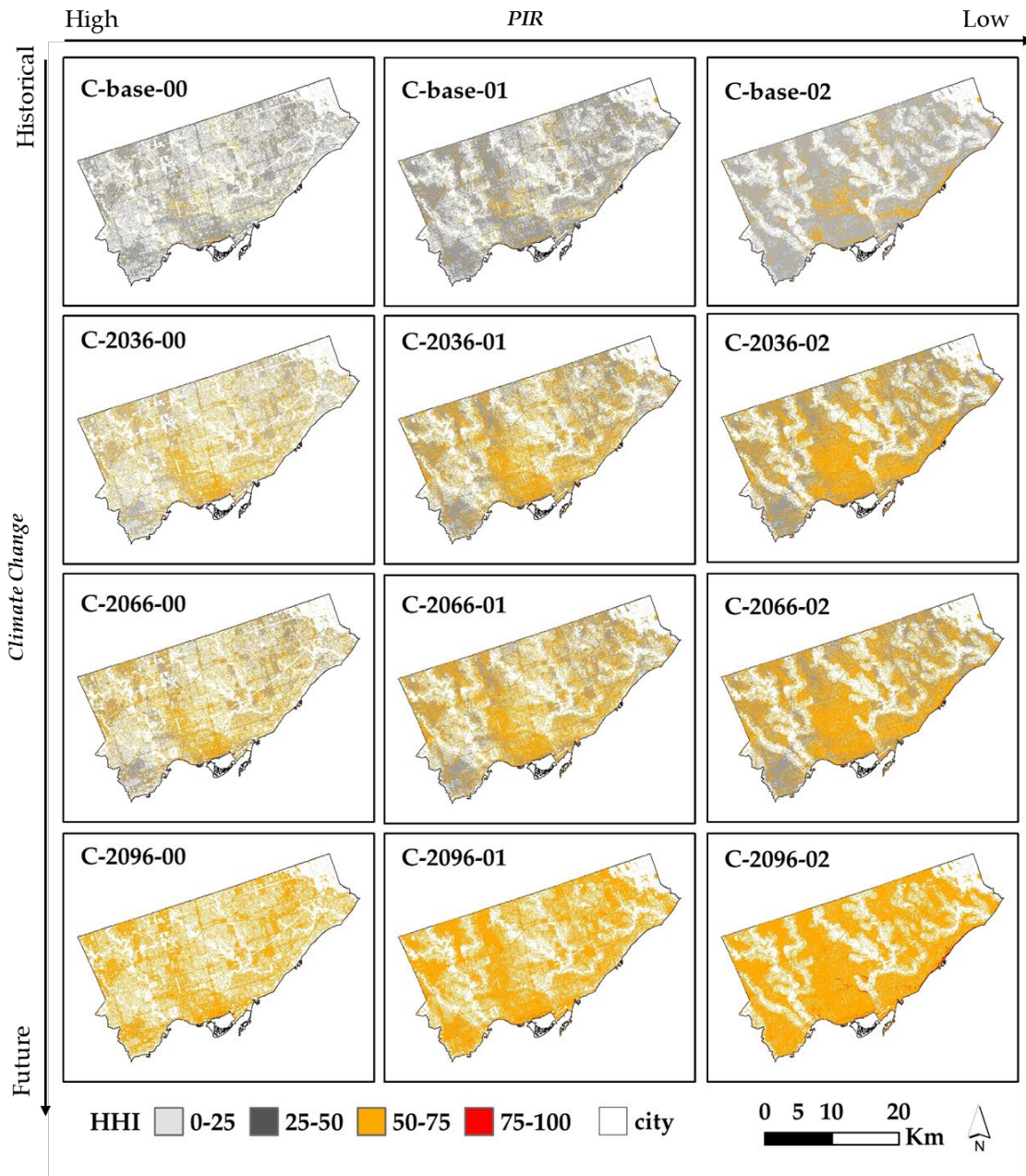


Figure 3.5 The HHI maps for Toronto under different climate (base year, 2036, 2066, and 2096) and land cover scenarios (base, Scenario 1, and Scenario 2).

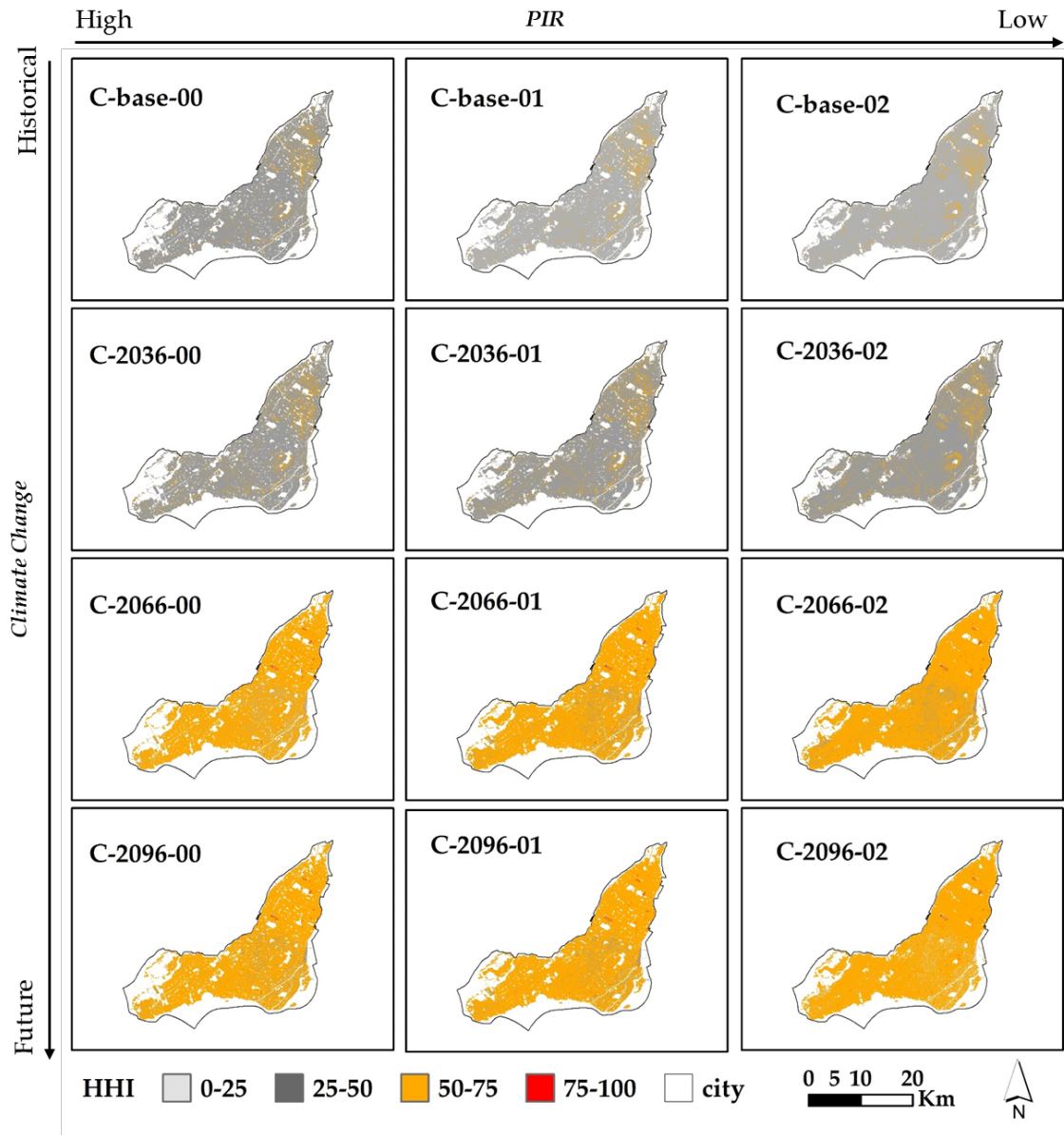


Figure 3.6 The HHI maps for Montreal under different climate (base year, 2036, 2066, and 2096) and land cover scenarios (base, Scenario 1, and Scenario 2).

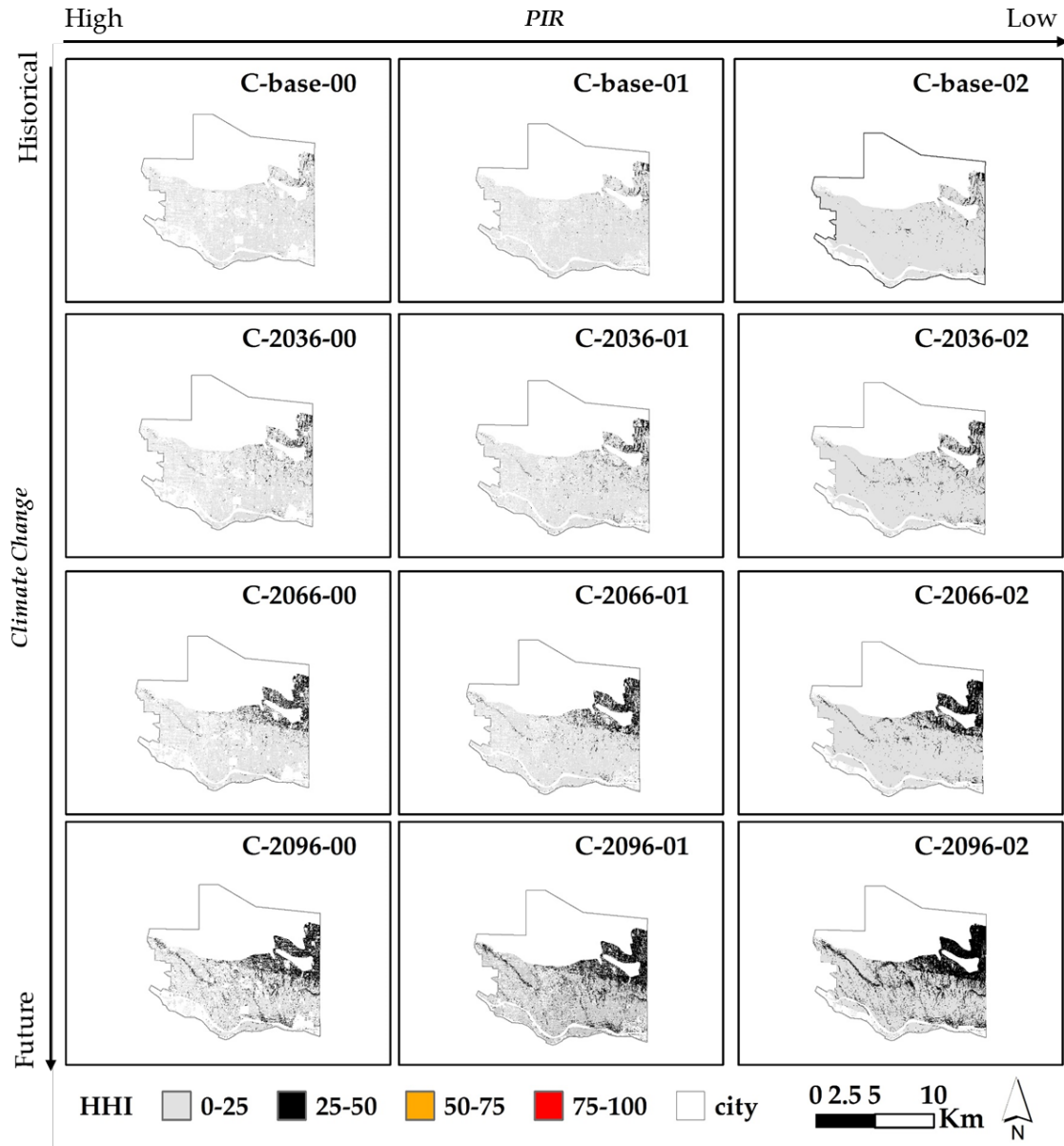


Figure 3.7 The HHI maps for Vancouver under different climate (base year, 2036, 2066, and 2096) and land cover scenarios (base, Scenario 1, and Scenario 2).

Figure 3.8 compares the histogram of HHI for each city, for each urbanization scenario, for the four climate periods. The results show that, with time (from the base time to 2096), the HHI values increase (i.e., have a higher mean), i.e., the histograms shift to the right, which indicates higher runoff generation potential and, thus, an increase in demand for LID for source control. This shift is the lowest for Vancouver compared with the other two cities. There is an exception in the observed trend in Toronto for the 2066 scenario for which the mean HHI change compared with the previous scenario (2036) is minor due to the similarity of the rainfall intensity of these scenarios. Likewise, in Montreal, Scenario 2096 has slightly followed the overall pattern because the rainfall intensity in this scenario has not increased compared with the previous scenario (2066). In addition, with urbanization, the number of cells (i.e., locations within the cities) generating runoff are increasing as well. This is because pervious areas have been converted to impervious areas—and thus, are generating runoff in areas that did not under the base urbanization scenario (resulting in higher peaks of the histograms).

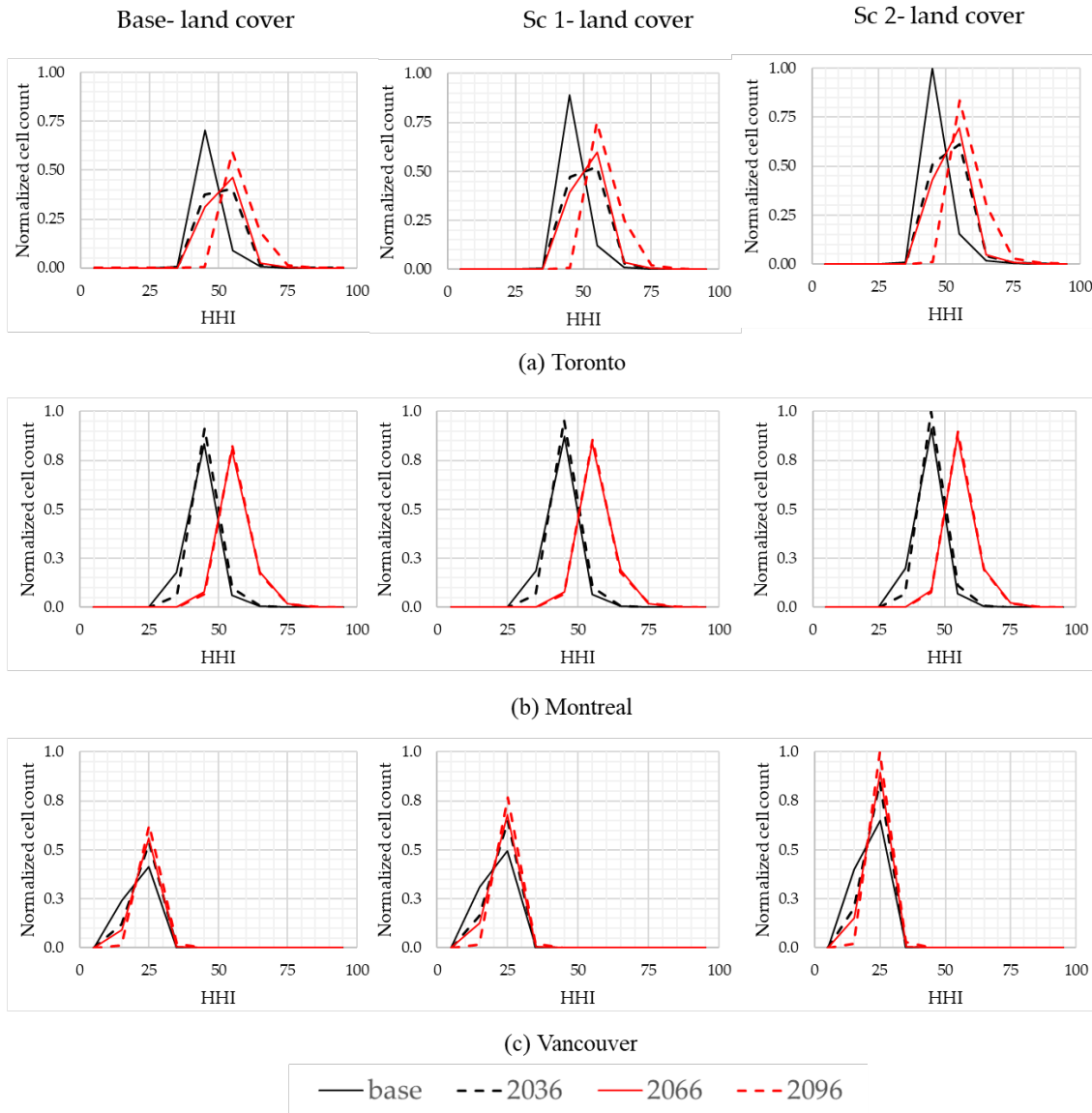


Figure 3.8 Normalized histograms of HHI (to the maximum HHI frequency of the cities) comparing the same urbanization scenarios (base, Scenario 1, and Scenario 2) and different Climate scenarios (base, 2036, 2066, and 2096) for: (a) Toronto; (b) Montreal; and (c) Vancouver.

Figure 3.9 shows a comparison of the climate change scenarios (i.e., rainfall intensity) for each city versus the different urbanization scenarios. This figure demonstrates that the change in climate has a relatively minor impact on the HHI frequency, as compared to the results shown in

Figure 3.8. An increase in urbanization results in an increase in the frequency of HHI as well as an increase in the number of cells generating runoff; this is more evident in Toronto and Vancouver than in Montreal. While the increasing rainfall intensity for each city results in higher HHI values for each urbanization scenario, the change is relatively smaller than the effect illustrated in Figure 3.8.

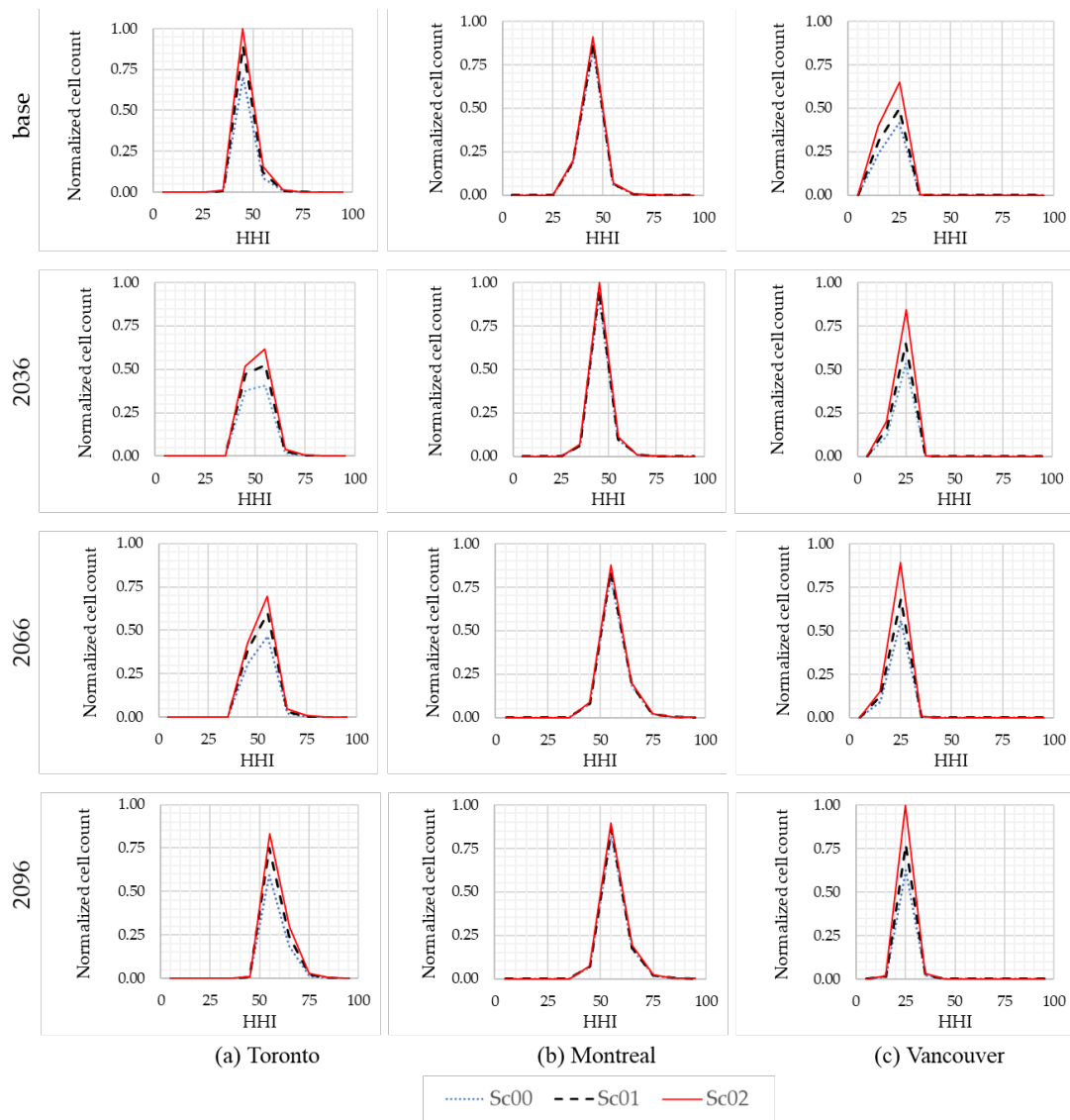


Figure 3.9 Normalized histograms of HHI (to the maximum HHI frequency of the cities) comparing the same climate scenarios (base, 2036, 2066, and 2096) and different urbanization scenarios (base, Scenario 1, and Scenario 2) for: (a) Toronto; (b) Montreal; and (c) Vancouver.

A comparison of all scenarios was conducted to determine the influence of urbanization and climate change on the magnitude of the area of sites that have a high demand for LID (referred to as high demand sites, HDS). To do this, the area of sites that have a value of HHI greater than a threshold value was calculated. The threshold was set at an HHI value of 50 for Toronto and Montreal and an HHI value of 20 for Vancouver (these values are the approximate mean HHI value for the C-base-00 scenario for each city). The area of HDS (AHDS) sites, the count of cells with an area of 25 m², was calculated for all scenarios and compared to AHDS of the baseline C-base-00 scenario. This comparison is shown in Figure 3.10.

Overall, in Figure 3.10, all three cities show an increasing trend of AHDS under integrated climate change and urbanization as well as the sole effect of these scenarios. The overall pattern under the climate change only scenarios is similar to the corresponding rainfall patterns in Table 3.2. For Toronto, urbanization seems to have a slight effect on AHDS, e.g., starting from 1.4 million cells for C-base-00 and reaching 2.5 million cells for C-base-02. In contrast, an increase in rainfall intensity due to climate change has a significant influence on increasing AHDS, e.g., the AHDS is 11.5 million cells for C-2096-00 and rises to 16.9 million cells for C-2096-02. Montreal presents similar behavior as Toronto; the AHDS of this city also has a notable increase with time for different climate scenarios. However, Vancouver's responses to climate change are similar to the impact of urbanization (from 1.2 million to 1.9 million cells in both cases) and are lower than in the other two cities. The reason is related to the low rainfall intensity of this city, which is a key difference between Vancouver and the other two cities.

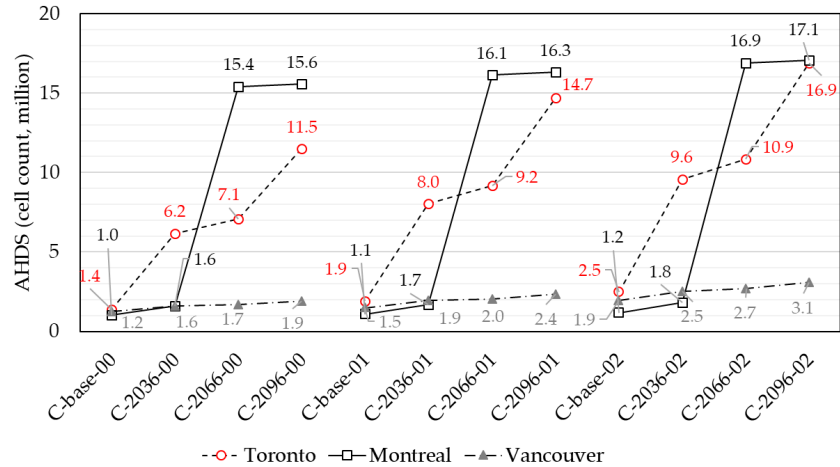


Figure 3.10 The total count of cells with HHI greater than the mean HHI for Toronto, Montreal, and Vancouver.

To further investigate the sole effect of urbanization and climate change on each city, the normalized histogram of the worst-case climate change scenario (C-2096-00) versus the worst-case urbanization scenario (C-base-02) was compared, as presented in Figure 3.11. As concluded above, in response to the effects of climate change, Toronto and Montreal present an increase of HHI value with a shift of the histograms to the right, whereas this shift is lower in Vancouver. In terms of urbanization, it is evident that in all three cities the frequency of HHI has increased (i.e., higher peaks). As mentioned above, this increase is due to the increase in the number of cells that are generating runoff (non-zero runoff cells).

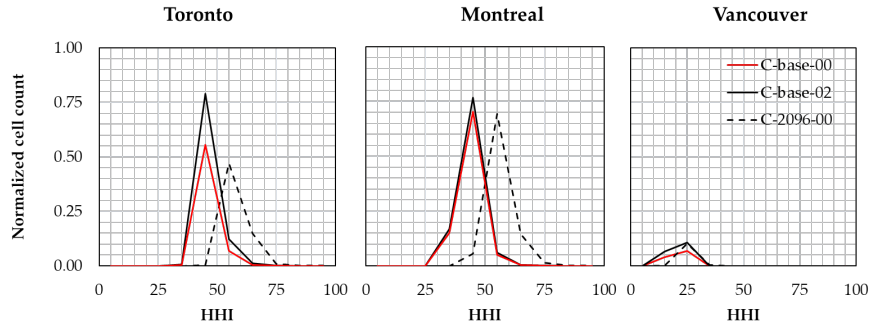


Figure 3.11 Normalized histograms of HHI (to the maximum count of three cities) of base scenario (C-base-00), the worst case of only the climate change scenario (C-2096-00) and the worst case of only urbanization (C-base-02) for the three cities (Toronto, Montreal, and Vancouver).

The trend of the mean HHI values for each city for all scenarios was also analyzed and is presented in Figure 3.12. The base scenario (C-base-00) shows that Toronto has a high HHI with a mean of 46.2. The mean HHI increases to 57.7 (a 24.9 % increase) due solely to climate change (C-2096-00) and slightly rises to 46.6 (a 0.9 % increase) solely with urbanization (C-base-02). The integrated influence of climate change and urbanization raises HHI to 58.2 (C-2096-02) (a 26.0 % increase). These results show that in Toronto the increase in mean HHI is due to climate change rather than urbanization. This is because the city has a high rainfall intensity, and the natural soil has low permeability. The consequence of increasing the HHI is that the total area of sites that need LID is increasing (since more sites are generating runoff). In this respect, the AHDS of C-base-00 for this city is 1.4 million cells (0.2 % of the city area) and reaches 11.5 million cells (8.4 times higher than the C-base-00) with the change of climate (C-2096-00). On the other hand, the AHDS growth is 78.6 % by reaching 2.5 million cells with urbanization (C-base-02). The integrated effect of climate change and urbanization increases AHDS to 16.9 million, which is 12.3 times higher than AHDS of the current state.

Montreal has a mean HHI of 44.0 in the state of the base scenario. This value rises to 56.4 with only climate change (a 28.2 % increase) and remains almost unchanged with only urbanization. The integrated effect of climate change and urbanization causes the increase of HHI value to the 56.4 (a 28.2 % increase), which reveals the significant and dominant effect of climate change on HHI in Montreal. The highly urbanized land cover of Montreal leaves limited room for more urbanization; thus, the land cover of this city has a limited change in Scenarios 1 and 2. Thus, HHI in Montreal is more sensitive to climate change scenarios rather than urbanization. Regarding AHDS, in the base scenario, Montreal has AHDS of 1.0 million cells, which increases to 15.6 million cells with only climate change and 1.2 million cells with only urbanization. The AHDS for this city rises to 17.1 million cells in the integrated climate change and urbanization scenario.

The mean HHI value for Vancouver at the base scenario is 21.3, and this increases with climate change to 25.1 (a 17.8 % increase) and remains unchanged with urbanization. The mean HHI rises to 25.1 (a 17.8 %) for the integrated climate change and urbanization scenarios. The AHDS for this city at the current state is 1.2 million cells (0.9 % of the city area), which increases to 1.9 million cells (1.6 times higher than the C-base-00) for only climate change scenarios and to 1.9 million cells (1.6 times higher than the C-base-00) for only urbanization scenario. The integrated climate change and urbanization scenario raises AHDS to 3.1 million cells, i.e., 2.5 times higher than the AHDS of the base scenario. The near-equal values of AHDS under the climate and urbanization scenarios indicate that the effect of both factors on HHI is similar. Although the mean HHI of urbanization scenarios remained the same, the increase of frequency of HHI has increased the overall AHDS.

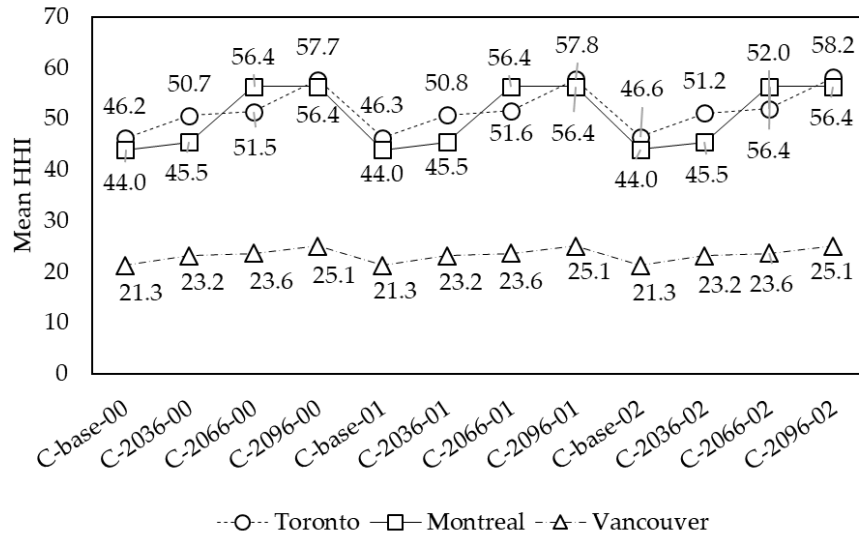


Figure 3.12 Comparing the trend of mean HHI of all twelve scenarios in Toronto, Montreal, and Vancouver.

3.6. DISCUSSIONS

An overall comparison of the cities reveals the fact that the demand for LID (which is estimated using the HHI) in Toronto and Montreal is relatively similar and is about twice the demand for LID in Vancouver. This growth in demand is represented via AHDS: the AHDS increases from 2.5 % to 16.8 %, from the base scenario (C-base-00) to the worst-case scenario (C-2096-02), respectively, for all three cities, which indicates that all cities similarly respond to the integrated climate change and urbanization scenarios. The highest growth in AHDS is for Montreal (16.8 times higher than the C-base-00), followed by Toronto (12.3 times higher than the C-base-00), and last Vancouver (2.5 times higher than the C-base-00). The growth in LID demand is also shown in the increase of the mean HHI values, which increased by 26 %, 28.2 %, and 17.8 % in Toronto, Montreal, and Vancouver, respectively. In addition, we showed that the demand for LID highly depends on the rainfall intensity rather than the overall mean annual rainfall. Vancouver,

which has the highest mean annual precipitation among the selected cities, has the lowest demand for LID, which is due to its low rainfall intensity.

Generally, we showed that, if we retain the land cover as it is in these three cities, climate change will cause an increase in demand for LID since the runoff generation potential for each city will increase. With climate change only, urbanization only, and an integrated change of both, the three cities showed similar behavior: an increase in HHI, which indicates an increase in runoff generation potential, as has been reported in previous studies [188]–[194].

However, the standalone effects of climate change and urbanization were different for these cities. Toronto and Montreal were more sensitive to climate change compared with urbanization, and Vancouver was sensitive to both factors. Thus, depending on the rainfall intensity and the extent of urbanization in the study area the dominance of these two factors varies. Which factor is likely to have a greater influence on runoff generation has been reported in previous studies? Some studies found that urbanization likely exerts a greater impact on runoff than climate change [189], [195]–[197], whereas other studies confirmed that climate change impact dominates the urbanization in runoff change [191], [193], [194]. Our finding is that the key factor is the rainfall intensity. Based on this, climate change dominates urbanization levels wherein the rainfall intensity is high (e.g., Toronto and Montreal) and adversely wherein the rainfall intensity is low (e.g., Vancouver). It is notable that, if the land cover of the study area is already impermeable (such as Toronto and Montreal), the dominance of climate change increases. In this context, the room for further urbanization is limited and climate change is the only factor that can alter the runoff.

In this study, we investigated the effect of poor urbanization by converting pervious land covers to impervious. By poor urbanization, we mean urban development by increasing

impervious surfaces without either decreasing imperviousness in other locations or implementing LID. Therefore, for future research, we suggest the study of more city-scale cases such as areas with both high permeability and runoff intensity (which were not included in three case studies) to further investigate the dominance of urbanization and climate change.

In addition, in contrast to the poor urbanization scenarios, a study on smart urban growth [22] is recommended. From the hydrological point of view, smart growth consists of measures such as preventing urban sprawl in future development (e.g., poor urban planning such as designing wide streets) [22] as well as using integrated stormwater management strategies such as LID [198]. Smart growth is related to the early stages of urban planning [198] and strategies that need to be considered for future development. LID techniques, a component of smart growth, can be a solution for both pre- and post-development conditions, i.e., they can be retrofitted into highly urbanized areas or be designed in the initial planning stages of new developments. Cities similar to Montreal that are already highly urbanized have limited options for new developments wherein LID can be installed; however, LID can be retrofitted into existing areas. Retrofitting LID broadly across the city will help reduce the negative impacts of poor urbanization by increasing the overall permeability of the city. Cities such as Toronto, which are not as highly urbanized and have low permeability of the natural soil, have a high demand for LID. Thus, for this city, smart growth for future development as well as retrofitting existing areas with LID are both viable options. For Vancouver, which has a low demand for LID compared to the other two cities, the actual need for LID should be investigated in more detail using detailed design studies and hydrological modelling. However, similar to the other two cities, smart growth is suggested since there is demand for LID and the impervious land cover in the city is dominant (61 % of the city area).

Overall, the future urban growth (increase in the proportion of impervious surfaces) needs

to be limited in order to reduce the runoff generation potential, and, hence, the risk of urban floods. Additionally, where possible, the current impervious land cover should be converted to natural, permeable surfaces. The increase in permeability (through the use of LID techniques) will help reduce runoff generation and offset the impacts of urbanization and climate change impacts.

3.7. CONCLUSIONS

In this study, we investigated the effect of climate change and urbanization on urban runoff generation potential using a geospatial framework for three Canadian cities (Toronto, Montreal, and Vancouver). The analysis was performed using a recently developed geospatial index (called HHI) using publicly available data. Four climate change scenarios (base, 2036, 2066, and 2096) and three urbanization scenarios (base land cover, Scenario 1, and Scenario 2) were developed. The HHI was estimated for the three cities for the 12 integrated climate change and urbanization scenarios.

In our study, we showed that climate change increases the mean HHI of the study area while urbanization raises the frequency of HHI. The extent of these changes varied based on the study area. Those with high rainfall intensity (Toronto and Montreal) showed a more significant increase in mean HHI compared with the study area with low rainfall intensity (Vancouver). In addition, the current impermeableness and room for further development within a city affected the extent of increasing the frequency of HHI.

The results agree with previous findings on the influence of climate change and urbanization on increasing the runoff and hence, the demand for LID. However, the magnitude of the effect of climate change and urbanization on the HHI varied in each city, which is also in

agreement with results of previous studies. For example, in cities such as Toronto and Montreal with high rainfall intensity and low permeability, climate change is a dominant factor compared with urbanization. This is different from Vancouver that has low rainfall intensity climate change and urbanization level. In this city, HHI is sensitive to both factors. We also concluded that Toronto and Montreal have a higher demand for LID, and this increases significantly with climate change and urbanization. Vancouver has a lower demand for LID and a lower rate of HHI change with the scenarios. The results of this study provide us with an insight into the contribution and the effect of climate and urbanization on the demand for LID.

These results, and the proposed methods, can be used in flood management, urban planning and for the sustainable development of cities. It is notable that, in addition to the rainfall and urbanization, HHI accounts for hydraulic conductivity, depth to the groundwater, and depth to the soil restrictive layer such as bedrock. In this study, we only investigated the effect of climate and urbanization on HHI and demand for LID, whereas modification of those parameters (hydraulic conductivity and depth to groundwater) in the future is possible and should also be studied.

CHAPTER 4: A SIMPLIFIED GEOSPATIAL MODEL TO RANK LID SOLUTIONS FOR URBAN RUNOFF MANAGEMENT

4.1. PREFACE

The focus of this chapter is the third sub-objective, developing a systematic and simplified geospatial model for ranking LID solutions (where and what type of LID to install) to maximize LID benefits. The model in this study is referred to as the LID-Solution Evaluation and Ranking Approach (SERAH). The LID demand index (LIDDI) developed in Chapter 2 was modified and enhanced to rank LID solutions. As a result, this chapter introduces SERAH to rank the LID solutions by incorporating the key contributing criteria (including LID benefits (hydrological, environmental-socioeconomic), cost, feasibility, and demand of the subcatchment). The applicability of SERAH is tested for a study area within the City of Toronto using a stormwater model (PCSWMM).

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Contributions:

The contributions of authors in the current chapter are as follows, **Sarah Kaykhosravi:** has conducted the literature review, performed the data collection and curation, developed the method, used the required software to perform the analysis and modelling, validated and visualized the results, and have prepared and wrote the original manuscript of this publication. **Usman Khan** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript. **Mojgan A. Jadidi** has supervised the research, provided the funding, contributed to the development of the method, writing, and editing the manuscript.

4.2. ABSTRACT

Many studies have shown the usefulness of Low Impact Development (LID) for runoff management in urban areas. However, there exists a gap for a systematic decision-making model to rank LID solution (where and what type of LID to install). In this research, a physics-based GIS-MCDM model is proposed, which we refer to as the LID-Solution Analysis and Ranking Approach (SERAH). SERAH integrates the key contributing criteria including LID benefits (hydrological, environmental-socioeconomic), cost, feasibility, and demand for LID within a subcatchment. The effectiveness and applicability of SERAH are demonstrated through modelling a catchment in the City of Toronto. Three types of LID (rain garden (RG), infiltration trench (IT), and porous pavement (PP)) were selected for the study. The LID solutions were ranked using SERAH. To test the effectiveness of SERAH, the hydrological performance of the ranked solutions

was estimated using a stormwater management model (PCSWMM). In PCSWMM nine scenarios including a base scenario (no LID installed in any subcatchment) and eight LID scenarios in which one type of LID (with identical design parameters and size) was implemented in individual subcatchments iteratively. The results demonstrated that the ranks of SERAH correspond to the best hydrological performance of stormwater model. The ranked subcatchments, in order, reduced the runoff volume by 9.8, 11.3, 9.0, 8.9 percent and peak runoff by 19.9, 10.4, 13.4, 1.3 percent compared with the base scenario, a catchment with no LID. In ranking the LID types, IT was ranked the highest amongst the three types for the 16 of the 19 subcatchments of the study area. The cost of LID was identified as a key factor in changing the rank of the LID type. However, in the remaining three subcatchments, the socioeconomic-environmental benefits of RG outweighed its higher cost. Thus, for these three subcatchments RG was identified as the highest-ranked LID type. The effect of different rainfall durations, frequencies, and temporal patterns on the performance of the highest-ranked LID solution suggested that LID provide higher performance in more severe events. SERAH lends itself to the scenario development for stormwater models and strategic planning for multifunctional sustainable infrastructure. It also suggests that future research is needed to better quantify the LID socioeconomic and environmental benefits to improve SERAH.

4.3. INTRODUCTION

Urban stormwater infrastructure such as LID (e.g., bioretention cells, rain gardens, green roofs, and permeable pavements), are used for detaining or retaining excessive rainfall (runoff) which in turn decreases runoff volume and peak flow rate also delays the time to peak in the

drainage system downstream [21], [25], [29]. The primary benefits of most types of LID is its hydrological benefits such as runoff peak and volume reduction [21], [25], [29], [57], [93], [94], and recharging groundwater [35], [199]. Also, many lateral benefits such as environmental and socioeconomic are associated with some types of LIDs [30], [200]. Examples of environmental benefits are improved water quality, decreased air pollution, and enhanced biodiversity [56], [57], [59], improving microclimates [38], mitigating urban heat island [39], [40]. Examples of socioeconomic benefits include access to amenities and green spaces, rainwater harvesting, enhancing health, and improving educational results [33], [34].

These benefits could be increased by ranking LID solutions based on the accrued benefit. A high-ranked LID type provides the highest ratio of benefits to cost compared with other feasible types of LID in a specific subcatchment. A high-ranked feasible subcatchment has the highest demand for LID benefits (primary and lateral LID benefits). Conventionally, to answer the question where to install LID, the focus typically goes toward determining locations wherein implementing LID is feasible (e.g., [109], [201]). The feasibility criteria are usually set by regulatory bodies through guidelines and standards. However, the link between the demand of subcatchments for LID and the benefits provided by each type of LID is typically overlooked. The demand for LID types is different from one subcatchment to another. Thus the benefit of one type of LID varies in different subcatchments [86], [100], [152], [202]. For example, if in a specific subcatchment, a green space in any form is not in high demand, implementing a green roof would not be the preferred option compared with much less expensive LID types such as rain barrels [203], [204]. As such, the cost of each type of LID is another factor that affects identifying the optimal LID solution. To identify an optimal LID solution at the catchment scale, it is necessary to systematically consider the feasibility of implementing LID, the demand of subcatchment for

LID, and the cost and benefits associated with LID types.

Most of the previous studies have used the scenario-based approach (e.g., [205] and [206]), which is a traditional iterative (trial and error) method for ranking the LID solutions. In these types of studies, several LID solutions are generated and compared, and the most hydrologically efficient one is selected. The combinations are typically selected based on the geospatial feasibility criteria for implementing LID along with other intuitive criteria such as managerial decision or expert judgment. These scenarios are evaluated using a stormwater model and their performance is compared to rank the scenarios. For example, Simperler et al. (2020) [205] have ranked the LID solution using the results of a stormwater model (using hydrological performance as the metric) and through iterative modelling of potential locations for LID and types of LID based on expert judgment. Radinja et al. (2019) [206] also introduced a multicriteria framework to evaluate the hydrological performance of seven different scenarios. In their approach, the location and types of LID were identified by preliminary placement constraints such as flooding rate and space availability. In both studies, lateral benefit and the cost of each scenario were not considered.

Other similar studies further have focussed on the role of cost in ranking LID solutions. These studies have investigated the trade-off between the cost and benefit of LID solutions with a particular focus on runoff reduction, e.g., [76], [207]–[209]. For example, Lee et al. (2020) [76] focused on the cost-effective design of LID by coupling an optimization model with the SWM. In their method, in addition to the runoff reduction, improvement of water quality (as a lateral benefit of LID) was also considered. Jia et al. (2013) [210] ranked different LID types using their reported primary and lateral benefits (via synthesizing the information from research literature and reports). These benefits were not linked to the geographical location and demand. This linking is important since we need to assess whether there is a demand for each of the LID benefits (e.g., is there a need

for a plant-based solution or not?). Considering this demand could improve the cost-effectiveness of the LID solution.

A few other studies have used Multi Criteria Decision Making models (MCDM) (e.g., [99], [210], [211]) to rank LID solutions. For example, Ariza et al. (2019) [99] used an MCDM system (not GIS-based) to integrate more significant factors such as the lateral benefit of LID and suggests LID solutions. Similarly, Jia et al. (2013) [210] introduced a multi-criteria selection index system (MCIS), which in a tabular format, quantifies and overlays multiple criteria (e.g., impact of LID types on water quantity and quality) to rank LID solutions. Likewise, Hager et al. (2015) [211] created the One Water Stormwater Planning Framework (OWSWPF) with a focus on identifying the most cost-effective LID solution. OWSWPF defines the target water balance distributed among LID, stormwater collection networks, and water reuse. Then ranks the LID solutions using a MCDM model (not GIS-based) overlaying the results of a simplified water balance model, LID benefits, and LID cost under various precipitation data. The MCDM model used in these studies is not GIS-based. Thus, these studies essentially have overseen the incorporation of the geospatial criteria into the MCDM process for ranking LID solutions. Also, the decision of where to implement LID is often considered as a strategic parameter and identified based on intuitive criteria.

There is a limited number of studies that have considered the use of GIS-based models to rank LID solutions (e.g., [212]–[214]). In a study, Tecca et al. (2021) [212] developed a GIS-based MCDM model to rank locations that demand for LID using their developed hydrological index. The focus of their method was mainly on hydrological benefits of LID, the geospatial feasibility for implementing LID, and lateral benefits of LID were overseen. Fletcher et al. (2021) [213] has used a GIS-based (raster discretization) models to identify high-demand cells for LID. Ranking

types of LID and the hydrological benefit were neglected in their framework. In another similar study, Hou et al. (2020) [214] proposed a GIS-based optimization algorithm to prioritize LID scenarios. The objective of their algorithm was to maximize the hydrological performance and pollution treatment and minimize the total cost of different types of LID. Unlike many other studies for estimating the hydrological and water quality performance, the conventional stormwater modelling approach was replaced by a GIS-based model. Their GIS model uses pixel discretization and assumes that each type of LID has a ratio of performance. The optimal scenario in their study was identified using the results of the calculated GIS-based performance against the cost of different scenarios. The popularity of the development of GIS-MCDM models in recent years demonstrates their effectiveness and usefulness to address ranking LID solutions. As noted by Nguyen et al. (2020) [20] in their recent review on the topic, there is very limited research that has integrated all contributing factors through a systematic framework to identify an optimal LID solution in a catchment.

In this research, a systematic and simplified geospatial model referred to as LID Solution Evaluation and Ranking Approach (SERAH) is proposed. SERAH ranks the LID solutions (where and what type of LID to install). The novelty of SERAH lies in its ability to incorporate physical principles and the MCDM model to meet urban stormwater management goals. SERAH uses a geospatial system and includes key contributing criteria. These criteria include LID benefits (hydrological, environmental-socioeconomic), cost, feasibility, and demand of the subcatchment. SERAH is applicable in all catchments and has not been customized for a specific catchment. To demonstrate the practical aspect of the proposed approach, it was applied to a highly urbanized catchment within the City of Toronto. Three types of LID (rain garden (RG (essentially a bioretention cell without drainage through an underdrain pipe)), infiltration trench (IT), and porous

pavement (PP)) were selected and ranked for the study. This allowed us to demonstrate the applicability of SERAH in a real-world case study. It offers a systematic objective solution as an alternative to the traditional intuitive (subjective) solutions. SERAH can further be incorporated into decision support tools for making rigorous sustainable urban planning and decisions. This paper is organized as follows: Section 4.4 presents the method and the case study. Section 4.5 includes the results and discussion, and Section 4.6 follow with a conclusion.

4.4. METHOD

4.4.1. Develop the LID-Solution Evaluation and Ranking Approach (SERAH)

SERAH was designed to integrate the key criteria that contribute to the decision of ranking LID solutions. As shown in Figure 4.1, it includes three components: (a) feasibility of subcatchments for implementing LID; (b) hydrological-hydraulic demand of subcatchments and the cost of each LID type; and (c) socioeconomic and environmental demand of subcatchments for each type of LID, and benefit offered by each LID type. SERAH uses publicly available data that conventionally has been used for stormwater modelling purposes.

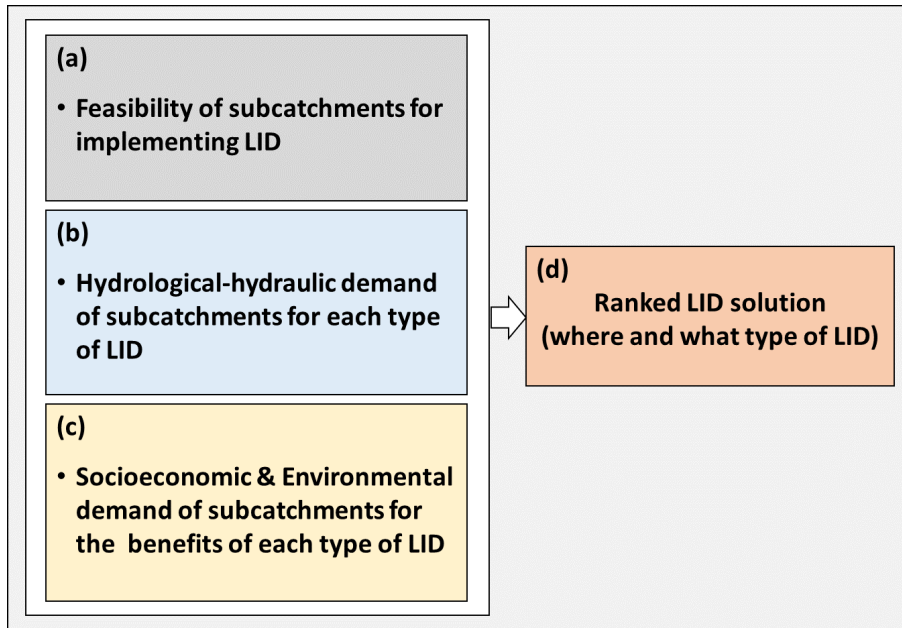


Figure 4.1 The conceptual schematic of SERAH for ranking LID solutions with its three components

Component (a) of the model identifies the feasible subcatchments for implementing LID using geospatial analysis. In this study, we have identified the feasible subcatchments in two stages. First, all data were converted to raster format where the raster consists of cells with a size of 5 m by 5 m, which is the resolution of the DEM data (in other words each subcatchment is discretized into 5 m by 5 m cells and is bounded by the subcatchment boundary which is defined by the DEM). Then the feasible cells were determined through the geospatial overlaying process, which is described in detail below. Then the subcatchments within the study area that include an adequate area of feasible cells were considered as feasible subcatchments.

Identifying feasible cells is commonly performed by geospatial overlaying methods considering the geospatial criteria (e.g., the slope of the cell, land cover, etc.) and constraints (e.g., the slope should be less than 0.5 %). These criteria and constraints are usually set by regulatory bodies through guidelines and standards (e.g., [99], [109], [175]).

Three types of LIDs were selected for this study (RG, IT, and PP) to be implemented and ranked by SERAH in each feasible subcatchments. These are the types of LID that are implementable in open spaces (rather than on buildings like green roofs). For these three types of LID, the feasibility criteria were identified based on the Toronto and Region Conservation Authority (TRCA) [175] recommendations which is the governing regulator authority of the selected case study (Section 4.4.2). We collected the required geospatial datasets, performed the data preparation and cleansing, segmented the study area as cells, performed multiple geospatial integration processes based on the criteria, and identified the feasible cells.

Based on TRCA recommendations, the locations (individual cells within a subcatchment) wherein LID is to be implemented (for RG, IT, and PP) need to meet the following criteria. The cells should have a slope of less than 5%. IT and RG need to have a minimum ratio of contributing drainage area to LID area of 5:1; this ratio can be 1:1 for PP. The maximum contributing drainage to LID area ratio should be 20:1, 10:1, and 1.2:1 for IT, RG, and PP, respectively. A setback of 4 m from buildings and be at least 1 m above the seasonal water table are recommended. The focus this study was on the conventional feasibility criteria. Thus, other TRCA recommendations, such as the hydrologic group of soil type, proximity to underground utilities, wellhead protection, pollution control based on land use, etc. are assumed to be met for simplicity. Also, subjective or practical feasibility criteria such as considering existing green spaces as a potential LID location was not considered.

The required datasets to analyze and identify feasible locations (individual feasible cells within a subcatchment) were Digital Elevation Model (DEM), land cover, and groundwater depth data. From the raster format DEM data (with a resolution of 5 m) the slope data was created and cells with a slope less than 5 % were extracted. Using the DEM data, we identified the cells that

met the requirement of minimum ratio of contributing drainage area to LID area (5:1). This requirement ensures that the IT and RG receive a minimum runoff from the upstream. Although PP does not have the same requirement (according to the TRCA (2010) guideline), to attain the same feasible cells for all three types of LID (for simplicity) we considered the same limitation for the PP as well. Without such an assumption, the number of feasible cells for PP would be higher, which will suggest PP as the only option for some of the subcatchments. Our focus in this study was on ranking subcatchments that are feasible for implementing all three types of LID. Investigating more complex scenarios (subcatchments are feasible for implementing an unequal number of LID alternatives) is suggested to be conducted using SERAH in a future study.

To extract the cells which meet the minimum ratio of contributing drainage area to LID area (5:1) the following process was performed. The flow direction, which shows the direction of flow at the cell to its steepest downslope neighbour was generated using DEM data. The result was used to create the flow accumulation raster. The flow accumulation represents the accumulated weight of all cells into each downslope cell. In the flow accumulation raster, the most upstream cell is assigned a weight of 1. For example, a weight of 5, shows that 5 upstream cells drain into the cell (contributing drainage area is 5 times the cell area). On this basis, the cells with a weight of 5 and greater can at least drain 5 upstream cells. These cells were identified and extracted.

Cells with a setback of 4 m and less from buildings were screened out using a 4 m buffer around the building cells (in raster data). Similarly, cells with a water table depth of 1 m and less were eliminated from the potential feasible cells. These analyses provided us with four data sets, each representing the feasible cells according to each criterion. These data sets were geospatially overlaid using a geospatial intersection operation. As a result, the feasible cells that corresponded to all criteria were identified. The conceptual geospatial model of the process is presented in Figure

4.2.

Following this, the feasible subcatchments were determined. To do so, the maximum of the LID area to the contributing drainage area ratio was considered as the criteria. This ratio allows for excluding the subcatchments that contain a few feasible cells from being considered as a feasible subcatchment. The ratio of the area of feasible cells within each subcatchment to the area of the subcatchment was estimated. The selected ratio for this step was the maximum of the suggested ratios, 20:1 suggested for IT, equals to 5 % of subcatchment. Final checking for the maximum LID area to the contributing drainage area ratios suggested by TRCA for all three types was conducted during the detailed design in the stormwater modelling process.

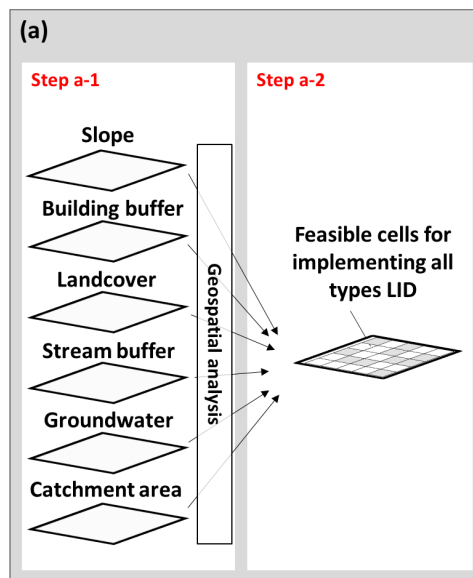


Figure 4.2 Component (a)-SERAH, the conceptual schematic for identifying feasible cells for LID, step 1: identifying the contributing data sets, step 2: generating the feasible cells data layer

The next component of SERAH, Component (b) (illustrated in Figure 4.3) was estimating and incorporating the Hydrological-Hydraulic Index (HHI) and the cost of different LID types. The HHI is a measure of the potential of a subcatchment to generate runoff [152]. Subcatchments that generate higher runoff, have a higher HHI value, and thus, have a higher demand for LID. To

estimate HHI, the equation developed in [152] was used. This equation has been validated against physics-based models and is a good geospatial index for decision-making purposes. Ranking the subcatchments based on HHI values highlights the subcatchments that are the main source of runoff generation. On this basis, we can target the high HHI subcatchments for LID implementation, and thereby effectively capture the runoff at the source [152]. Since the demand for LID corresponds to the HHI values, a subcatchment with high HHI values is considered a subcatchment with high demand for LID [152]. The HHI index accounts for seven variables, as presented in Eq. 4.1. The estimation of HHI included the two following steps. First, the data were converted to raster format with the size of the DEM data, then and HHI was generated using Eq. 4.1. Second, the HHI of the subcatchments was calculated using the sum of the HHI of cells that fall within the subcatchment.

$$HHI_i = \begin{cases} \left[R_i - ((K_s)_i \cap (K_i)_i) \cap \left(n_j \times ((D_g)_i \cap (D_r)_i) \right) \right] \times [1 + (\tan S)^{0.385}] & \text{for } R_i > Ks_i \\ 0 & \text{for } R_i \leq Ks_i \end{cases} \quad (\text{Eq 4.1})$$

In Equation 4.1, i is the cell number; HHI_i is HHI at cell i ; R_i is rainfall intensity (mm/h) at cell i ; $(K_s)_i$ is saturated hydraulic conductivity of the surficial soil (mm/h) at cell i ; $(K_i)_i$ is the hydraulic conductivity of impervious areas (e.g., roads, parking lots, and building rooftops) at cell i , which is set equal to zero for impervious cells; n_i is the soil porosity at cell i ; $(D_g)_i$ and $(D_r)_i$ are, respectively, depth to groundwater (mm) and depth to the first restrictive soil layer (mm) at cell i ; and S is the terrain slope (degrees) at cell i [152].

Following the generation of HHI for all subcatchments, the Hydrological-Hydraulic Cost

Indices (HHCI) for different LID types were developed. It was performed based on normalizing the HHI with the LID cost-equivalent (cost per equal volume runoff reduction, $\$/m^3$) as shown in Eq. 4.2 and Figure 4.3. In this study, we have used the capital cost (per equal volume runoff reduction) values derived from a study conducted by Joksimovic et al. (2014) [203] which estimated the capital cost of a single and different combination of LID types per runoff volume reduction (in $\$/m^3$). As noted, this cost only represents an estimate of the capital costs, and if the life-cycle costs are available, we suggest including these if possible.

$$HHCI_{i,j} = \frac{HHI_i}{Cost_j} \quad (\text{Eq 4.2})$$

Where i is cell number; j is LID type number; $HHCI_{i,j}$ is the modified HHI of LID type j at cell i , HHI_i is the HHI at cell i , and $Cost_j$ is the cost of LID type j .

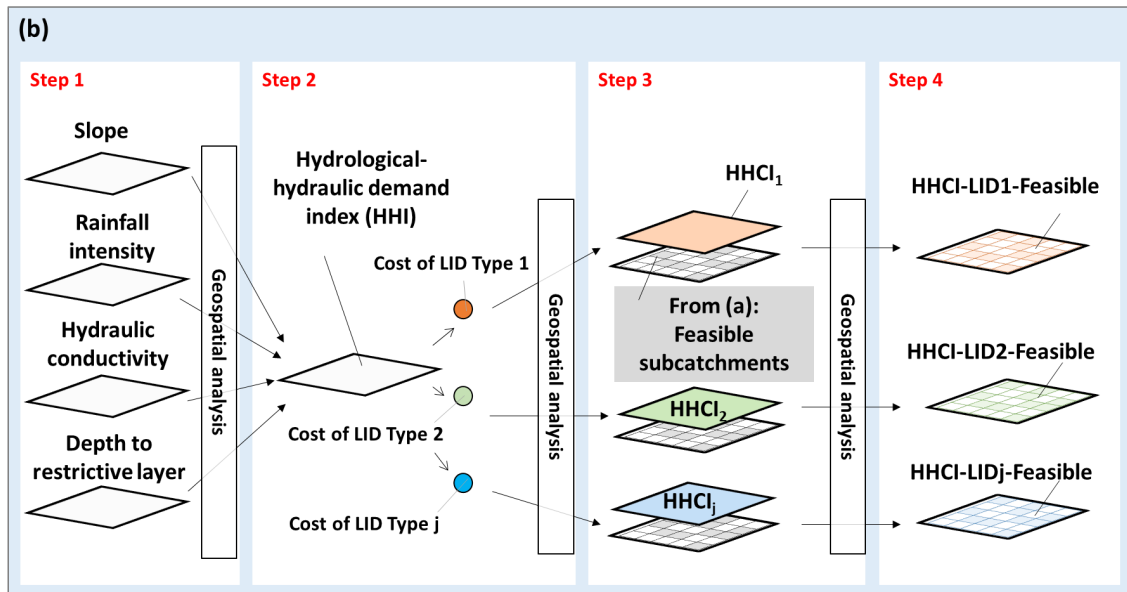


Figure 4.3 Component (b)-SERAH, the conceptual schematic for determining the hydrological-hydraulic demand for each type of LID at each feasible subcatchment

The third component of SERAH, Component (c), as shown in Figure 4.4, indexes the study area based on the demand of subcatchments for the environmental and socioeconomic benefits (i.e., the lateral benefits) of each LID type. An example of the physical meaning of the index is that if there is a high demand for treating “air pollution” at a subcatchment, the LID type that offers such a benefit should receive a higher rank compared with another LID type that is not able to treat air pollution. To what extent each LID type can treat air pollution could be a metric based on which LID types can be ranked (e.g., bioretention cell is ranked higher than a rain barrel in this regard since they have the potential to improve air quality [210]). On the flip side, where there is no air pollution, the type of LID that provides air pollution treatment should not receive a high rank. Thus, at a subcatchment with minimal demand for air pollution treatment, the rank of a bioretention cell and a rain barrel are equal in this respect. Previous research has overlooked this link between the lateral benefits of LID and the demand of subcatchment for that benefit.

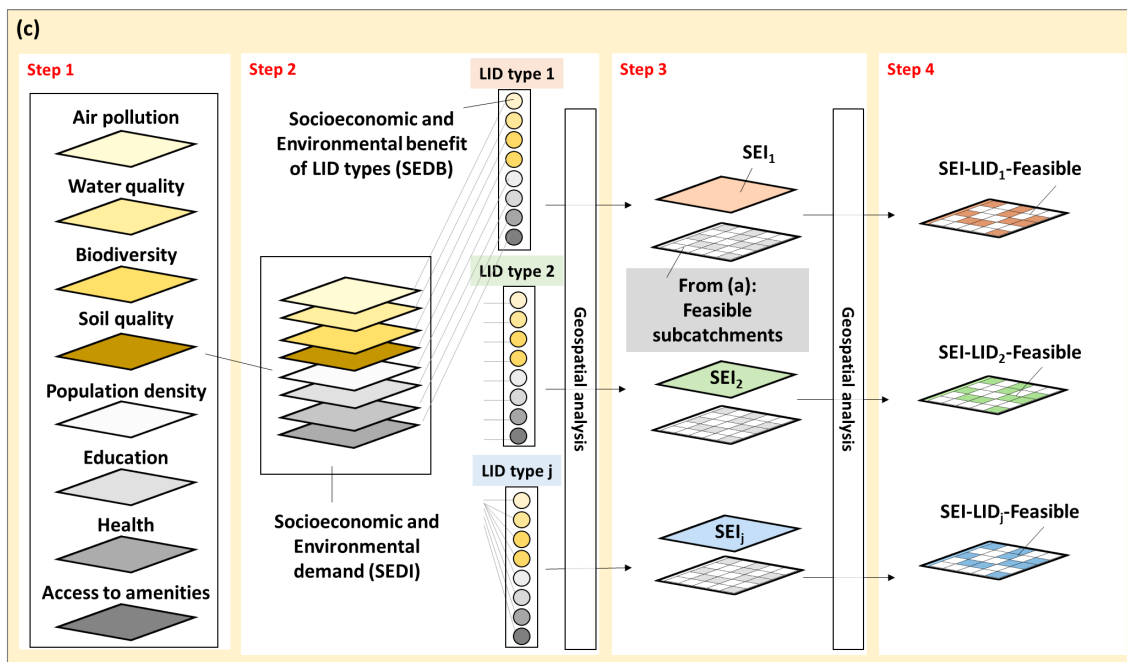


Figure 4.4 Component (c)-SERAH, the conceptual schematic for determining socioeconomic and environmental demand for each type of LID at each feasible subcatchment

All types of LID do not provide all benefits for the demands that may exist in the subcatchments. Also, the magnitude of benefits of individual LID types is different. To account for this, for each type of LID a Socioeconomic-Environmental Index (SEI) was generated. SEI represents the integrated benefit that each type of LID can provide considering the demand of the subcatchment for the same benefit. For example, if green space is not in high demand at a subcatchment, implementing PP and IT (which are not considered green spaces) are ranked equal to a rain garden (which is considered as green space). This is to change the traditional point of view of constant privileging LIDs with higher benefits (which are usually more costly) wherein that benefit is not required. For example, a study by Jia et al. (2013) [210], have used a GIS-independent MCDM system, compared the hydrological and environmental benefits of eight types of LID, and ranked bioretention cells as the first and rain barrel as the eighth. Their study gave bioretention cells a preference without identifying if there is a demand for this type of LID. Unlike this traditional point of view, SEI incorporates the extent of demand to the benefit of each LID type.

The estimation of SEI included the two following steps. First, the data were converted to raster format with the size of the DEM data (5 m by 5 m), then the SEI of cells was generated using Eq. 4.3 and Eq. 4.4. Second, the SEI of subcatchments was created by estimating the mean of the SEI of cells that fall within the subcatchment.

The mathematical model for applying this concept was performed through a GIS-based heuristic relationship (Eq. 4.4). First, three Socioeconomic-Environmental Demand Indices (SEDI) were generated [152], based on the three selected criteria for this study. These criteria included: i) decreasing Total Suspended Solid (TSS) concentration (denoted as $SEDI_1$) [70]; ii) even distribution of green spaces, for its ecological benefits (denoted as $SEDI_2$) [210]; iii) aesthetic

benefit for buildings (SEDI₃) [210]. Note that out of many possible criteria (e.g., [30], [70], [208], [215]), we selected these three to focus on to demonstrate the application of SERAH. Thus, the criteria may change according to the case study and its associated needs.

All three demand indices representing TSS, even green spaces, and aesthetic benefits were generated by calculating the Euclidean distance from the source [216]. The sources have a distance equal to zero and cells farther from the source have a higher Euclidean distance. The source for SEDI₁ was pavement cells (streets, roads, parking lots, etc. where TSS is typically washed off from). The objective was to capture the TSS at the source and the distance from the pavement lowers the priority of the subcatchment. TSS from pavements is one of the main contributors of the TSS sources in our urban study area (other possible contributors are erosion, landfills, construction sites, etc. which does not apply to our case study) [217]. The source for SEDI₂ was green spaces. The reason is to increase the even distribution of green spaces to enhance the LID ecological benefits. To achieve an even distribution, cells in the vicinity of green spaces were ranked lower. The source for SEDI₃ (aesthetic benefit) was building cells. EPA (1995) has reported that the value of buildings next to well-designed types of LID has increased about 28 % based on a study conducted by the National Association of Home Builders [208], [215].

All three indices were standardized by applying the linear standardization between 0 and 1. The linear standardization assumes that the demand is a linear function of distance, which is a simplification of reality. This standardization is a well-known procedure [218] in the design of decision-making systems that allows for bringing a wide range of criteria with various magnitudes into a similar unit to be comparable and integrable. For SEDI₁ and SEDI₃, the maximum value, one (1), was given to minimum distance (representing a high demand for LID close to the pavement surfaces and building blocks) and inversely the minimum value was assigned to the

maximum distance from the pavements. In contrast, for $SEDI_2$ the maximum value, one (1), was assigned to the maximum distance to the green spaces (representing a high demand for LID wherein the distance from green spaces is far). The process is presented in Table 4.1.

Table 4.1 The process of generating the socioeconomic-environmental demand index (SED) for each of the selected criteria

Criteria	Data set generated by calculating	Comment	Priority	Standardization
SED1: decreasing TSS concentration	Euclidean distance to the pavement	1- buildings were considered as a barrier	closer distance higher priority	inversely rescaled by linear function between 0 and 1
SED2: even distribution of green spaces	Euclidean distance to green spaces	2- distance calculated before clipping the data to the extent of the catchment to account for the neighbourhood	closer distance lower priority	rescaled by linear function between 0 and 1
SED3: aesthetic benefit for buildings	Euclidean distance to the building			

$$SEDI_i = \frac{ASEDI_i}{(ASEDI_i)_{\max}} \quad (\text{Eq. 4.3})$$

Where i is the cell number, $ASEDI_i$ is the actual value of SEDI at cell i , $(ASEDI)_{\max}$ is the maximum value of ASEDI within the study area, and $SEDI_i$ is the standardized ASEDI at cell i . The mathematical model for SEI which incorporates the demand index (relates to the cell) into the benefit that the type of LID provides for the same demand is presented in Eq. 4.4.

$$SEI_{i,j} = \sum_{k=1}^n w_k \times SEDI_{i,k} \times SEB_{j,k} \quad (\text{Eq. 4.4})$$

Where SEI_{ij} is Socioeconomic-Environmental Index at cell i ($i=1$ to l , l is the number of cells covering the study area), for LID types j ($j=1$ to m , m is the number of selected LIDs), $SEDI_{i,k}$ is SEDI at cell i for benefit k ($k=1$ to n ; where n is equal to three in this study), $SEB_{j,k}$ is the

Standardized Socioeconomic-Environmental Benefit k (0 to 1) of LID type j , and w_k is the weight of criteria k and the sum of weights for all criteria should be 1. The SEB of the selected LID types in this study and their associated SEDI are presented in Table 4.2.

Table 4.2 Standardized benefits of the selected LID types in this study and their associated SED

Decreasing TSS concentration benefit		Even distribution of green space benefit		Aesthetic benefit for buildings			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
LID Type	Percent decreased TSS concentration [70] *	Mean column (2)	Normalized: column (2)/ max(column(2))	Percent benefit (compared to other LID types) [210]	Normalized: column (5)/ max(column(5))	Percent aesthetic benefit (compared to other LID types) [210]	Normalized: column (7)/ max(column (7))
RG	-6-99	46.5	0.63	80	1.00	1.0	1.00
IT	46-100	73.0	0.95	20	0.25	0.2	0.20
PP	47-100	73.5	1.00	20	0.25	0.4	0.40

*change in concentration [220]

An example of how SEI is calculated for two assumed subcatchments (x and y) are presented in Table 4.3. Subcatchment x has a demand of 1 for TSS removal ($SEDI_{x,1}=1$), no demand for green space ($SEDI_{x,2}=0.0$), and 0.25 for aesthetic benefit ($SEDI_{x,3}=0.25$). Subcatchment y has an equally high demand for all benefits ($SEDI_{y,1}=SEDI_{y,2}=SEDI_{y,3}=1$). Also, it was assumed that all three benefits are equally important, so have equal weights of one-third (0.33). The ranking results in Table 4.3 suggest that at subcatchment x , PP is the most suitable LID whereas at subcatchment y , RG is the priority option offering more benefits. This is because SERAH accounts for the demand of the subcatchment and justifies the benefit of each type based on the demand. Therefore, even though the rain garden for subcatchment x is the most beneficial LID (Table 4.2), the subcatchment demand can change this perception. Note that this ranking was only based on the lateral demand and benefits. SEI needs to be incorporated into the primary demand and benefit (HHCI) to rank the subcatchments and rank the types of LID comprehensively.

Table 4.3 Estimation of SEI for two sample subcatchments (x and y) for prioritizing LID alternatives (LID1 to 3)

subcatchment ID	LID	$SEI_{x,1} = (w_1 * SEDI_{x,1} * SEB_{1,1}) + (w_1 * SEDI_{x,2} * SEB_{1,2}) + (w_1 * SEDI_{x,3} * SEB_{1,3})$	Rank of LID Type
x	RG	$SEI_{x,1} = (0.33 * 1 * 0.63) + (0.33 * 0.0 * 0.95) + (0.33 * 0.25 * 1) = 0.29$	3
	IT	$SEI_{x,2} = (0.33 * 1 * 1) + (0.33 * 0.0 * 0.25) + (0.33 * 0.25 * 0.25) = 0.35$	2
	PP	$SEI_{x,3} = (0.33 * 1 * 1) + (0.33 * 0.0 * 0.20) + (0.33 * 0.25 * 0.40) = 0.36$	1
y	RG	$SEI_{y,1} = (0.33 * 1 * 0.63) + (0.33 * 1 * 0.95) + (0.33 * 1 * 1) = 0.85$	1
	IT	$SEI_{y,2} = (0.33 * 1 * 1) + (0.33 * 1 * 0.25) + (0.33 * 1 * 0.25) = 0.50$	3
	PP	$SEI_{y,3} = (0.33 * 1 * 1) + (0.33 * 1 * 0.20) + (0.33 * 1 * 0.40) = 0.53$	2

Since implementing LID in all cells are not feasible, the subcatchments infeasible cells' demand for LID should also be accounted for. To do this, we modified the HHCI and SEI indices by incorporating the demand of infeasible into the feasible cells through modifying the SEI and HHCI.

The SEI was modified using a cell-based calculation based, then, the mean SEI (of cells within the subcatchment) was calculated for the feasible subcatchments. The concept for modifying SEI was that the benefit of LID in a specific cell can be gained from implementing LID in the same cell or with a different magnitude of benefit in a neighbourhood cell. For example, if the need for green space (e.g., for ecological benefit) is high in an infeasible cell, the closest feasible cell can address that need. To mathematically model this concept, we used the focal weighted mean principle (the feasible cell as the focal cell) and assumed higher weights for the closer cells and lower weights for the farther cells. The weighted mean of the SEI was calculated for all feasible cells. For the weights, we assumed a linear decreasing weight that is 1 at the focal cell and 0 at the farthest cell (the boundary of the study area).

The HHCI was modified on the subcatchment discretization level (not cell-based) for the simplicity and through the hydrological concepts. Implementing LID in feasible subcatchments can capture the runoff from upstream infeasible ones. Thus, by adding the HHCI of infeasible to

the downstream feasible subcatchment the hydrological demand of those subcatchments (represented by HHCI) is reflected in the HHCI of feasible subcatchments.

We overlaid the two modified indices (HHCI and SEI) generated for the feasible subcatchments using the weighted sum method. The weight of both indices was selected identical and equal to 0.5 (Eq. 4.5). It is noticeable that the overlaying method and weights are selected to demonstrate the application of SERAH. The selection of optimal weights for the two indices is out of the scope of the research (e.g., pairwise comparison) since the focus of this study is on the development of SERAH. The selection of weights depends on a variety of parameters such as the demands of the study area, the nature of the criteria considered, the strategic decisions, and the responsibilities and objectives of stakeholders who want to implement LID.

$$\text{@ cell } i, \text{ for LID types } 1 \text{ to } j: \begin{cases} HSE_{i,1} = 0.5 \times HHCI_{i,1} + 0.5 \times SEI_{i,1} \\ \vdots \\ HSE_{i,j} = 0.5 \times HHCI_{i,j} + 0.5 \times SEI_{i,j} \end{cases} \quad (\text{Eq 4.5})$$

where $HSE_{i,1}$ is HSE at cell i for LID type 1; $HSE_{i,j}$ is HSE at cell i for LID type j ; $SEI_{i,1}$ is the SEI at cell i for LID type 1; $SEI_{i,j}$ is the SEI at cell i for LID type j ; $HHCI_{i,1}$ is the HHCI at cell i for LID type 1, and $HHCI_{i,j}$ is the HHCI at cell i for LID type j .

Figure 4.5 presents the fourth component of SERAH, Component (d), a conceptual schematic for the HSE layers (step 1); an example of the HSE value in one of the catchments that each are associated with a feasible subcatchment (step 2); and how it leads to ranking the type of LID (step 3). The ranking of subcatchments is conducted based on the values of HSE. Subcatchments with the highest HSE value have the highest rank for implementing LID.

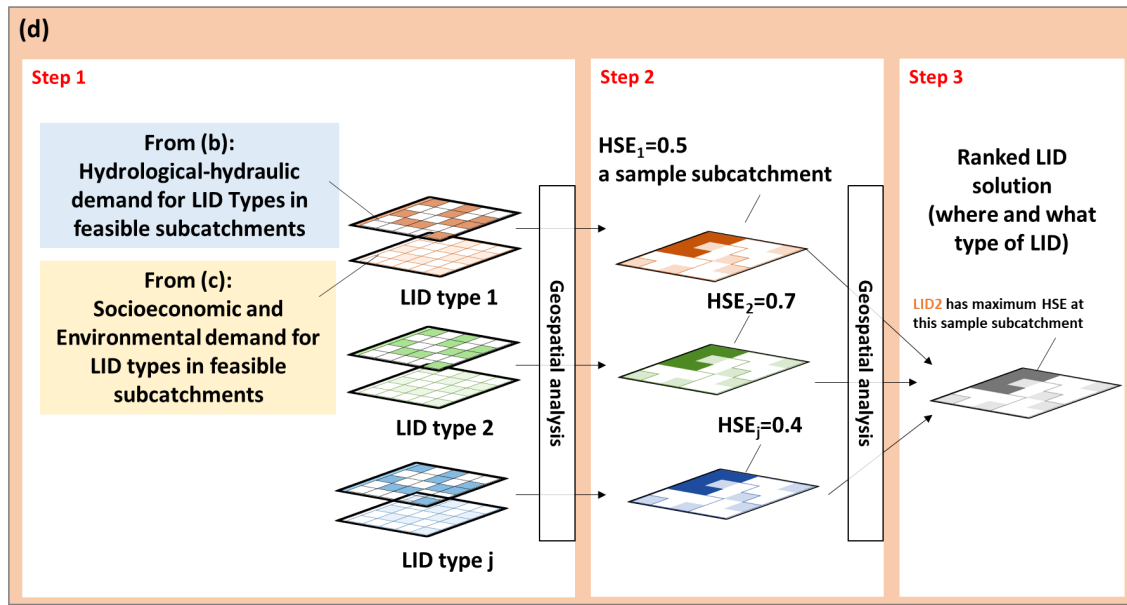


Figure 4.5 Component (d)-SERAH, The conceptual schematic for ranking LID solution, step 1) geospatial analysis of components (b) and (c), step 2) geospatial ranking of the HSE datasets, step3) identifying the rank of LID subcatchments and types

Types of LID are ranked through the geospatial ranking of HSE datasets (HSE_1 to HSE_3). For each feasible subcatchment, a comparison is made among the value of all three HSE indices of the subcatchment. The LID type with the highest HSE value is introduced as the highest priority LID for the same subcatchment. Thus, for all feasible subcatchments, the high-ranked type of LID may be identified.

4.4.2. Develop the stormwater model

To investigate the applicability of SERAH, we applied it to a case study for a location within the City of Toronto. First, the LID types and subcatchments were ranked for the case study using SERAH and geospatial analysis (using Arc-GIS Pro_15). Then the results of ranking by SERAH were hydrologically modelled using PCSWMM version 7.3. The objective of the

hydrological modelling is to validate the hydrological-hydraulic component of the method and simulating the effects of the ranked LID solutions using a hydrological model. It is notable, that the focus of the validation is on the hydrological component. The validation of the MCDM model related to the lateral benefit is not feasible since it is a decision-making component and can not be compared against a stormwater model [86].

Case study

The case study was an area of 7.3 ha located in the City of Toronto, within the East Don River watershed. This area is located upstream of one of the flood-vulnerable clusters reported by TRCA [219]. It also provides a good variety of land cover types which provides us with a variation of HHI and SEDI, which are indices that depend on the land cover of the study area. The land cover in this catchment includes high-density residential (0.18 ha, 2%), general commercial (1.1 ha, 15%), green spaces (0.78 ha, 11%), and the remaining are parking lots and streets (5.24 ha, 72%). Except for the green space (11%) which is pervious, the remaining 89% of the land cover is impervious. The location of the area and its land cover are presented in Figure 4.6. The study area overall has 8 inlet junctions, about 715 m of circular pipe conduits, with diameters ranged from 0.6 to 1.2 m [220]. The outfall of the network is located at the central south side of the study area. It is notable that, SERAH is not limited by the size of the study area of interest, as long as the necessary data (as listed in Section 4.4.1) are available.

The data used for the urban drainage network was acquired from the City of Toronto [220]. A list of data that were used in this study, their format and source are presented in Table 4.4. The drainage network and its delineated subcatchments are presented in Figure 4.7. The subcatchments were delineated using the “watershed delineation” tool in PCSWMM. The tool uses DEM data and

burns in manhole data as points. However, some judgment and justification were conducted to account for the inadequacy of DEM data precision in representing urban features such as the elevation of curbs. Some of the subcatchments were routed into the downstream subcatchments (e.g., S06 and S07 to S08) and some were directly routed to the downstream hydraulic system (e.g., S04). The maximum subcatchment size is about 1.25 ha and the minimum subcatchment area is about 0.06 ha.

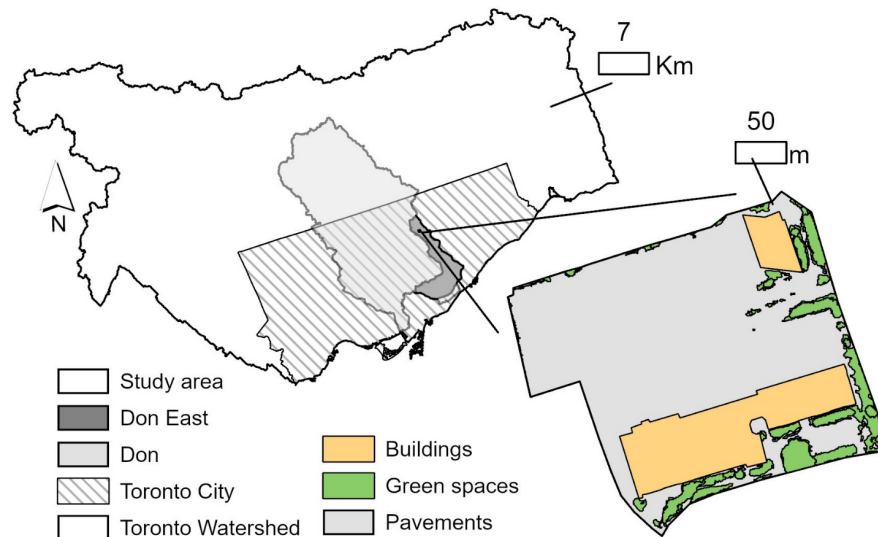


Figure 4.6 The location of the selected study area in the Toronto watershed and administrative border of the City of Toronto, Don sub-catchment and its Eastern River branch

Table 4.4 The name, format, and source of the input data in alphabetical order

Data	Format	Data Source
Bedrock layer	Vector/polygon	Ministry of Northern Development and Mines
Digital elevation model (DEM)	Raster (5 m)	Ontario Ministry of Natural Resources and Forestry - Provincial Mapping Unit
Groundwater table	Vector/point	Groundwater Information Network (GIN)
Land cover	Raster (0.6 m)	City of Toronto
Surficial geology and saturated hydraulic conductivity (K_s)	Vector/polygon	Government of Canada open data website
Toronto precipitation data	Vector/point	Institute for Catastrophic Loss Reduction and Western University [176]
Toronto rivers	Vector/polyline	Toronto and Region Conservation Authority (TRCA)
Urban drainage network	DWG file	City of Toronto

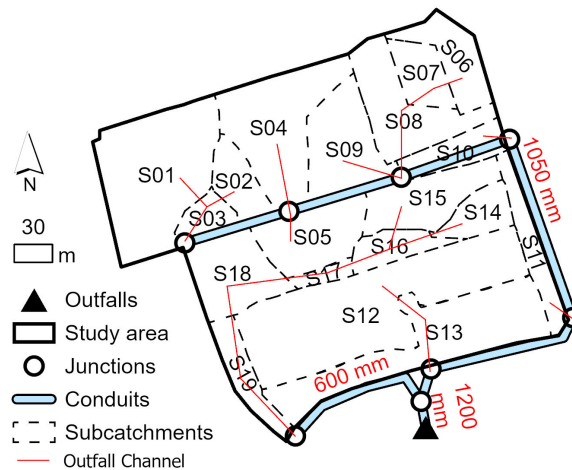


Figure 4.7 The layout of the study area, including subcatchments (S01 to S19), inlet junctions and conduit

Developing the PCSWMM model

To evaluate the effectiveness of SERAH in ranking the subcatchments, the study area was modelled in PCSWMM software. The modelling included two parts.

First, the effectiveness of SERAH in ranking subcatchments and representing their potential in runoff generation was studied. To do this, nine scenarios were developed and

modelled. Scenarios included a base scenario with no LID implemented in the subcatchments and eight LID scenarios in which one type of LID (with identical design parameters and size) was implemented in individual subcatchments iteratively. The selected type of LID was IT which was sized using the design parameters suggested in Song et al (2017) [105] and TRCA (2013) [204] (the details of the parameter values are available in Appendix F). Using this identical design, area and one type of LID for all scenarios allowed for comparing the impact of the subcatchment on the runoff reduction in the catchment. Scenarios were denoted as S01, S02, S04, S05, S08 (which receives runoff from the S06, and S07 which are infeasible subcatchments, therefore no scenarios are needed for them), S09, S13 (receives runoff from S12 which is infeasible catchment), S19 (receives runoff from feasible subcatchments (S14 to S18) with and without LID. For example, scenario S01 had IT assigned to the subcatchment S01. The assigned LID was an arbitrary area of 400 m² of LID (selected within the recommended range of LID to subcatchment area ratio) which was added to the eight subcatchments iteratively. In this part, since the selected study area (Section 4.4.1) had a time of concentration (t_c) of less than one hour the duration of 1-hr (the smallest recommended duration [221]) was used for design rainfall. Different frequencies for LID design is suggested by guidelines including 2-year [172]–[174], 5-year [173], 10-year [172], [175], or 100-year [222]. However, we have selected the most recommended frequency (10-year) and the common rainfall pattern of the study area (AES Southern Ontario).

Second, the influence of patterns on the selected LID solution was investigated using four different rainfall patterns that are commonly used in the Toronto area and are suggested by conservation authorities. It was done through simulating two scenarios: i) with LID (using the top-ranked LID solution derived from SERAH results), and ii) without LID (no LID installed) under different rainfall patterns. All results were compared and discussed based on three hydrological

metrics: i) volume runoff reduction; ii) peak runoff reduction, and iii) delaying the peak flow time. The four rainfall patterns included AES Southern Ontario, Chicago, SCS Type II, and Hurricane Hazel [222], with standard durations of 6, 12, and 24 hours were also modelled for which was available. Testing the performance of LID for the extreme events has been recommended by the TRCA. To do so, we have selected the most extreme duration and frequency for the four selected rainfall patterns. The longest duration of the AES_SO rainfall pattern is 12-hours which were generated for a 100-year frequency. Hurricane Hazel is a historical extreme event with an about 12-hours duration which has an average of about 230 mm rainfall. Chicago and SCS type II patterns also were simulated with a 24-hours duration and 100-year return period.

4.5. RESULTS AND DISCUSSIONS

4.5.1. Identifying feasible subcatchments (component a)

As mentioned in Section 4.4.1, the determination of feasible subcatchment was conducted in two stages. First, the feasible cells, which met all feasibility criteria were extracted. The feasibility criteria were based on the TRCA recommendations for the selected types of LID (Figure 4.8). Second, feasible subcatchments were determined based on the percentage of the area of feasible cells within them. The subcatchments that had an area of 5% and greater feasible cells were identified as feasible subcatchments. This was to provide an adequate area of LID in each subcatchment, also this ratio is recommended by TRCA for IT and RG (the minimum ratio of subcatchment area: LID area is 20:1). Figure 4.9 presents the location of feasible subcatchments in the study area.

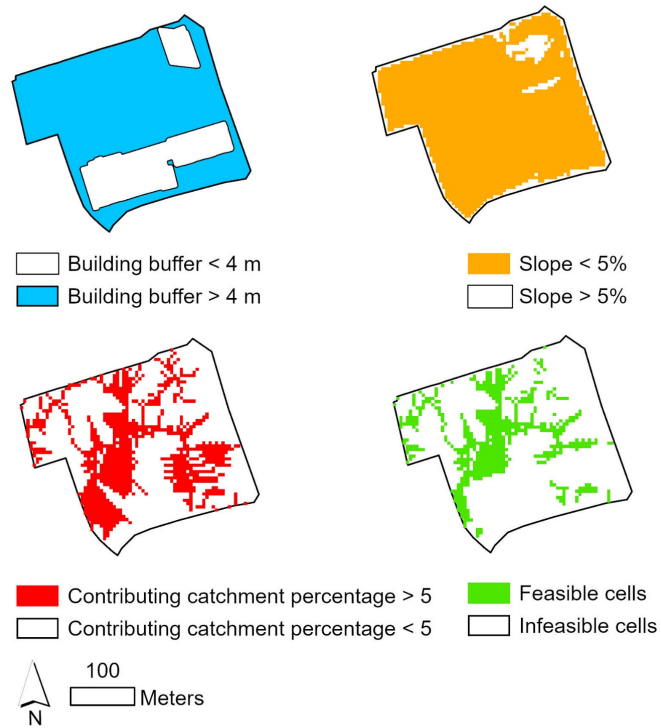


Figure 4.8 Feasibility criteria: top-left: cells farther than 4 meters from buildings; top-right: cells with slopes less than 5 %; bottom-left: cells with a contributing drainage area of 5 times and greater, bottom right: identified feasible cells (coloured green)



Figure 4.9 The location of feasible subcatchments (the area of feasible cells within the catchment is greater than 5 % of the area of catchment)

4.5.2. HHI and HHCI generation (component b)

HHI was generated using the geospatial integration of the input data in Eq. 4.1. R_i (mm/hr) was the distribution of the rainfall data (mm) for 1-hour rainfall intensity and 10 years return period [223]. It is notable that due to the size of the study area, the spatial variation of the rainfall was negligible (about 0.02 mm/hr), yet the variation of other parameters (e.g., slope and hydraulic conductivity) was considerable. K_s and K_i (mm/hr) were respectively derived from the surficial geology and land cover data of the study area and converted to the raster format. D_g and $n \cdot D_r$ were respectively derived from the data representing the depth to the groundwater and bedrock in the study area. These two parameters $((D_g)_i \cap (D_r)_i)$ were significantly greater than $(K_s)_i \cap (K_i)_i$. Thus, the intersection of the parameters was dominated by the intersection of hydraulic conductivity. The slope (in degrees) was derived from the DEM data. For generating HHI the actual value of the input data was used, and no standardization was conducted. The generated HHI for each cell is presented in Figure 4.10 (a).

The layout of the catchment (the connection between subcatchments and inlet junctions) was found to be an important factor in the estimation of the HHI of each subcatchment. The HHI of subcatchments that were the outlet of upstream subcatchments needed to account for the HHI of upstream (all cells that contribute to the runoff in the subcatchment) as well. In our case study among feasible subcatchments, S08 and S19 accepted runoff from upstream. The HHI of S08 was calculated by adding the HHI of S07 and S06 to the HHI of S08. Likewise, for S19, HHI of S19 was the sum of HHI within S14 to S19 (all cells that contribute to the runoff in S19) An example is subcatchment S19 (Figure 4.10). Other feasible subcatchments did not receive runoff from upstream and the HHI was the sum of HHI of cells within the subcatchment.

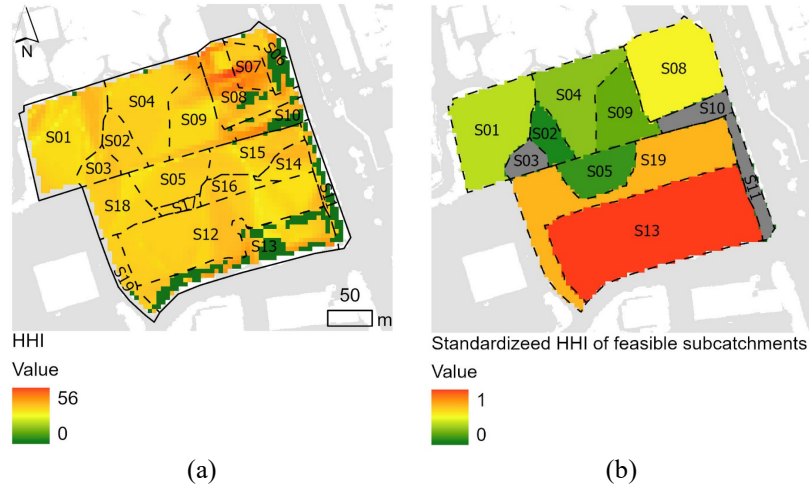


Figure 4.10 Generated (a) HHI of each cell (b) HHI of each subcatchments (normalized between 0 and 1)

The results of the stormwater modelling of LID scenarios (eight scenarios, under AES_SO rainfall pattern with 1-hour duration and 10-year frequency) are presented in Table 4.5. The results suggest that the total inflow into the LID from the S13 is the highest whereas the S02 is the lowest. It also, revealed that LID has an infiltration loss from 182 mm to 585 mm, which contributes to 46 to 100% runoff reduction. The remaining runoff is discharged to the hydraulic system from the LID as outflow. The maximum outflow is from the LID located in S13 with a value of 677 mm and the minimum is zero for S02, S05, and S09. This shows that implementing LID at these three subcatchments has reduced the runoff to zero, while other subcatchments need LID with a higher capacity. The performance of LID with equal design when is iteratively installed in different subcatchments allows for ranking the subcatchments based on their demand for LID. Thus, with an overall comparison, one can decide with a limited resource implementing LID in which subcatchment will provide the most runoff reduction result.

Table 4.5 The inflow, infiltration, and outflow of LID individually implemented in subcatchments (volume runoff per area of LID) as well as the percentage runoff reduction (the eight scenarios, under AES_SO rainfall pattern with 1-hour duration and 10-year frequency)

Subcatchment	Total inflow per area of IT mm	Infiltration loss per area of IT mm	Percentage runoff reduction	Surface outflow per area of IT mm
S13	1245	568	46	677
S19	1203	585	49	530
S08	709	540	76	169
S01	808	551	68	257
S04	632	543	86	89
S09	458	458	100	0
S05	367	367	100	0
S02	182	182	100	0

The normalized inflow and infiltration loss (normalized to the maximum value) are compared against the normalized HHI of subcatchment (normalized to the maximum value) in Figure 4.11. Overall, the figure suggests that there is a better agreement between the ranking by HHI and inflow compared with the infiltration loss (except S08). S08 has a slightly lower rank than S01 according to the “inflow” into the LID and has a marginally higher rank than S01 based on HHI. S08 is a high slope subcatchment (about 4 %) compared with S01 whose slope is 1%. In addition to runoff volume generation, HHI accounts for peak flow by considering the slope of the subcatchment, and it can cause a marginal outranking of high slope subcatchments.

The infiltration loss graph (solid blue line) and Table 4.5 showed that, once the runoff of the catchment exceeds the capacity of the LID (which starts at S04), the infiltration loss becomes almost constant. This explains the similarity of the infiltration loss of S13, S19, S08, S01, and S04. However, the potential of these subcatchments in runoff generation is high as is shown by the inflow graph (solid black line). Thus, an increase in the capacity of LID in these subcatchments helps with the increase of infiltration and presenting their actual rank by infiltration loss. Since

HHI represents the potential for runoff generation it is corresponding to the inflow into the LID.

In this highly urbanized case study, the contributing drainage area of the subcatchment was found to be a key variable in ranking the subcatchments by HHI. On this basis, the highly ranked subcatchments were found to be subcatchments that have a high contributing area (Figure 4.11 and Figure 4.12). An example of this is S19, which receives runoff from S14 to S18. The area of S19 is 0.19 ha but it receives runoff from about 1.8 ha area upstream. Despite that S19 does not generate a high volume of runoff (compared with S13 which has a high rank), implementing LID in this subcatchment has a significant contribution to the runoff reduction of the catchment. This result suggests that the topographically lowest subcatchment that has the most contributing area is the best efficient location for implementing LID. However, implementing multiple LID upstream with a capacity equal to their corresponding subcatchment will give a different result. In such a case, the subcatchment that generates the highest runoff will be the best subcatchment for implementing LID. This is along with the findings that suggest the location of LID at the end-of-pipe or the most downstream location presents better performance [98] [224].

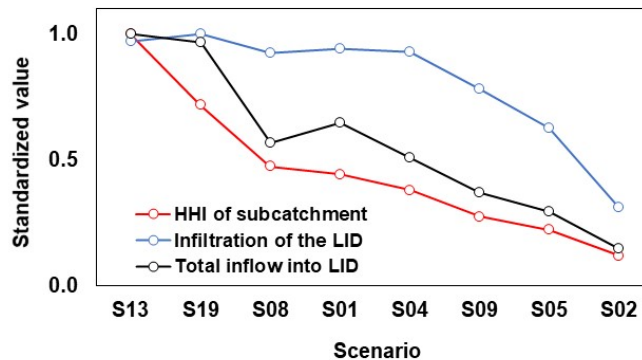


Figure 4.11 The normalized (values divided by the maximum value) HHI of subcatchments, inflow entered the LID controls (scenarios S01, S02, S04, S05, S08, S09, S13, S19), and the infiltrated runoff in each LID of individual subcatchments

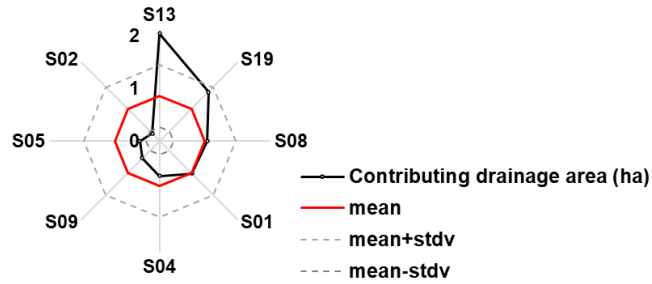


Figure 4.12 The comparison of the area of feasible and runoff receiving subcatchments (ha) with its statistics (mean, standard deviation) for the scenarios S01, S02, S04, S05, S08, S09, S13, S19

The impact of implementing LID (the eight previous scenarios) on the outflow of the case study is presented in Figure 4.13. by comparing the hydrograph of the catchment at the outlet for all scenarios (the base and LID scenarios). The result shows the stark effect of LID in attenuating the peak of the hydrograph at the outlet of the system. It also reveals that the impact of implementing LID at the first four subcatchments which were ranked higher by HHI (S13, S19, S01, S08) has a higher impact on runoff reduction, compared with the other scenarios.

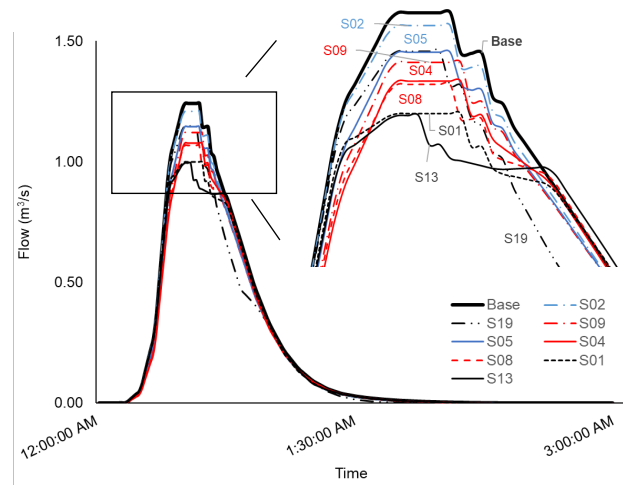


Figure 4.13 Hydrograph of the outfall of the catchment, for all scenarios (the base scenario and, scenarios S01, S02, S04, S05, S08, S09, S13, S19)

The HHCI was calculated based on dividing the HHI-subcatchment by the normalized cost of the LID. Then the results were normalized against the maximum HHI-subcatchment of all LIDs (Figure 4.14). For this study, we used the results of research conducted by TRCA (2013) and Joksimovic & Alam (2014) [203], [204], which has calculated the cost of each LID type per unit volume runoff reduction. According to this study, IT have the lowest cost, thus have the highest HHCI among the three LID types (with a maximum value of 1.0). PP, however, is the most expensive option and has a maximum value of HHCI which is one-tenth the IT and RG are in between two options (Figure 4.14). Thus, conducting a maximum operation among all three HHCI data sets suggests that IT is the most suitable option among the LID types, which was expected due to its low cost. Thus, if only the primary benefit of LID is the only concern (the lateral benefits are overlooked), the LID type that is the least expensive (cost compared based on the identical hydrological-hydraulic performance) is the most suitable option for the study area. Integrating lateral benefits could increase the priority of the more expensive types of LID.

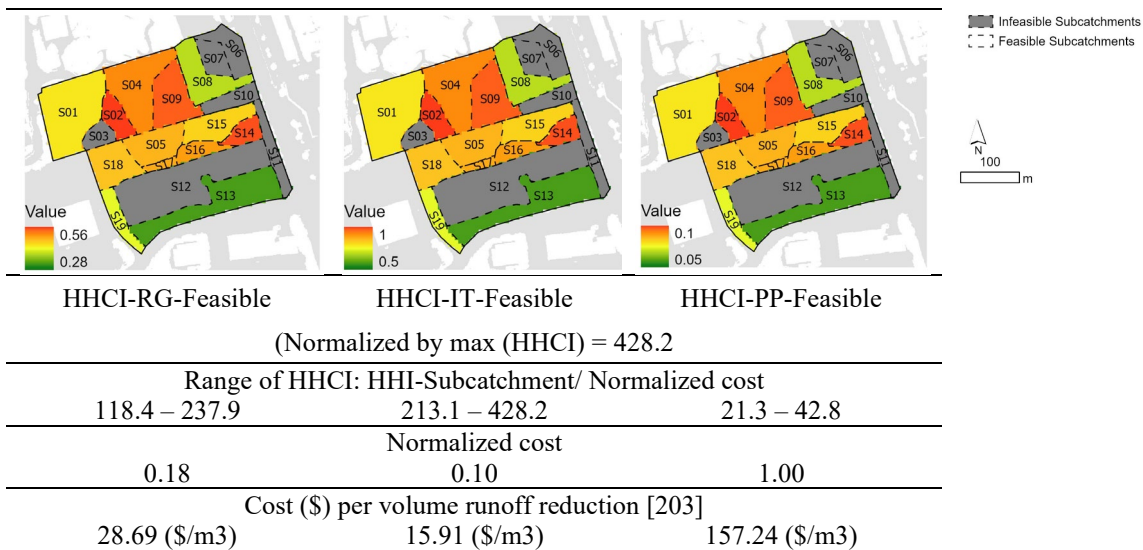


Figure 4.14 The HHCI of the three selected LIDs (RG, IT, and PP) normalized by the maximum HHCI value (428.2), the range of the generated HHCI before standardization, and the cost of each LID in \$ per volume runoff reduction in m³ (before and after standardization)

4.5.3. SEI generation (component c)

SEI was generated by following the steps presented in Table 4.1. All three layers (SED₁: decreasing TSS concentration; SED₂: the even distribution of green spaces; SED₃: aesthetic benefit for buildings) were generated by calculating the distance from the source. Comparing the results (Figure 4.15 a, b, and c) shows that there is a high demand for TSS removal across all subcatchments, whereas the demand for green spaces is only high at the west of the catchment. The eastern part of the catchment where the density of buildings is higher, has a higher demand for the aesthetic benefit of LID. The result of the integration of the demand indices (SED₁ to SED₃) into the benefit of each type of LID (SEB₁ to SEB₃) is presented in Figure 4.15 (d, e, f). Overall, the demand for RG (Figure 4.15d) is the highest among all LID types and the demand for IT is the lowest. Figure 4.15 (d) and (f) suggests that the demand for RG and PP around the north of the southern building is higher than in other parts of the catchment. The location of the demand for all LIDs is the lowest wherein green space exists. One of the remarkable results of this approach is that where the demand for the LID benefit is low the index value is low. For example, RG is a high benefit LID but the demand for RG is low wherein green space exists. This helps us with the systematic allocation of the resources where it is required.

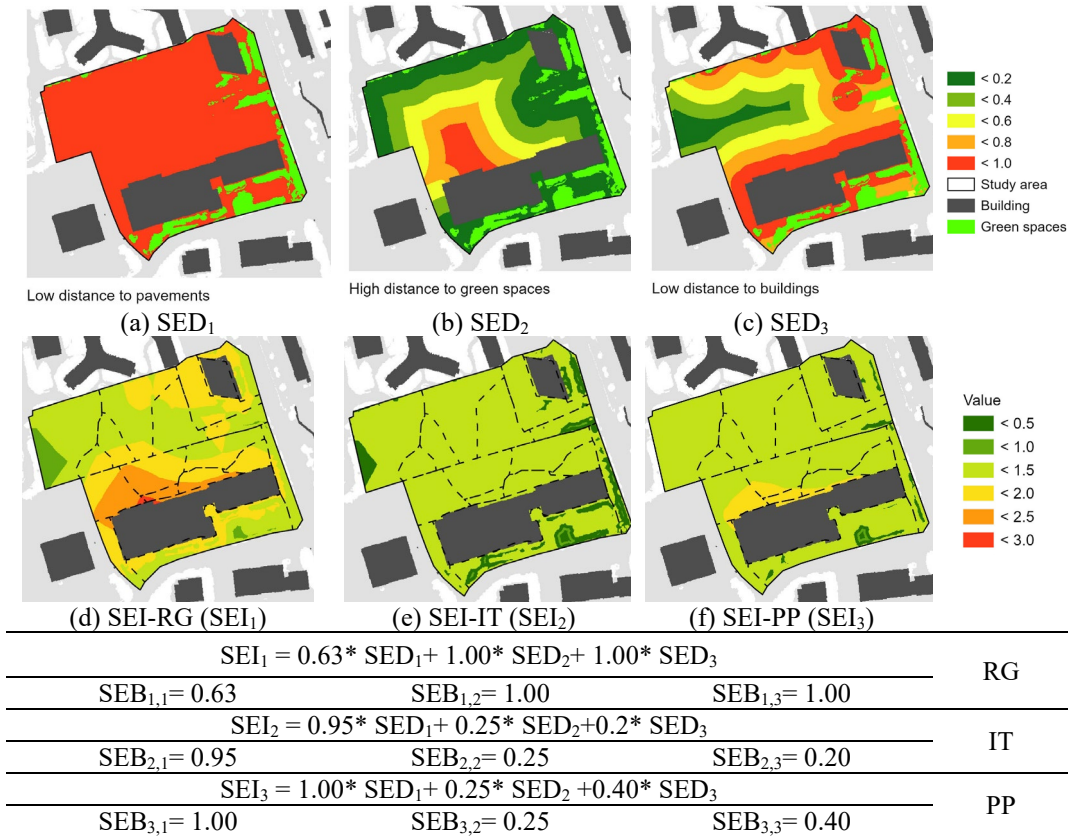


Figure 4.15 socioeconomic-environmental indices (a) low distance to pavements (representing SED_1) (b) high distance to green spaces (representing SED_2) (c) low distance to buildings (representing SED_3) (d) socioeconomic-environmental demand index for rain garden (e) socioeconomic-environmental demand index for IT (f) socioeconomic-environmental demand index for porous pavement

To account for the effect of the neighbourhood the focal weighted mean of SEI-RG, SEI-IT, and SEI-PP was generated. The results are presented in Figure 4.16 (a, b, c). Overall, the effect of the neighbourhood decreased the SEI of cells with high SEI (e.g., north of the southern building), and increased the SEI of some areas with low SEI and are located close to the high SEI areas (e.g., SEI-RG of south of the southern building). Following this, the SEI of the feasible subcatchments was created and integrated into the HHCI of each feasible subcatchment (Figure 4.16 d, e, and f). The range of the values suggest that the socioeconomic-environmental demand

for RG is higher than the other two type of LIDs (Figure 4.16 d, e, and f). Comparing the SEI of subcatchments demonstrates that the SEI of S16, S17, and S18 are the highest for all three LID types. There is also a high demand for only RG and IT at subcatchments S02, S04, S05, S14, S19. Whereas S01 and S13 have the lowest demand for RG and PP. Likewise, S13 has the lowest SEI for IT, yet the second lowest SEI-IT is not S01 and is S08.

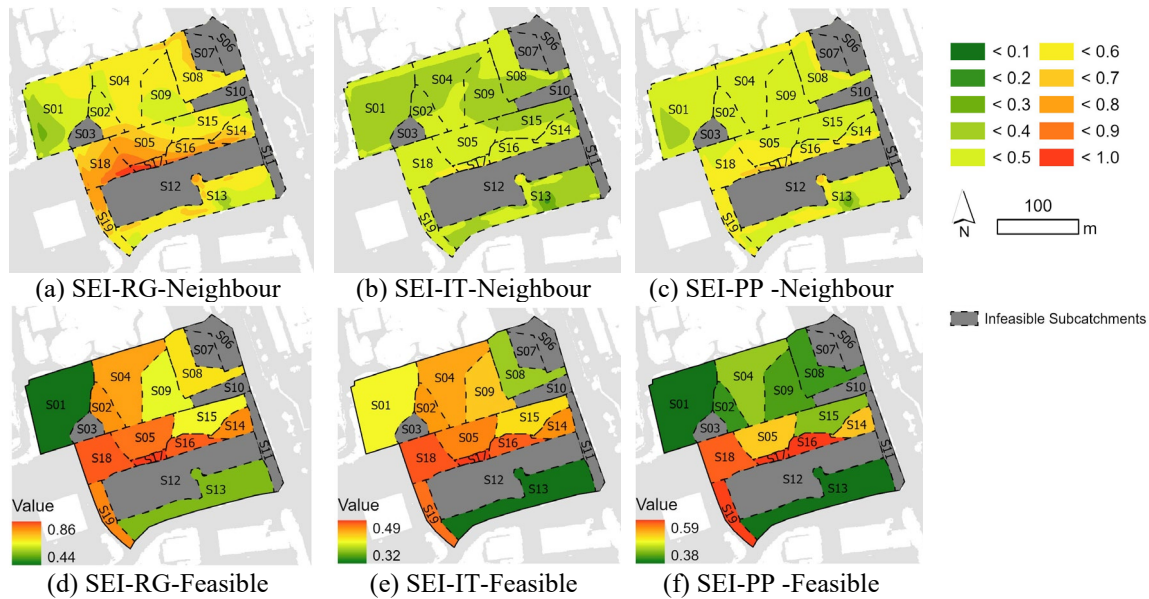
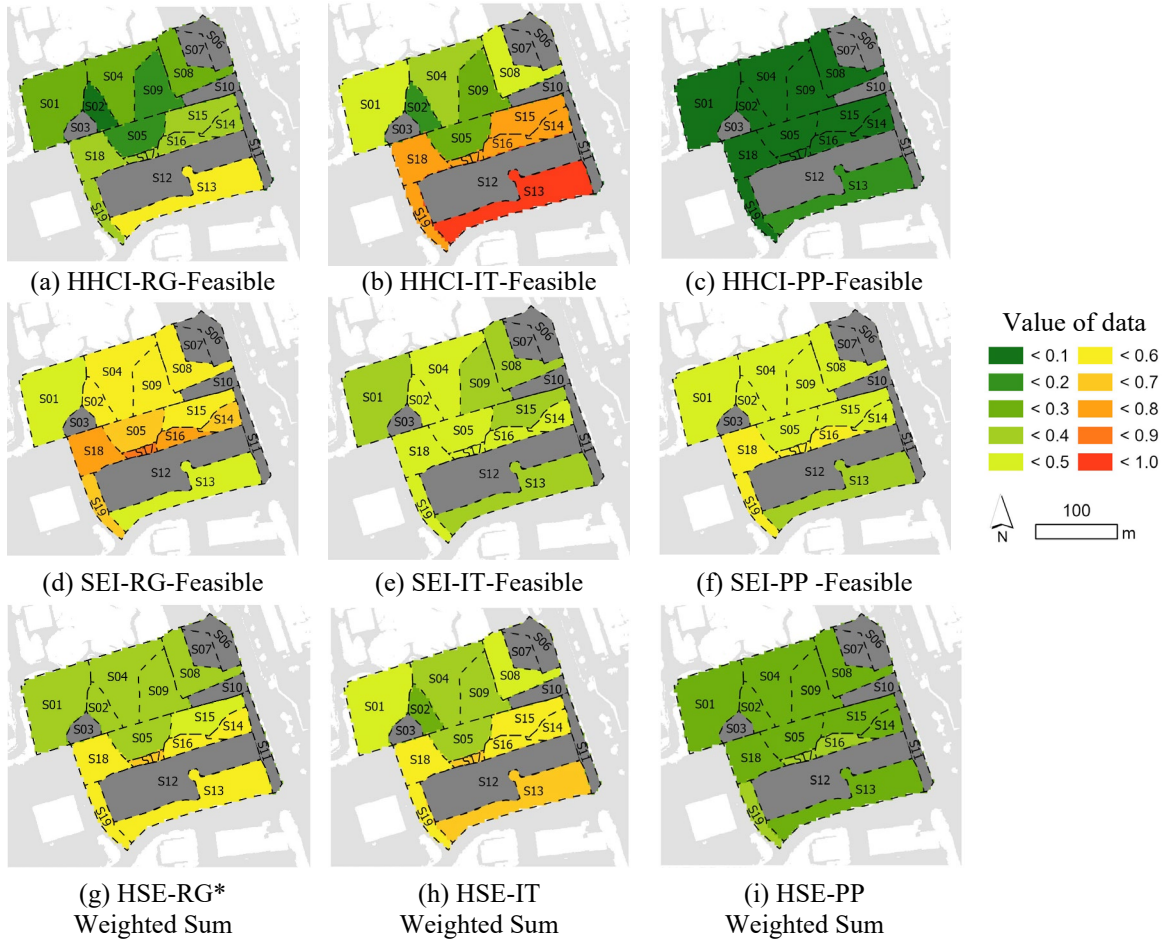


Figure 4.16 Focal weighted mean of (a) SEI for RG (b) SEI for IT (c) SEI for PP, also, the mean of SEI in each subcatchment for the three LID types at feasible subcatchments (d) RG (e) IT (f) PP

4.5.4. HSE generation (component d)

The HHCI and SEI of the feasible subcatchments are integrated using the weighted sum method considering equal weights for both indices. HHCI, SEI and HSE are colour rendered between 0 and 1, with equal intervals of 0.1 (Figure 4.17 (a) to (i)). Overall, HHCI for IT is the highest among all three types of LID whereas PP is the lowest. SEI of RG is the highest, whereas

IT and PP are about identical. The HSE for IT and RG are higher than PP. The geospatial ranking of the three HSE data sets ranks the LID types (RG, IT, PP) at each subcatchment.



*e.g., $HSE-RG = 0.5 * "HHCI-RG-Feasible" + 0.5 * "SEI-RG-Feasible"$

Figure 4.17 The HHCI, SEI, and HSE of all three LID types (RG, IT, PP)

The result of the geospatial ranking of HSE-RG, HSE-IT, and HSE-PP is presented in Figure 4.18. The figure shows that for subcatchments S02, S05, and S17 the value of HSE-RG is the highest among all, so RG was introduced as the most suitable LID for these subcatchments. For the remainder of the subcatchments, IT was identified as the highest-ranked LID. The priority of IT over the other types of LID is a result of its low cost compared with the other two LIDs. PP

acquired the lowest rank since it is costly (10 times the cost of IT) and offers low lateral benefits. The cost of RG is 1.8 times the cost of IT, yet its high lateral benefits outweighed the cost and introduced the RG as the best alternative in three subcatchment (S02, S05, and S17).

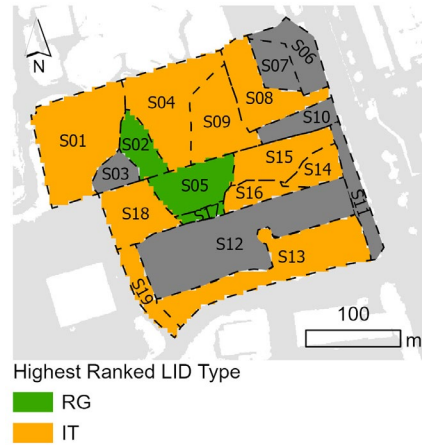


Figure 4.18 The priority of LID types to be implemented in each subcatchment

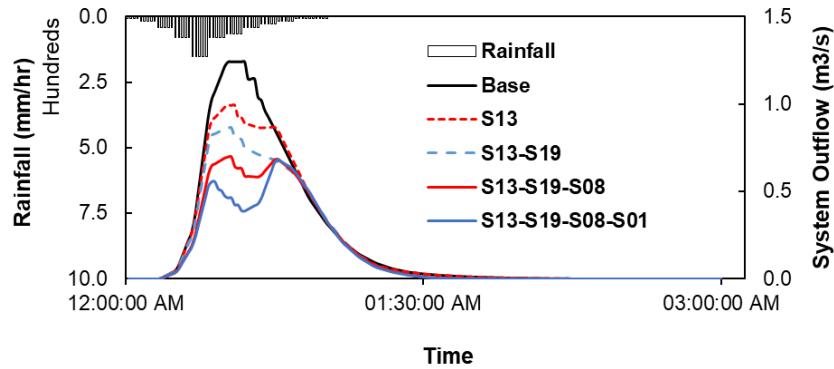
4.5.5. Hydrological Modelling

Using SERAH the feasible subcatchments and the LID types were ranked. Using the results of SERAH, we selected the first four high-ranked subcatchments (S13, S19, S01, and S08) to model after the implementation of the highest ranked LID type in each subcatchment (which was IT for each of the four). These models were developed and run to demonstrate the application and effectiveness of the ranked LID solutions provided by SERAH. In the model we assigned an area of 400 m² of IT to the four high-ranked subcatchments iteratively (Figure 4.19). The scenarios were analyzed under AES_SO rainfall pattern, 1-hour duration, and 10-year. The hydrological performance of the results (compared with the base scenario (without LID) and the scenario parameters are presented in Table 4.6.

Table 4.6 The scenario development and results of the performance of the selected solutions (a) and (b)

Scenario ID	Subcatchment with IT added to the previous scenario	The contributing drainage area (ha) of the subcatchment added	The cumulative area of IT (m ²)	Incremental area of IT (m ²)	The cumulative runoff volume reduction %	The incremental runoff volume reduction %	The cumulative peak runoff reduction %	Scenario incremental peak runoff reduction %
S13	S13	2.04	400	400	9.8	9.8	19.9	19.9
S13-S19	S19	1.14	800	400	21.1	11.3	30.3	10.4
S13-S19-S08	S08	0.90	1200	400	30.2	9.0	43.7	13.4
S13-S19-S08-S01	S01	0.87	1600	400	39.1	8.9	45.0	1.3

Table 4.6 shows that the scenarios respectively reduce the runoff volume by 9.8, 21.1, 30.2, and 39.1% and peak runoff by 19.9, 30.3, 43.7, and 45.0% (Figure 4.19) compared with the base scenario. These results showed the overall impact of IT when is implemented in the top-ranked subcatchments. Also, the scenarios respectively reduce the runoff volume by 9.8, 11.3, 9.0, 8.9% and peak runoff by 19.9, 10.4, 13.4, 1.3% (Figure 4.19) compared with the prior scenario (e.g., S13 is the prior scenario of S13-S19). These results revealed the importance of subcatchment selection for implementing IT by comparing the performance and its impact on runoff reduction (volume and peak). Overall, these results suggest that with the addition of IT to the lower rank subcatchment the subsequent effect to the total runoff reduction decreases. The exception is subcatchments S13 and S19, S13 shows the highest impact on the peak runoff reduction and S19 has the highest effect on runoff volume. S13 has a higher slope (2.52 %) than S19 (1.17 %) thus the IT has attenuated the peak runoff in this catchment significantly.



(a)

Figure 4.19 The change in the system outflow hydrograph when iteratively implementing the high-ranked LID, equal area of IT (400 m^2 per subcatchment) in each subcatchment (respectively S13, S19, S08, and S01)

Another comparison was made to investigate the effect of the different design rainfalls on the performance of IT in the four top-ranked subcatchments. For comparing the impact of rainfall frequency, we used the combination of AES_SO pattern with different frequencies of 2, 5, 10, 25, 50, and 100 years and 1-hour duration for the design rainfall. Using these rainfall patterns, six different pairs of scenarios: one with and one without IT were generated (twelve scenarios in all). Area of 400 m^2 of IT was considered in subcatchment S13, S19, S08, and S01, 1600 m^2 of IT overall. The results of the comparison are shown in Figure 4.20. The results showed that the total percentage of runoff reduction varies between 35.0 to 61.1% with an average of 42.6% for all six pairs of scenarios. Also, the peak runoff attenuated between 42.8 and 54.3% with an average of 47.3%.

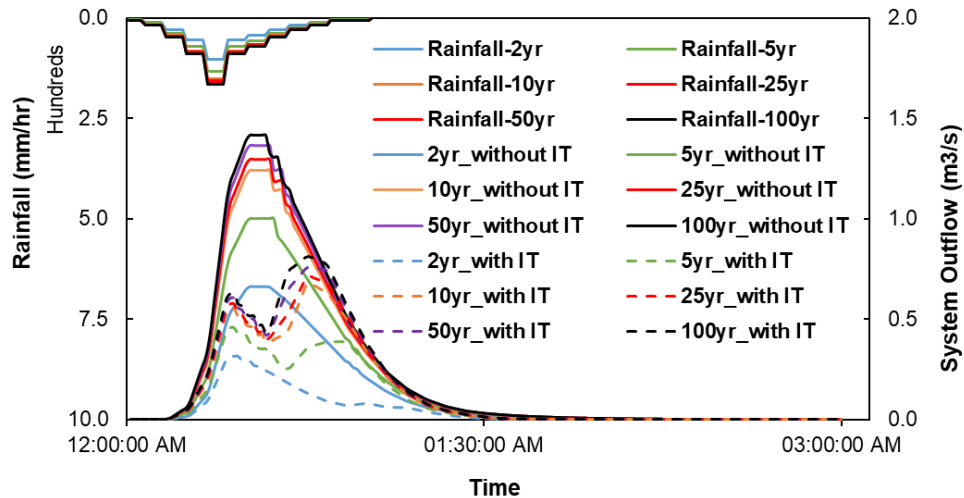


Figure 4.20 A comparison of the LID performance (implementing IT in the four top-ranked subcatchments) for AES Southern Ontario 1-hour rainfalls and 2, 5, 10, 25, 50, and 100 return periods

The influence of patterns and of extreme events on the performance of the selected LID solution were modelled based on Section 4.4.2 using the same implementation of IT in the top-four ranked subcatchments. Results of these simulations are shown in Figure 4.21 and the performance of IT under different rainfalls are presented in Figure 4.22. Overall, the results suggested that under extreme rainfall events the selected LID solution performs at a higher capacity (m^3) compared to the low frequency and duration events. The percent runoff reduction has remained between 31.6% and 61.2% for all events. But it did not exhibit a strong correlation with the frequency and duration events. In low-intensity rainfall patterns such as Hurricane Hazel, IT exhibited high performance in runoff volume reduction (maximum of all scenarios). The high-intensity rainfall patterns such as Chicago presented the lowest performance in percentage runoff reduction (the minimum of all scenarios). This result reveals the impact of the rainfall intensity on the performance of LID (IT) which agrees with other findings which reported the sensitivity of the

performance of the selected LID solution to the rainfall intensity and hydraulic conductivity [70]. Meaning that in areas with higher rainfall intensity the performance of LID (IT) is lower.

A comparison among all scenarios has suggested that implementing IT in the four high-ranked subcatchments has delayed the peak of runoff hydrograph of the catchment somewhere between 10 to 65 minutes. In this case, the impact of IT on delaying the peak of runoff was higher on rainfall patterns with lower intensities (e.g., Hurricane Hazel was delayed the most). However, there was an exception for three of the patterns which had two peaks, and the higher peak occurs earlier. Even in these cases, the overall delay of hydrograph and shift toward the later time is evident through the comparison of their hydrographs in Figure 4.21.

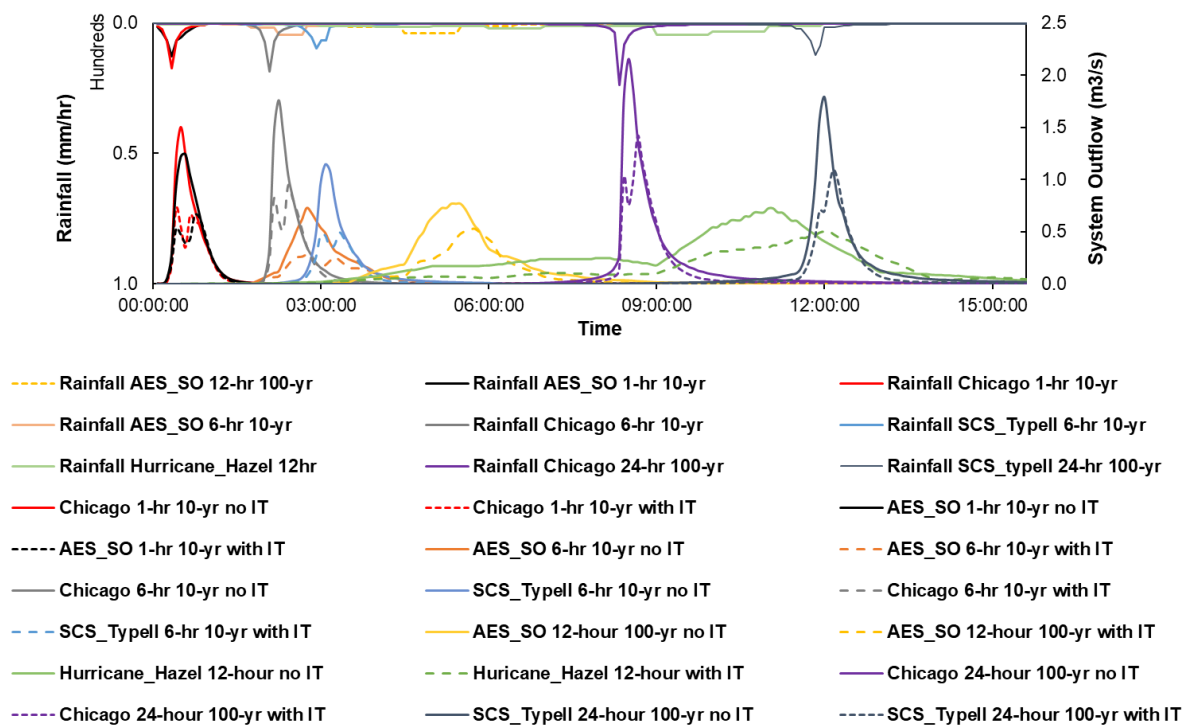


Figure 4.21 A comparison of hydrographs of the catchment outflow without and with LID (IT implemented in the four top-ranked subcatchments) under different rainfall patterns and durations

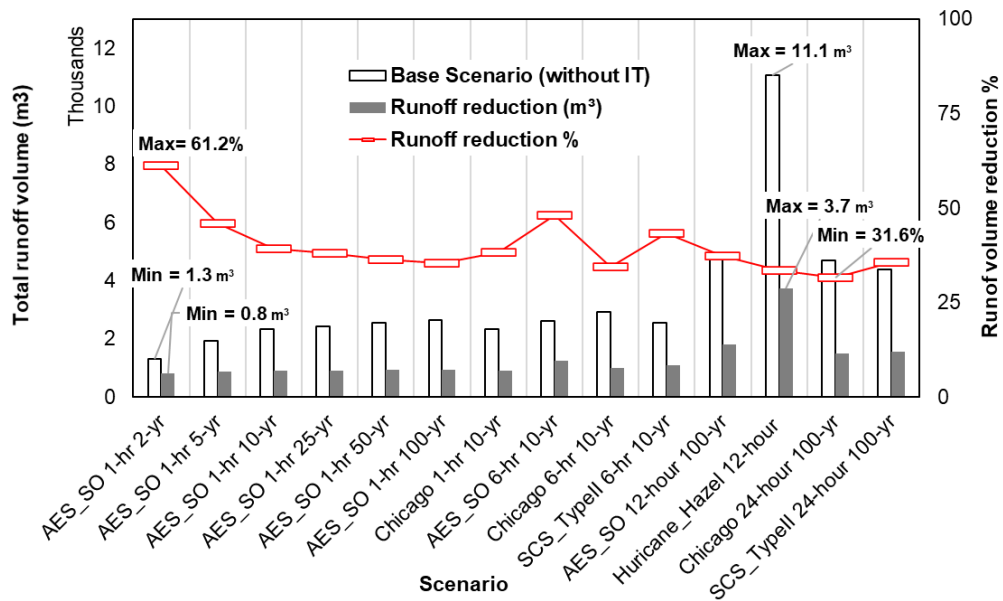


Figure 4.22 A comparison of the performance (volume and percentage runoff reduction) of LID (IT implemented in the four top-ranked subcatchments) under different rainfall patterns (AES_SO, Chicago, Hurricane Hazel, and SCS Type II), durations (1, 6, 12, and 24-hour), and return periods (2, 5, 10, 25, and 100 years)

Overall, in this section two parts of stormwater modelling were presented. First, the stormwater modeling of LID solution ranking by SERAH was conducted to examine its ability on ranking subcatchments. The results suggest that SERAH captures the potential of runoff generation of subcatchments and their demand for LID since implementing LID in the high-ranked subcatchments showed a higher performance (e.g., S13 and S19, S08, and S01). Second, the effect of different rainfall temporal patterns, duration and return periods on the LID solution suggested by SERAH (IT implemented in the first four high-ranked LID subcatchments) investigated. The results suggested that the selected LID solution exhibits a higher performance under severe rainfalls, however a high rainfall intensity can decrease the performance.

4.6. CONCLUSION

In this study, we addressed the gap of the lack of a systematic model for ranking LID solutions. To do so we developed a systematic and simplified geospatial model (referred to as SERAH), which can be used as input of stormwater models. This was conducted through the establishment of a geospatial relationship between the key contributing factors including LID benefits (hydrological, environmental-socioeconomic), cost, feasibility, and demand of the subcatchment. To examine the applicability of SERAH was applied to a catchment within the City of Toronto, located at eastern Don River.

The results showed that the hydrological-hydraulic index (HHI) effectively ranked the LID subcatchments and represented their potential in runoff generation. In our case study, which is a highly urbanized area, the contributing drainage area of the subcatchment was found to be an important variable in their ranks. The HHI ranking results were validated against a stormwater model. The stormwater modelling showed that implementing an equal area of IT (400 m²) in the individual subcatchments reduces the runoff from 46 to 100%. In prioritizing the types of LID, the cost of the LID type was identified as a key factor. However, the lateral benefits of LID can outweigh the cost if the demand for those benefits is high. For example, RG was more expensive than IT but was ranked the highest at three subcatchments due to its high lateral benefits. The geospatial methods for quantifying the lateral benefits of LID types effectively reflected the demand of subcatchments, yet there is a vast need for research in this area for quantifying the selected lateral benefits. Incorporating the lateral benefits of LID into the demand of subcatchments for these benefits allowed for the subcatchment-specific ranking of LID types. An example of the identified LID solution (IT considered for the first four top-ranked subcatchments)

was applied to the case study. The result showed that implementing an infiltration trench with a total area of 1600 m² (2.2 % of the study area) in the first four high-ranked subcatchments reduces the runoff volume by 39.1% and peak by 45%. The study of the influence of different rainfall patterns, frequency, and duration suggested that in response to higher runoff volumes LID exhibits a higher performance. However, the pattern of the rainfall (rainfall intensity) was shown to be an important factor in affecting the performance. LID was found to have a more effective performance in response to lower rainfall intensities (such as Hurricane Hazel).

SERAH efficiently prioritizes the subcatchment and types of LID and is applicable in all catchments (was not customized for a specific catchment). It is suitable for the strategic planning and detailed design phases of LID projects. SERAH integrates benefits of LID to the demand of subcatchments for LID. It provides us with information about the distribution of demands for LID across the catchment. SERAH identified future areas of research, particularly the incorporation of the non-hydrological aspects of LID into LID planning.

CHAPTER 5: INPUT DATA SOURCES AND SENSITIVITY ANALYSIS

5.1. PREFACE

This chapter includes two sections. The first section presents the data used in this research, the sources of data and discussion about the data gathering challenges. The second section investigates the effect of input data (parameters and weights) on the indices (HHI, LIDDI, HSE) suggested in this dissertation (chapters 2, 3 and 4).

5.2. INPUT DATA SOURCES AND SUMMARY INFORMATION

One of the main stages in this research was the geospatial data preparation and cleansing. The multiple resources of data, various reference coordinate systems and projections, and conflicting data classifications were challenging. A standard data repository platform (spatial data infrastructure) linking all these data will assist the end users with a more efficient data preparation and cleansing, access to the most suitable dataset, and reduces the duplication and redundancy of

data. Because of the diversity of the reference coordinate systems used for the different sets of data at the same location, the coordinate transformation was applied to tackle this issue. Also, there was a considerable inconsistency on the data interpretation and classification for the same set of data prepared by different organizations. For example, the land cover map of the three cities, Toronto, Montreal, and Vancouver has followed a significantly different ways of classification of land covers. Having an ontology for data classes (a unified terminology for data interpretation) will help the users with a more efficient understanding and synthesizing of the data.

The last and most important challenge was the inadequacy of the available data. This included inadequacy in the precision of the available data in representing the reality (e.g., data was too simplified to address the need of this research) as well as the amount of information that could be derived from a set of data. Out of all other reasons, this could be impacted by the common acceptable lack of precision which has various known sources (the discussion is out of the scope of this research); the extent of simplification of data (data represents rough information about the location (e.g., biodiversity data set for the City of Toronto provided us with a minimum required information); the age of data (data were old and have not been updated and revised), etc. In some cases of detailed data sets (less simplified), the amount of information that could be derived from was not adequate. For example, determining the saturated hydraulic conductivity of the surficial soil of the cities was a major challenge since it was not provided in many of the available geological data sets. One of the reasons causing this could be the need for data from multiple disciplines (hydrological- hydraulic, environmental, and socioeconomic), for stormwater management purposes.

A summary of datasets, their sources, and their characteristics are presented in Table 5.1 to 5.3. for City of Toronto, Montreal, and Vancouver, respectively. All these data were collected

from the publicly available data sources.

Table 5.1 The geospatial data used for Toronto, including a summary of the metadata and access links

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Toronto							
Air pollution (TPM2.5)	Government of Ontario, Ministry of Environment, Conservation and Parks	Monitoring air quality	2000-2021	Province of Ontario	Recording stations	CSV/HTML/XML	Temporal (hourly) Spatial (point data (stations))
Access link: http://www.airqualityontario.com/history/index.php							
Bedrock topography and overburden thickness mapping, southern Ontario	Ministry of Northern Development and Mines	This digital mapping initiative for southern Ontario was undertaken to determine the true nature of the bedrock surface both in thin-drift areas and in areas where overburden is thick in order to better understand both exposed and buried bedrock topographic features in relation to the known and/or inferred regional bedrock geology	2006	West Bounding Coordinate: -83° 29' East Bounding Coordinate: -74° 21' North Bounding Coordinate: 46° 01' South Bounding Coordinate: 41° 41'	Aerial Survey	SHP/Vector	0.005 decimal degree
Access link: http://www.mndm.gov.on.ca/en/mines-and-minerals/applications/ogsearch							
Census Tracts Boundary File	Government of Canada; Statistics Canada; Statistical Registers and Geography Division	Census tracts (CTs) are small, relatively stable geographic areas that usually have a population of less than 10,000, based on data from the previous Census of Population Program. They are located in census metropolitan areas and in census agglomerations that had a core population of 50,000 or more in the previous census	2004	West bound longitude: -180° East bound longitude: 180° North bound latitude: 89.999531° South bound latitude: 36.265059°	Census records	Vector/polygon	NA
Access link: http://www12.statcan.gc.ca/census-recensement/2011/geo/bound-limit/bound-limit-eng.cfm							

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Digital elevation model (DEM)	Ontario Ministry of Natural Resources and Forestry - Provincial Mapping Unit	The Ontario Digital Elevation Model (Imagery-Derived) is a raster elevation product that provides a generalized representation of both surface and ground features	2017, data is continually being updated	West longitude: -93.0983° East longitude: -78.871° North latitude: 50.568° South latitude: 41.3011°	Aerial photography	Raster	5 m (in 2017) (2 m in 2021)
Access link: https://geohub.lio.gov.on.ca/datasets/mnrf::ontario-digital-elevation-model-imagery-derived							
Ecozones of Ontario	Scholars Geoportal	Work is proceeding on many fronts to protect Canada's ecosystems. Activities include establishing protected areas to help conserve ecosystems and implementing species and habitat recovery programs. The federal government now provides tax incentives to individuals for donations of lands for conservation purposes. Industries such as forestry and agricultural are incorporating ecosystem management practices into their working practice.	2002	West Bounding Coordinate: -141° East Bounding Coordinate: -52° North Bounding Coordinate: 84° South Bounding Coordinate: 42°	Source Scale Denominator: 250000	Vector/polygon	0.000001 decimal degree
Access link: http://geo2.scholarsportal.info/proxy.html?http://_giseditor.scholarsportal.info/details/view.html?uri=/NAP/Geogratias_1991_1998_Ecoatlas.xml&show_as_standalone=true							

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Groundwater Level Time Series of the Oak Ridges Moraine	Groundwater Information Network (GIN)	This dataset exhibits the surficial geology of the Oak Ridges Moraine area, southern Ontario. The study area includes most of the Greater Toronto Area. This dataset presents groundwater level time series of monitoring sites from the Oak Ridges Moraine.	Dec-2011 to Dec-2012	West bound: 80.007888000° East bound: NA North bound: 44.108799000° 43.862067° South bound : 43.495759000°	The dataset comes from the Provincial Groundwater Monitoring Network (PGMN) from the Ministry of the Environment and Climate Change Ontario	Vector/point	1: 75000
Access link: https://gin.gw-info.net/service/api_ngwds:gin2/en/data/standard.download.html?THEME=5&BBOX=-79.829254,43.637329,-78.266449,44.186646							
Land cover for the City of Toronto, ONT	City of Toronto	This dataset was developed as part of the Urban Tree Canopy (UTC) Assessment for Toronto. As such, it represents a "top down" mapping perspective in which tree canopy over hanging other features is assigned to the tree canopy class. At the time of its creation this dataset represents the most detailed and accurate land cover dataset for the area	2007	West bound: 79.643724° East bound: 79.113286° North bound: 43.862067° South bound : 43.574826°	The primary sources used to derive this land cover layer were QuickBird satellite imagery (0.6 m) acquired in 2007.	Raster	0.6 m
Access link: https://open.toronto.ca/dataset/forest-and-land-cover/							

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Water course centerline in TRCA jurisdiction	Toronto and Region Conservation Authority (TRCA)	The data set is a line feature layer representing the approximate centerline of the river channel.	2017 (was used) 2021 (latest updated)	Top: 4,875,905.071300 m Bottom: 4,826,760.423200 m Left: 578,555.410900 m Right: 661,998.401100 m	Current orthophoto graphy as the base source, The update was using 2015 Lidar DEM and 2018 ortho photo	Vector/polyline	0.0001 m
Access link: https://data.trca.ca/dataset/watercourses-trca							
Surficial Geology of Southern Ontario	Government of Canada	This data provide a detailed overview of the surficial geology of provinces including southern Ontario and associated attributes available to the land-use planning, consulting, aggregate/industrial mineral industry and development community as well as government geoscientists, resource scientists, conservation authorities, land-use planners and academic researchers.	2010	North bound: 46° 00' South bound: 42° 00' West bound: -83° 00' East bound: -74° 00'	OGS Hard copy Quaternary geology maps by Ontario Geological Survey, Ministry of Northern Development and Mines	Vector/polygon	1:50 000
Access link: http://open.canada.ca/data/en/dataset/a75c3d6c-354d-436d-999d-431fb3a9de79							

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Precipitation data	The Institute for Catastrophic Loss Reduction	This data is prepared to generate local IDF curve information that accounts for the possible impacts of climate change. It applies a user-friendly GIS interface and provides precipitation accumulation depths for a variety of return periods (2, 5, 10, 25, 50 and 100 years) and durations (5, 10, 15 and 30 minutes and 1, 2, 6, 12 and 24 hours), and allows users to generate IDF curve information based on historical data, as well as future climate conditions that can inform infrastructure decisions.	Temporal data up to 2017(about 10 years)	800 Environment and Climate Change Canada operated rain stations from across Canada	Gridded dataset produced for the IDF_CC tool [225]	Vector/p oint	NA
Access link: https://www.idf-cc-uwo.ca/home							
Educational institute	City of Toronto	NA	NA	NA	NA	KML	NA
Access link: https://www.google.com/maps/search/toronto+ Educational institute							
Toronto Hospitals	City of Toronto	NA	NA	NA	NA	KML	NA
Access link: https://www.google.com/maps/search/toronto+hospitals							
Flood vulnerable areas	Toronto and Region Conservation Authority (TRCA)	NA	NA	NA	TRCA	PDF	NA
Access link: https://data.trca.ca/dataset/flood-vulnerable-cluster							

Table 5.2 The geospatial data used for Montreal, including the type of data, the format, and the source of data

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Montreal							
Digital elevation model (DEM)	City of Montreal	This data set is the Montreal Digital Elevation Model is a raster elevation product that provides a generalized representation of both surface and ground features.	2015-11-24 to 2015-12-08	West bound: - 73.995838° East bound: - 73.458903° North bound: 45.706882° South bound: 45.391025°	LiDAR data (Point Cloud) acquired in partnership with the city of Montreal.	Raster	1 m
Access link: https://ftp.maps.canada.ca/pub/elevation/dem_mne/highresolution_hauteresolution/dtm_mnt/1m/VILLE_MONTREAL/VILLE_MONTREAL/thumbnail/							
Groundwater	Gouvernement of Quebec	This data set is prepared to include the drilling reports transmitted by drilling companies, drilling teams from the Ministry of Natural Resources, and unknown well diggers, or geotechnical drilling carried out by the Ministry of Transport	1978 to 2019	North bound: 2,728,943.753180 m South bound: 2,666,255.978993 m West bound: 1,709,015.306867 m East bound: - 1,767,673.263497 m	European Petroleum Survey Group (EPSG)	Vector/polygon	1: 10 000
Access link: http://www.sih.environnement.gouv.qc.ca/inforesultats.php#lithologie							
Land Cover	Metro Montreal	The data is to present land use of the Montreal, as compiled by the CMM for all of its territory on the land use mapping, version 2016, using a methodology, a classification and segmentation rules of its own.	2016	West bound: 265,961.230900 m East bound: 306,814.230900 m North bound: 5,063,078.067800 m South bound: 5,027,324.067800 m	The data land use numbers are those used for the production of the 97 fact sheets. the land use mapping	Vector/polygon	1: 1000
Surficial geology and saturated hydraulic conductivity (K _s)	The same data source used for Toronto						
Precipitation data	Same data source used for Toronto						

Table 5.3 The geospatial data used for Vancouver, including the type of data, the format, and the source of data

Official name	Owner	Purpose for Collecting	Time Coverage	Spatial Coverage	Data source	Format	Resolution
Vancouver							
Digital elevation model (DEM)	City of Vancouver	The data include the Digital Elevation Model (DEM) data coverage up to extents of City of Vancouver's legal jurisdiction	2013	West bound: 483,639.100000 m East bound: 498,326.600000 m North bound: 5,463,000.430000 m South bound: 5,449,435.930000 m	LiDAR data	Raster	1 m
Access link: https://opendata.vancouver.ca/explore/embed/dataset/open-data-change-log/log/?disjunctive.datasets&sort=logdate&refine.datasetids=digital-elevation-model&refine.datasets=Digital%20elevation%20model							
Groundwater	Province of British Columbia	The data presents the well data including the active with real -time, active without real-time, and inactive	2017 to 2019	West bound: 487,075.983400 m East bound: 496,523.967700 m North bound: 5,458,148.955300 m South bound: 5,449,778.012900 m	European Petroleum Survey Group (EPSG)	Vector/p oint	1: 1000
Access link: https://governmentofbc.maps.arcgis.com/apps/webappviewer/index.html?id=b53cb0bf3f6848e79d66ffd09b74f00d							
Land Cover	City of Vancouver	The data is to create a Canada wide topographic dataset which can be used for cartographic display, facilities management, and location-based services	2014	West bound: 479,351.596508 m East bound: 500,227.798140 m North bound: 5,463,416.209166 m South bound: 5,445,137.327789 m	DMTI Spatial Inc.	Vector/p olygon	
Access link: http://www.metrovancouver.org/metro2040/land-use-designation/Pages/default.aspx							
Surficial geology and saturated hydraulic conductivity (K_s)	The same data source used for Toronto						
Precipitation data	The same data source used for Toronto						

5.3. THE SENSITIVITY ANALYSIS FOR INPUT DATA (PARAMETERS AND WEIGHTS)

This section includes the sensitivity analysis of the input data (parameters and weights) of the models and indices developed in this dissertation (HHI, LIDDI, HSE). Sensitivity analysis methods investigate the effect of possible errors in input data on the model outputs. Meaning that sensitivity analysis methods are used to exhibit the impact of alternative assumptions of the modelling process through visualization and numerical analysis [226]. There are a variety of methods for sensitivity analysis. The most conventional method tests the model based on changing one parameter at a time and assuming other inputs are constant. Also, there exist other different methods that test the combined effect of the input data which are not considered in this study [226].

To investigate the sensitivity analysis, we applied it to an artificial catchment. This catchment was discretized into 25 square-shaped subcatchments represented in Figure 5.1 (a), with an assumed flow direction (Figure 5.1 (b)). Among all 25 subcatchments, 10 feasible subcatchments were randomly selected as the subcatchments which layouts are present in Figure 5.1 (c).

The geospatial characteristic of the catchment including slope (S), rainfall (R), hydraulic conductivity (Ks), depth to groundwater table (Dg), depth to restrictive soil layer (Dr), environmental demand indices (assumed to be four indices), socioeconomic demand indices (assumed to be four indices) were randomly generated through random functions for all 25 subcatchments (C01 to C25). The minimum and maximum values for S, R, Ks, n, Dg,

and Dr were generated based on the actual data from the city of Toronto [152]. However, the range of environmental and socioeconomic indices was considered to fall between 0 and 1, which overall led to eight different random layers (four for environmental and four for socioeconomic). Also, in our conceptual model, we compare three arbitrary LID types. These LID types are assumed to have three different costs (normalized between 0 and 1), and eight benefits. Each benefit was assumed to be a corresponding benefit to a demand of the artificial catchment. These benefits also were randomly generated which resulted in assigning eight values to each LID type.

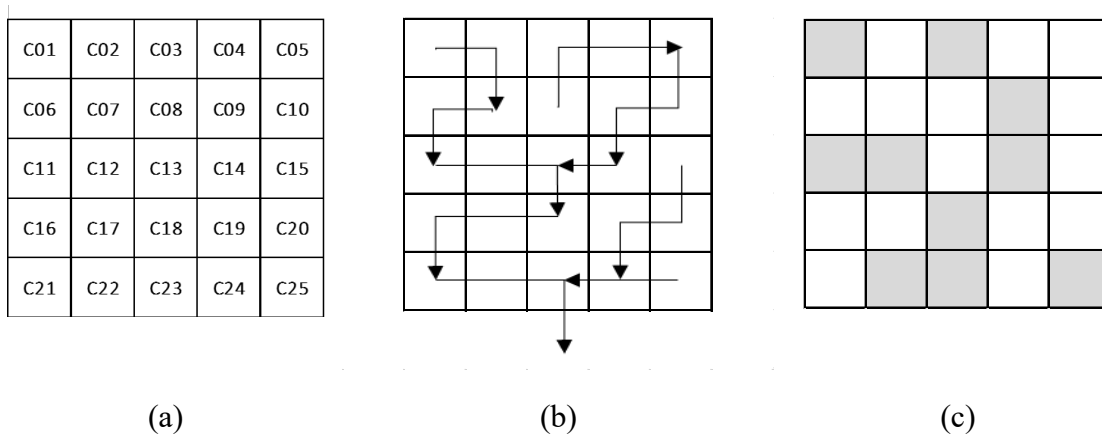


Figure 5.1 the characteristics of the conceptual model including (a) The layout of the catchment and assigned name of the subcatchments (b) The direction of flow (black arrows) to the outlet (c) feasible subcatchments (grey)

The base scenario was randomly generated in the range of actual data of the City of Toronto. The sensitivity analysis was performed considering a -30 %, -20 %, -10 %, +10 %, +20 %, and +30 % change in the input data (the deviation from the input data of the base scenario) [227] [228]. The sensitivity analysis was conducted in four stages: First, generating 875 subcatchments' data for exploring the impact of Rainfall (R), hydraulic conductivity

(Ks), Depth to restrictive layer (Dr), porosity (n), and Slope (S) on HHI. Second, the impact of changes in HHI in combined with constant environmental (ENI) and socioeconomic benefit (SEI) on LIDDI has been studied as well as the correlation of these data with LIDDI. Third, three types of LID and their benefits and cost were generated randomly. Then the impact of change of the input data on the HSE was examined. Fourth, the weights used for combining HHCI and SEI were changed from 10 to 100 percent by 10 percent intervals. Then, the effect of the change of these weights on the HSE was explored.

5.3.1. HHI sensitivity to input parameters

The sensitivity of HHI to the five input parameters (rainfall, slope, porosity (n), depth to restrictive layer (Dr), and hydraulic conductivity (Ks)) was explored. To do so, 6 scenarios for each input parameter were generated including -30 %, -20 %, -10 %, +10 %, +20 %, and +30 % change in the input parameter. Table 5.4 and Table 5.5 present the summary of the results. Including the scenario ID, the average value of each parameter per catchment for each scenario, percent change of the average and standard deviation of the output (HHI and LIDDI). The results suggest that the sensitivity of HHI to the rainfall (R) and the hydraulic conductivity (Ks) is the most, with Ks slightly lower than the R. It showed that HHI is marginally sensitive to the slope (for -30 % change in slope the HHI decreased approximately 4 percent). Also, the sensitivity of HHI to Dr and n was the least since the Ks outweighed these values in the relationship and was always the minimum value. Since these parameters represent the infiltration rate similar to Ks the sensitivity of HHI to Dr is identical to the Ks if they outweigh the Ks. Figure 5.2 presents the relationship between HHI and each of the

input parameters to investigate the correlation between these data. The plots presented in Figure 5.2 agree with the findings of Table 5.4 and Table 5.5. They exhibit a strong correlation between HHI and R as well as HHI and Ks. This correlation confirms the high sensitivity of HHI to R and Ks parameters.

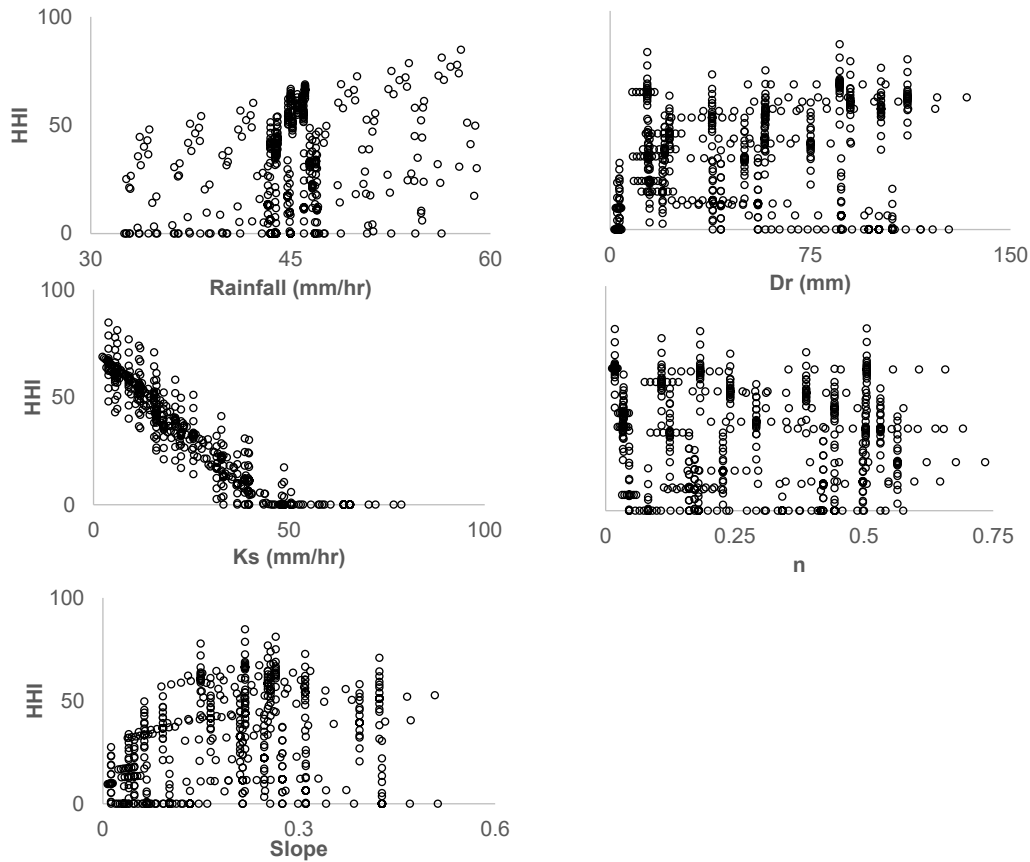


Figure 5.2 HHI versus the input data (Rainfall, Hydraulic conductivity (Ks), Slope, Depth to restrictive layer (Dr,), and porosity n)

Table 5.4 The impact of -30, -20, -10, 10, 20, 30 percentage changes in input data on the average of HHI compared to the base scenario

Scenario	Average of rainfall	Average of slope	Average of Dr	Average of n	Average of Ks	Average of HHI
R -30%	33.70	0.20	52.35	0.28	28.48	-43.75%
R -20%	37.48	0.20	52.35	0.28	28.48	-30.96%
R -10%	41.26	0.20	52.35	0.28	28.48	-15.99%
Base	45.05	0.20	52.35	0.28	28.48	
R +10%	48.83	0.20	52.35	0.28	28.48	16.49%
R +20%	52.61	0.20	52.35	0.28	28.48	34.13%
R +30%	56.40	0.20	52.35	0.28	28.48	52.47%
S -30%	45.05	0.14	52.35	0.28	28.48	-4.39%
S -20%	45.05	0.16	52.35	0.28	28.48	-2.82%
S -10%	45.05	0.18	52.35	0.28	28.48	-1.36%
S +10%	45.05	0.22	52.35	0.28	28.48	1.27%
S +20%	45.05	0.24	52.35	0.28	28.48	2.48%
S +30%	45.05	0.26	52.35	0.28	28.48	3.62%
Dr -30%	45.05	0.20	36.65	0.28	28.48	0.00%
Dr -20%	45.05	0.20	41.88	0.28	28.48	0.00%
Dr -10%	45.05	0.20	47.12	0.28	28.48	0.00%
Dr +10%	45.05	0.20	57.59	0.28	28.48	0.00%
Dr +20%	45.05	0.20	62.82	0.28	28.48	0.00%
Dr +30%	45.05	0.20	68.06	0.28	28.48	0.00%
n -30%	45.05	0.20	52.35	0.20	28.48	0.00%
n -20%	45.05	0.20	52.35	0.22	28.48	0.00%
n -10%	45.05	0.20	52.35	0.25	28.48	0.00%
n +10%	45.05	0.20	52.35	0.31	28.48	0.00%
n +20%	45.05	0.20	52.35	0.33	28.48	0.00%
n +30%	45.05	0.20	52.35	0.36	28.48	0.00%
Ks -30%	45.05	0.20	52.35	0.28	19.94	33.73%
Ks -20%	45.05	0.20	52.35	0.28	22.79	21.61%
Ks -10%	45.05	0.20	52.35	0.28	25.63	9.82%
Ks +10%	45.05	0.20	52.35	0.28	31.33	-9.01%
Ks +20%	45.05	0.20	52.35	0.28	34.18	-16.89%
Ks +30%	45.05	0.20	52.35	0.28	37.03	-22.82%

Table 5.5 The impact of -30, -20, -10, 10, 20, 30 percentage changes in input data on the standard deviation of HHI compared to the base scenario

Scenario	StdDev of rainfall	StdDev of slope	StdDev of n	StdDev of Dr	StdDev of Ks	StdDev of HHI
R -30%	0.81	0.12	0.18	36.78	17.86	-24.62%
R -20%	0.95	0.12	0.18	36.78	17.86	-14.69%
R -10%	1.08	0.12	0.18	36.78	17.86	-6.96%
Base	1.22	0.12	0.18	36.78	17.86	
R +10%	1.35	0.12	0.18	36.78	17.86	6.70%
R +20%	1.49	0.12	0.18	36.78	17.86	11.85%
R +30%	1.62	0.12	0.18	36.78	17.86	16.02%
S -30%	1.22	0.09	0.18	36.78	17.86	-4.64%
S -20%	1.22	0.10	0.18	36.78	17.86	-2.97%
S -10%	1.22	0.11	0.18	36.78	17.86	-1.43%
S +10%	1.22	0.13	0.18	36.78	17.86	1.35%
S +20%	1.22	0.15	0.18	36.78	17.86	2.62%
S +30%	1.22	0.16	0.18	36.78	17.86	3.83%
Dr -30%	1.22	0.12	0.18	25.74	17.86	0.00%
Dr -20%	1.22	0.12	0.18	29.42	17.86	0.00%
Dr -10%	1.22	0.12	0.18	33.10	17.86	0.00%
Dr +10%	1.22	0.12	0.18	40.46	17.86	0.00%
Dr +20%	1.22	0.12	0.18	44.13	17.86	0.00%
Dr +30%	1.22	0.12	0.18	47.81	17.86	0.00%
n -30%	1.22	0.12	0.13	36.78	17.86	0.00%
n -20%	1.22	0.12	0.14	36.78	17.86	0.00%
n -10%	1.22	0.12	0.16	36.78	17.86	0.00%
n +10%	1.22	0.12	0.20	36.78	17.86	0.00%
n +20%	1.22	0.12	0.22	36.78	17.86	0.00%
n +30%	1.22	0.12	0.24	36.78	17.86	0.00%
Ks -30%	1.22	0.12	0.18	36.78	12.50	-12.15%
Ks -20%	1.22	0.12	0.18	36.78	14.29	-7.33%
Ks -10%	1.22	0.12	0.18	36.78	16.08	-2.31%
Ks +10%	1.22	0.12	0.18	36.78	19.65	1.74%
Ks +20%	1.22	0.12	0.18	36.78	21.44	2.60%
Ks +30%	1.22	0.12	0.18	36.78	23.22	1.45%

5.3.2. LIDDI sensitivity to input parameters

LIDDI is generated from the HHI, SEI and ENI as presented in Chapter 2. The change in input parameters led to a change in HHI and consequently change in LIDDI. To investigate this change, SEI and ENI were remained unchanged for all scenarios and LIDDI was generated in Table 5.6 presents the summary of the analysis. The results revealed that change in HHI causes an identical change in LIDDI. It was deduced from both average and standard deviation values of HHI and LIDDI. Thus, any change in the input parameters R, S, Ks, Dr, and n will have a direct impact on LIDDI as HHI. Correlation between LIDDI versus HHI, SEI1 to SEI 4, and ENI1 to ENI 4 was explored by plotting these data. Figure 5.3 shows the results, which suggest a strong correlation between LIDDI and HHI. This confirms the findings of the earlier sensitivity analysis (Table 5.6).

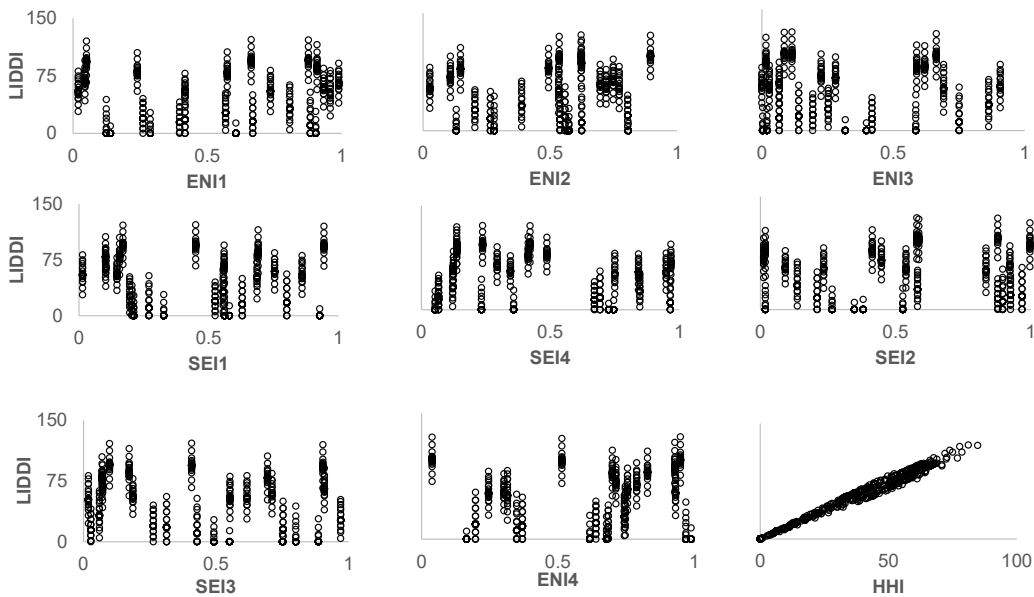


Figure 5.3 LIDDI versus the input data HHI, ENI1-4 and SEI1-4

Table 5.6 The impact of HHI changes on LIDDI compared to the base scenario

Scenario	ENI1	ENI2	ENI3	ENI4	SEI1	SEI2	SEI3	SEI4	Average of HHI	% change of average of HHI	Average of LIDDI	% change of average of LIDDI	StdDev of LIDDI	% change of StdDev of LIDDI
R -30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-43.75%	-43.75%	24.12	-43.91%	25.62	-24.59%
R -20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-30.96%	-30.96%	29.64	-31.08%	29.00	-14.66%
R -10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-15.99%	-15.99%	36.08	-16.09%	31.64	-6.89%
Base	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47			43.00		33.98	
R +10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	16.49%	16.49%	50.13	16.57%	36.25	6.68%
R +20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	34.13%	34.13%	57.72	34.22%	38.04	11.94%
R +30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	52.47%	52.47%	65.61	52.56%	39.50	16.23%
S -30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-4.39%	-4.39%	41.12	-4.37%	32.43	-4.58%
S -20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-2.82%	-2.82%	41.80	-2.80%	32.98	-2.93%
S -10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-1.36%	-1.36%	42.42	-1.35%	33.50	-1.42%
S +10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	1.27%	1.27%	43.55	1.27%	34.43	1.33%
S +20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	2.48%	2.48%	44.06	2.47%	34.86	2.58%
S +30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	3.62%	3.62%	44.55	3.60%	35.26	3.77%
Dr -30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Dr -20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Dr -10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Dr +10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Dr +20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Dr +30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n -30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n -20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n -10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n +10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n +20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
n +30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	0.00%	0.00%	43.00	0.00%	33.98	0.00%
Ks -30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	33.73%	33.73%	57.53	33.79%	29.95	-11.85%
Ks -20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	21.61%	21.61%	52.33	21.68%	31.54	-7.18%
Ks -10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	9.82%	9.82%	47.27	9.91%	33.19	-2.32%
Ks +10%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-9.01%	-9.01%	39.08	-9.12%	34.60	1.83%
Ks +20%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-16.89%	-16.89%	35.68	-17.02%	34.88	2.65%
Ks +30%	0.54	0.51	0.33	0.61	0.46	0.51	0.47	0.47	-22.82%	-22.82%	33.11	-23.01%	34.49	1.49%

5.3.3. HSE sensitivity to input parameters

HSE sensitivity analysis was conducted using the same catchment as the previous steps. To calculate HSE three random LID types were generated with eight benefits. These benefits are corresponding to the eight LID demands (SEI1 to SEI4 and ENI1 to ENI4). All benefits and demands are assumed to be normalized between 0 and 1. Table 5.7 presents a comparison between the three random LID types. It shows that the maximum of benefits is 2/8 for LID1 2/8 for LID2 and 5/8 for LID3. LID1 is the most expensive and LID3 is the least expensive type. In this step, the impact of change in input data (R, S, Ks, Dr, n) on the HSE1 to HSE3 was investigated and the weight of HHCI and SEI were considered equal. Following this, in the next step, the impact of weights of HHCI and SEI on HSE was explored. Table 5.7 shows the summary of the analysis by presenting the change in average and standard deviation of HSE1 to HSE3 against the change in HHI. The results suggest that change in HHI has the maximum impact on the average of HSE3 and the minimum impact on the average of HSE1. It also shows that the standard deviation had not significantly changed and is similarly the highest for HSE3 and the lowest for HSE1. The extent of the impact of HHI seems to be related to the cost of LID type. The lowest the cost the highest the sensitivity to change in the input data

Table 5.7 The cost and benefit comparison among the three selected LID types (LID1 to LID3)

LID ID	Benefit1	Benefit2	Benefit3	Benefit4	Benefit5	Benefit6	Benefit7	Benefit8	Cost
LID1	0.417022	0.302333	0.18626	0.538817	0.204452	0.670468	0.140387	0.968262	1.2
LID2	0.720324	0.146756	0.345561	0.419195	0.878117	0.417305	0.198101	0.313424	0.6
LID3	0.000114	0.092339	0.396767	0.68522	0.027388	0.55869	0.800745	0.692323	0.12

Table 5.8 The impact of HHI changes on a mean and standard deviation of HSE of the three selected types of LID

Scenario	Scenario	Average of HHI	StdDev of HHI	Average of hse_lid1	Average of hse_lid2	Average of hse_lid3	StdDev of hse_lid1	StdDev of hse_lid2	StdDev of hse_lid3
Sc01	R -30%	-43.75%	-24.62%	-0.63%	-1.22%	-4.79%	-0.19%	-4.63%	-8.38%
Sc02	R -20%	-30.96%	-14.69%	-0.46%	-0.89%	-3.48%	-0.69%	-3.69%	-6.68%
Sc03	R -10%	-15.99%	-6.96%	-0.22%	-0.43%	-1.70%	-0.65%	-1.98%	-3.50%
Sc04	Base								
Sc05	R +10%	16.49%	6.70%	0.20%	0.38%	1.50%	1.00%	2.20%	3.64%
Sc06	R +20%	34.13%	11.85%	0.40%	0.77%	3.03%	2.51%	4.72%	7.52%
Sc07	R +30%	52.47%	16.02%	0.59%	1.14%	4.47%	3.80%	7.04%	10.97%
Sc08	S -30%	-4.39%	-4.64%	0.00%	-0.01%	-0.03%	-0.03%	-0.06%	-0.05%
Sc09	S -20%	-2.82%	-2.97%	0.00%	0.00%	-0.02%	-0.02%	-0.04%	-0.03%
Sc10	S -10%	-1.36%	-1.43%	0.00%	0.00%	-0.01%	-0.01%	-0.02%	-0.02%
Sc12	S +10%	1.27%	1.35%	0.00%	0.00%	0.01%	0.01%	0.02%	0.01%
Sc13	S +20%	2.48%	2.62%	0.00%	0.00%	0.01%	0.02%	0.03%	0.03%
Sc14	S +30%	3.62%	3.83%	0.00%	0.01%	0.02%	0.02%	0.05%	0.04%
Sc15	Dr -30%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc16	Dr -20%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc17	Dr -10%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc19	Dr +10%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc20	Dr +20%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc21	Dr +30%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc22	n -30%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc23	n -20%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc24	n -10%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc26	n +10%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc27	n +20%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc28	n +30%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Sc29	Ks -30%	33.73%	-12.15%	0.53%	1.02%	4.00%	3.61%	5.85%	8.82%
Sc30	Ks -20%	21.61%	-7.33%	0.59%	1.15%	4.50%	3.82%	7.08%	11.06%
Sc31	Ks -10%	9.82%	-2.31%	0.27%	0.51%	2.02%	1.49%	3.05%	4.97%
Sc33	Ks +10%	-9.01%	1.74%	-0.25%	-0.48%	-1.89%	-0.72%	-2.18%	-3.86%
Sc34	Ks +20%	-16.89%	2.60%	-0.46%	-0.90%	-3.51%	-0.71%	-3.74%	-6.80%
Sc35	Ks +30%	-22.82%	1.45%	-0.60%	-1.16%	-4.56%	-0.35%	-4.55%	-8.29%

5.3.4. Sensitivity of the result of SERAH to weights of HHCI and SEI

The impact of the selected weights on the rank of the LID types was investigated by changing the weight of HHCI and SEI. The weight of HHCI was started with 0.1 to 1.0 by 0.1 intervals. The sum of the weights was 1.0, so the weight of SEI was decreased from 0.9 to 0.0 by 0.1 intervals. As a result, 10 scenarios were generated and compared to the base scenario (equal weights for HHCI and SEI, weights = 0.5). The summary of the results is presented in Table 5.9 and Figure 5.4 The impact of HHCI and SEI weights on the HSE values. Table 5.9 presents how the rank of each LID type has change (e.g., -1 means that LID has down-ranked by 1, and 1 means that LID is up-ranked by 1 compared to the base scenario). Overall, the change in weights about $\pm 20\%$ (HHCI weights = 0.3 to 0.7) has not changed the ranks significantly. The changes $\pm 30\%$ had a mild effect on the ranks. However, $\pm 40\%$ of the change in the weights had a significant impact on the ranks of LID3, where the variation of the rank in this type of LID is the highest among all. Thus, the rank of LID3 is the most sensitive compared to the other two types. The reason is related to the cost of this type of LID. Wherein the HHCI weight is the maximum, the rank of LID3 increases significantly. The results suggest that with increasing the weight of HHCI, the rank of the unexpensive LID (LID3) increases whereas decreasing the weight of HHCI, outweighs the lateral benefit of LID1 to its cost and gives this type of LID a higher rank.

The variation of SEI of the three LID types is presented in Figure 5.4, which agrees with these results. This figure shows that the value of HSE increases for LID3 (grey colour solid lines) dramatically with higher weights. It also suggests that LID3 is the most sensitive

to the weights compared to the other two types.

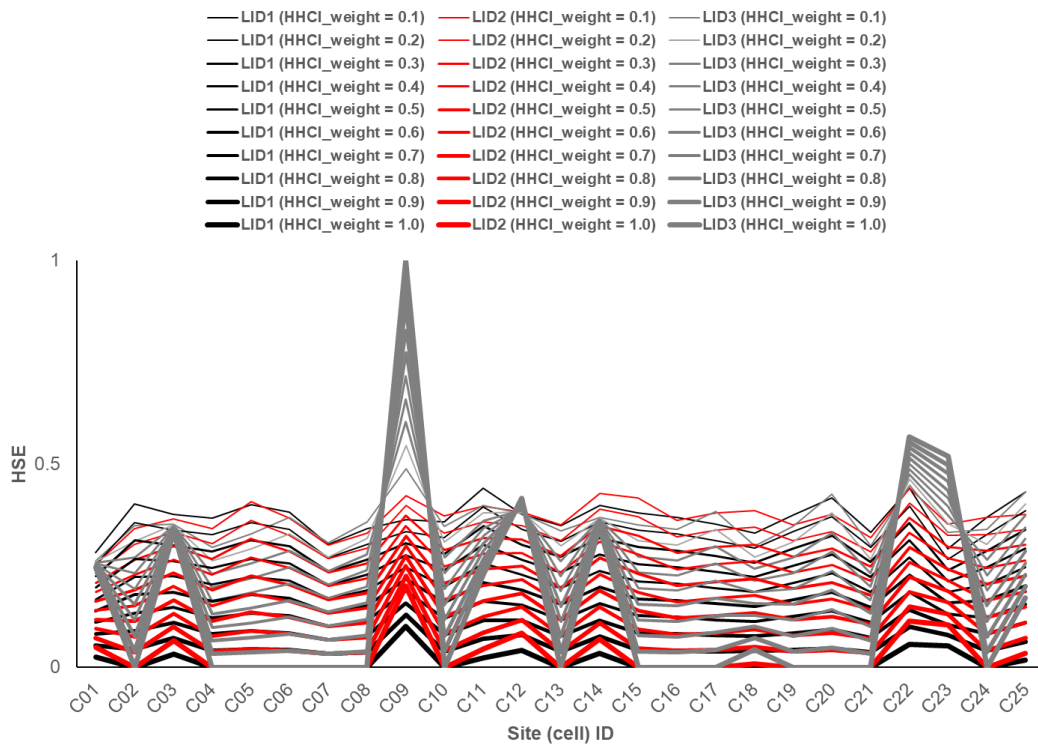


Figure 5.4 The impact of HHCI and SEI weights on the HSE values

Table 5.9 The impact of weight of HHCI and SEI on the rank of LID types in different subcatchments (cells) compared with the base scenario (equal weights for HHCI and SEI = 0.5)

CellID	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3	LID1	LID2	LID3						
	HHCI Weights																																									
	0.1	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4	0.4	0.5	0.5	0.5	0.6	0.6	0.6	0.7	0.7	0.7	0.8	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.0												
C01	-1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0						
C02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
C03	-2	0	2	-1	1	0	-1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
C04	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0				
C05	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0				
C06	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0			
C07	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	-1	2	0			
C08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	-1	2	0			
C09	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
C10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0	0			
C11	-1	0	1	-1	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0	1	-1	0			
C12	0	-1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
C13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0	0			
C14	-1	-1	2	0	-1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
C15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0	0			
C16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
C17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
C18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	-1	1	0	-1	1	1	1	-2	1	1	-2	1	1	-2	1	1	-2	1	1	-2	1	-2	0		
C19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
C20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	-1	2	0	0		
C21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
C22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
C23	0	-1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
C24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
C25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

5.4. CONCLUSION

This chapter presents, first, the challenges related to the input data, the sources, and the summary of the metadata used for this research. Second, the sensitivity of the input data (parameters and weights) on the output of the suggested models and corresponding indices (HHI, LIDDI, and HSE) are investigated. Generally, the data gathering and cleansing still are challenging processes due to some drawbacks such as the multiple resources of data, reference coordinate systems and projections, and conflicting data classification. The concern about the accuracy of the input data led our research to investigate the sensitivity of the output on the input data. This investigation was performed through a synthetic catchment and random dataset.

The sensitivity analysis for -30 %, -20 %, -10 %, +10 %, +20% , +30% change in input data (rainfall, slope, D_r , n , K_s) showed that the HHI is the most sensitive to rainfall and least sensitive to the slope. LIDDI has a linear relationship to HHI, therefore the impact of rainfall on LIDDI is identical to HHI. The effect of change in HHI on the rank of LID types suggested that the magnitude of the impact is related to the cost of LID type. The lowest the cost the highest the sensitivity to change in the input data. The sensitivity of the HSE to the weights by changing the weight of HHCI from 0.1 to 1.0 by 0.1 intervals was compared with the base scenario of equal weights for HHCI and SEI. Thus, the results showed that the rank of LID3 is the most sensitive compared to the other two due to the cost of LID3. Wherein the HHCI weight is the maximum the rank of LID3 increases and vice versa. This result is aligned with the results of Chapter 4 which suggested the cost of LID is an important parameter in the determination of the rank.

CHAPTER 6: CONCLUSION

This chapter in three sections provides the summary on the major conclusions from each chapter, presents the novel contributions of this dissertation, and recommendations for future research.

6.1. GENERAL CONCLUSIONS

The overall objective of this dissertation was to develop a novel GIS-based LID framework for sustainable urban runoff management and using LID techniques. This objective was reached by dividing it into three sub-objectives: i) developing a simplified geospatial index for ranking LID subcatchments, ii) applying the proposed index under climate change and urbanization, iii) developing a simplified geospatial model for ranking LID solutions, which also included a comprehensive review on LID models. The major conclusions of each objective are provided below.

6.1.1. Developing a simplified geospatial index for ranking LID subcatchments

In Chapter 2 a simplified geospatial index was developed to rank the subcatchments within a study area. The index was generated through an innovative framework and determines the rank of subcatchments using the physics of the runoff generation phenomenon and a GIS-based MCDM model. In this Chapter, the contributing criteria to the decision were comprehensively identified, quantified, and integrated through geospatial analysis. The data preparation and cleansing were performed using an automated process through developed scripts in Python.

The framework ranked the study area by generating the LID Demand Index (LIDDI). LIDDI ranks the subcatchments of the study area based on the three proposed indices: Hydrological-Hydraulic Index (HHI), Environmental Index (ENI), and Socioeconomic Index (SEI). Subcatchments with high LIDDI have a high rank for implementing LID. HHI indexes the study area based on the potential of subcatchments in runoff generation using a novel and heuristic physical-based geospatial relationship that was proposed in this chapter. HHI was validated by comparing the GIS-generated results against the results of a hydrological model (HEC-HMS) and historical flood-vulnerable locations within the study area. High ENI and SEI in a subcatchment represent a high environmental and socioeconomic demand for LID. HHI, ENI, and SEI were integrated through a second heuristic equation which considered the lateral benefit (SEI and ENI) as an additive value to the primary benefit (HHI). Also, a sensitivity analysis (as presented in Section 5.3) was performed to investigate the impact of the change in input data (parameters and weights) on the HHI and LIDDI.

LIDDI was generated for the City of Toronto. The results showed that the developed

indices offer multiple advantages. LIDDI resolved the lack of a knowledge-based decision-making system for identifying high-rank subcatchments for implementing LID. LIDDI creates a novel index for the runoff reduction benefit of LID, HHI, and integrates it into the indices generated for lateral benefits of LID (environmental and socioeconomic). The integration of an HHI into lateral benefits through MCDM and heuristic relationships suggests an innovative approach. The data required to generate LIDDI are publicly available, which facilitates the wider use of the framework. The framework is not limited to the scale of the study area and modelling multiple scales (micro-, meso-, and mega-scale) is feasible. This is a significant advantage for modelling city-scale study areas for narrowing down the decision of which subcatchments need to have LID implemented. It accepts the actual values of data and does not require modification or customization of data to generate the indices. Lastly, the developed model is universal and is not limited to a certain study area. Thus, it can be used in any study area or region of interest.

6.1.2. Applying the proposed index under climate change and urbanization

In Chapter 3 using the application of the novel hydrological-hydraulic index (HHI) developed in Chapter 2 was investigated. This investigation also lends itself to studying the impact of climate change and urbanization on the potential of runoff generation (demand for LID) for three Canadian cities (Toronto, Montreal, and Vancouver). The study considered twelve combinations of climate change and urbanization scenarios to cover a wide range of possible future conditions. The combinations were created from four climate change scenarios (considering historical precipitation data as the “base” scenario and three projected

precipitation data for the years 2006 to 2036, 2066, and 2096). Also, three urbanization scenarios, “base” scenario (based on the current land cover status), Scenario 1 (medium urbanization), and Scenario 2 (high urbanization). The variety of case studies (three Canadian cities) having different climate and urbanization statuses increased the breadth of these variables under the investigation.

Overall, the results of this Chapter agreed with previous findings of the impact of urbanization and climate change on runoff generation. This result represented the overall demand for LID. A comparison among all three cities showed that for a status of urbanization and climate, Toronto and Montreal have a higher demand for LID compared with Vancouver. Also with time, the magnitude of increase in demand for LID was higher for these cities and lower for Vancouver. The extent of the impact of future scenarios was a function of the current permeability of the city and the rainfall intensity. These parameters (rainfall intensity and current permeability) determine the change in which future factor (urbanization/climate change) has a higher effect on runoff generation. Unlike Vancouver with low rainfall intensity, in Toronto and Montreal climate change is the key factor compared with the urbanization. Unlike these cities, in Vancouver, it was found that HHI is sensitive to both urbanization and climate change. In this Chapter, it was revealed that climate change increases the mean HHI of all three cities in contrast to urbanization which causes an increase in HHI frequency. Meaning that with time demand for LID will increase but the magnitude of this change varies depending on the case study. The mean HHI in Toronto and Montreal more dramatically raised compared with Vancouver. Because these cities have high-intensity rainfall compared with Vancouver with lower rainfall intensity. The change in frequency of HHI (representing the increase in the number of subcatchments that demand LID) was

affected by the current permeability status of the cities. The high current impermeability leaves lower room for a raise in HHI.

Modelling city-scale study areas through traditional stormwater models is associated with complexity due to numerous input data including LID subcatchments, constant urban change (and growth), global climate change, and the non-uniform spatial distribution of land cover and rainfall. This chapter overcame this complexity through an innovative index (HHI) and facilitated modelling three cities for future scenarios. This modelling allowed us to reach knowledge about how changes in climate and urban land cover impacts the demand for LID. Such information lends itself to urban planning, designing multifunctional urban infrastructure, policymaking regarding urban growth, and the optimal assignment of financial resources for runoff and flood risk management.

6.1.3. Developing a simplified geospatial model for ranking LID solutions

In Chapter 4, the objective was attained utilizing the indices developed in Chapter 2 and investigated in Chapter 3. In this chapter a simplified geospatial model for ranking LID solutions was developed. The model is referred to as LID-Solution Evaluation and Ranking Approach (SERAH). SERAH considers the key criteria contributing to ranking LID solutions including LID benefits (hydrological-hydraulic, environmental, and socioeconomic), costs, demand for LID, and feasibility for implementing LID. It develops a systematic and knowledge-based decision-making model for ranking the LID solutions to address the gap for such a model in the field. The effectiveness and applicability of SERAH were tested and demonstrated for an actual case study within the City of Toronto using a

stormwater model (PCSWMM). Also, a sensitivity analysis (as presented in Section 5.3) was conducted to exhibit the impact of the change in input data (parameters and weights) on the results of SERAH and its related indices (HHI and HSE). As the result, SERAH were able to rank LID solutions and the sensitivity of the results on the parameters were demonstrated to enhance the reliability of the results of SERAH in practice.

Overall, the results of the case study modelling showed that the hydrological-hydraulic index (HHI) is representing the potential of subcatchments in runoff generation and ranks the subcatchments effectively on this basis. In our case study (located in Toronto), which is a highly urbanized area, the contributing drainage area of the subcatchment was found to be an important variable in their ranks. The stormwater modelling showed that implementing an equal area of IT (400 m²) in the individual subcatchments reduces the runoff from 46 to 100 percent. In prioritizing the types of LID, the cost of the LID type was identified as a key factor. However, the lateral benefits of LID outweighed the cost wherein the demand for lateral benefits was high. The geospatial methods for quantifying the lateral benefits of LID types effectively reflected the demand of subcatchments, however, there is an area for research in this field for quantifying all key lateral benefits. Incorporating the lateral benefits of LID into the demand of subcatchments for these benefits allowed for subcatchment-specific ranking of LID types.

SERAH effectively ranked the need for LID at subcatchments and coressponding LID types. The developed method is universally applicable. SERAH lends itself to the strategic planning for multifunctional sustainable infrastructures (LID) involving multiple stakeholders and decision-makers. Also, SERAH helps with attaining a comprehensive insight into the demands for LID across the catchment. It also suggests areas for future

research through multidisciplinary approaches (water resources, geography, socioeconomic, and environment) for runoff-reduction management.

6.2. LIMITATIONS

The limitations and shortcomings of developed method in this research are presented in this section. To apply SERAH for ranking LID solutions these limitations need to be considered.

1. *Hydrological-hydraulic component*

- 1.1. The focus of the research is on the runoff reduction in urban areas using LID and pluvial flood management,
- 1.2. Each ranked LID subcatchment is considered hydrologically homogenous,
- 1.3. Cost of LID needs equivalent hydraulic performance and is limited to capital cost, the life cycle cost can be added in future studies,
- 1.4. The discussions on the effect of urbanization and climate change on the demand for LID is limited to the case studies,

2. *Socioeconomic-Environmental components*

- 2.1. The weights of the indices in the weighted sum methods are considered equal,
- 2.2. Linear standardization has been used,

3. *GIS component*

- 3.1. The subcatchments were discretized as regular grid cells in the Chapter 2 and 3 and then this was improved as regular grid cells and vector polygons in Chapter 4, which should be considered while using SERAH,
- 3.2. Using SERAH requires a resolution that is suitable for detailed design

stormwater projects. The HHI component assumes that the cell is hydrologically homogenous to rank the subcatchments. Thus, the resolution should reflect this assumption. However, like other stormwater projects using excessively fine cells (e.g., 0.1 m) can increase the redundancy of data and computational cost. In contrast, using very coarse cells (e.g., 50 m) needs to be used by considering the assumption. The judgment and the extent of acceptance of the accuracy of the result is the engineer's decision.

6.3. NOVEL CONTRIBUTIONS

This research investigated the solutions for a GIS-based LID framework for sustainable urban runoff management. The innovation and novel contributions of this research include:

- 1- An innovative physics-based GIS-MCDM index (LIDDI) was developed to systematically rank the LID subcatchments. LIDDI integrates the primary (hydrological-hydraulic) and lateral (environmental and socioeconomic) benefits of LID by suggesting three innovative indices (respectively HHI, ENI, and SEI),
- 2- A heuristic geospatial relationship was established between variables contributing to runoff generation, called hydrological-hydraulic index (HHI), and validated against a physical model. The HHI is a novel stand-alone index that provides us with a comprehensive insight into the spatiotemporal hydrological status of the catchment,
- 3- The complexity of city-scale modelling for attaining an insight about future scenarios (a wide range of climate and urbanization) overcame through proposing a physics-GIS-

- based index (HHI). Three Canadian cities were modelled to explore the applicability of the index. Also, for all cities, the impact of these scenarios on the runoff generation (represented by HHI) and demand for LID in the future is extensively portrayed,
- 4- A physics-based GIS-MCDM model (SERAH) was proposed to rank LID solutions (LID subcatchments and types). The innovation of SERAH lies in overcoming the complexity of the integration of multiple key contributing factors (feasibility/demand, LID cost/benefit, and variety of LID types). HSE establishes a mathematical and geospatial relationship between these key contributing factors and suggests effective LID solutions,
 - 5- The application of SERAH was tested for a real-world set of data using a SWM. The novelty of these types of modelling lies in testing the effectiveness of the proposed theory with new sets of data, analyzing, portraying the results, and reporting the limitations and areas for improvement.

6.4. FUTURE RESEARCH DIRECTIONS

Using LID in stormwater collection networks still has a wide range of unexplored areas and aspects. During this research many of these areas were highlighted and are suggested for future research:

6.4.1. Identifying and quantifying the key lateral benefit of LID

In Chapters 2 and 4, several lateral benefits (environmental and socioeconomic) of LID were identified, quantified, and integrated into the primary benefit of LID (hydrological-

hydraulic). The selected lateral benefits demonstrated the application and effectiveness of the proposed SERAH and its indices. However, there is a need to extensively identify and quantify the most common lateral benefits that are considered in different study areas. The approach for quantification of these benefits varies depending on the nature of that benefit. For example, for air treatment, a distance from the center of pollution was considered as a metric. This was different for the population concentration or biodiversity which had concentration within a polygon as the metric. A comprehensive literature review and data gathering from the decision-makers are required to conduct the suggested research. Such research will enhance the use of SERAH by incorporating the most common and important lateral benefits of LID into ranking the LID types and subcatchments in a catchment and identifying the optimal LID solution. There is limited research in this area some examples of such studies are conducted by Yu et al. (2020) and Bai et al. (2019) [229], [230].

6.4.2. Exploring further geospatial relationships for the integration of the lateral benefits into the primary benefit

In Chapter 2, to generate LIDDI, the lateral benefits (SEI and ENI) were integrated into the primary benefit (HHI) using the weighted sum method and considering equal weights for considered criteria (eight criteria). This was the first step to demonstrate the framework and its effectiveness. However, the use of other MCDM models in geospatial concept, contrasting the different method and their impact on the results can lead to developing improved approaches or increasing the confidence toward the results of the existing framework. There are limited investigations in this area some examples of such studies are

by Kuller et al. (2019) and Gallet (2011) [86], [214].

6.4.3. Developing a model which allows for DEM-based outlet detection and routing for LID-scale subcatchments in urban areas

One of the drawbacks in this research was the lack of a model that can automatically delineate and route the pixel-size “urban” subcatchments downstream subcatchments and lastly to the downstream hydraulic unit (inlet or manhole). In conventional models, the discretization of the catchment is through delineating subcatchments using DEM data overlooking “urban” features (such as land cover and land use). Developing an automatic urban catchment delineation method that allows for a more accurate delineation and routing between the subcatchments considering urban features will allow for wide use and further development of frameworks that require finer resolution subcatchments. The research around the subcatchment delineation as a general hydrologic concept has been conducted in previous studies. However, yet there is a need for different approaches, particularly for finer resolution subcatchments. Some examples of recent research are conducted by Islam et al. (2020) and Liu et al. (2020) [231], [232].

6.4.4. Investigation further spatial discretization formats

In Chapter 2 and part of Chapter 4, the regular grid cells and polygon-based discretization formats were used as a representative of a LID subcatchment (one unit of a geographical entity). Future research that uses other spatial discretization methods (e.g.,

Triangular irregular networks (TIN), Voronoi Diagram, Hexagonal, etc.) for representing geographical entities for the LIDDI and HSE frameworks is suggested. Investigating the impact of shapes (e.g., irregular shapes), resolution, and distribution (e.g., nonhomogeneous size) of the discretized units across the study area could introduce on the results the potential advantage of using other discretization methods. The potential advantages can be improving the computational cost or suggesting innovative methods for overlaying the contributing criteria. An example of similar recent research is by Liao et al. (2020) [233].

6.4.5. Developing physics-based indices for lateral benefits of LID

The hydrological-hydraulic index (HHI), the primary demand index, was developed based on the physics principles governing the runoff generation phenomenon. Lateral benefits of LID were quantified using MCDM concepts. As discussed in Chapter 2, physics-based decision-making models can be validated against an actual physics-based model (as done for HHI in this research). However, validating the fact that MCDM models are accurately representing reality is not practical. Thus, through multidisciplinary research developing physics-based indices for lateral benefits of LID like HHI is recommended for further studies. Integration of such indices will allow for developing a fully physics-based comprehensive LIDDI (LID demand index). An example of similar research is Hou et al. (2020) [214] which models water quality and She et al. (2021) [52] which models carbon emission using GIS and integrates it into the runoff reduction.

6.4.6. Further investigation of the LID demand under future scenarios

In this research, the impact of climate (by projecting rainfall) and urbanization (by projecting imperviousness ratio) on hydrologic-hydraulic demand for LID were investigated. The projection of other variables such as hydraulic conductivity or depth to groundwater in the future is also possible and could be studied using HHI. Also, the demand for lateral benefits of LID (environmental and socioeconomic) under future scenarios such as urbanization and climate change are suggested to be investigated.

6.4.7. Investigation the adequacy of available geospatial data and methods for their improvement for use in LID projects

As discussed in Chapter 5, the inadequacy of data from many aspects such as diversity of projection system, format, resolution, et. were one of the challenges of this research. Thus, an investigation on the quality and adequacy of the existing data, a comprehensive comparison and suggestions for improvement can help the future similar studies in the data processing phase.

6.4.8. Correlating HHI with the basement floods in Toronto

We have corelated the results of HHI with the flood vulnerable areas in the city of Toronto. A future study on a method that corelates this index to the basement floods which has causes further than upstream flood generation is suggested. Such a study will assist the decision-

makers of the City of Toronto in planning for future basement flood reduction.

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APPENDICES

APPENDIX A: PYTHON CODE FOR CHAPTER 2

Preparing the data to be used in HHI generation and LIDDI generation code

```
# This script prepares data for LIDDI generation
# Import system modules
*****
import arcpy
arcpy.CheckOutExtension("Spatial") # Check out the ArcGIS Spatial Analyst extension license
*****
from arcpy import env
from arcpy.sa import *
from arcpy.geoprocessing import env
import time
import os

start_time = time.time()

# Create list of variables of HHI
*****
work_space = "C:/Users/Sarah/01/Montreal"
cell_size = 5
study_area = "city.shp"
study_area_t = "city.shp" # This is the study area that euclidean distance is calculated within it
dem = "dem" # The name of the DEM raster file
rainfall = "idf_h" # the rainfall intensity raster (mm/hr)
ks = "ks" # the hydraulic conductivity raster (mm/hr)
groundwater = "gw"
bedrock = "bdrck" # the depth to impermeable layer raster (m)
parking_lot = ""
open_space = "" # all land covers except buildings and pavements
building = ""
pavement = ""
land_cover = "lc"
air = ""
biodiversity = ""
stream = "strm.shp" # feature class data
population = ""
green_space = ""
school = "" # feature class data
hospital = "" # feature class data

# Enter the name of variables that needs Euclidean distance calculations
*****
dist_list = [stream, pavement, green_space, school, hospital]

# A list of data that need to be convert from feature to raster.
*****
# This is a 2D list (first col is data name, second is the "field" that is going to be the "value"
of the raster) that
# need conversion from shp to raster. e.g., conversion[["strm", "watershed"], ["hospital", "FID"]]
conversion_list = []
# This a list of all variables
*****
```

```

toclip_list = [rainfall, ks, groundwater, dem]

#print("Create new folder for the results
*****

#try:
#   my_path = work_space + "/" + my_folder
#   print(my_path)
#   os.mkdir(my_path)
#except OSError:
#   print("my_py already exists")
#else:
#   print("Successfully created the directory my_py")

# Set environment settings
*****
env.workspace = work_space # Input the path of the folder that includes all inout files
env.cellSize = cell_size # cell size of the results
env.overwriteOutput = True # Allow to overwrite new files on the old files
env.mask = study_area # Input the extent of the study area (raster or feature file)
env.snapRaster = land_cover
env.extent = study_area

*****
if len(conversion_list) != 0:
    for i in range(len(conversion_list)):
        map = conversion_list [0, i]
        shp_type = arcpy.Describe(map).shapeType
        inFeatures = map
        outRaster = map[0:-4]
        assignmentType = "MAXIMUM_COMBINED_LENGTH"
        priorityField = ""
        if shp_type == "Polygon":
            valField = col
            map_raster = arcpy.PolygonToRaster_conversion(inFeatures, valField, outRaster, assignmentType,
priorityField, cell_size)
        elif shp_type == "Polyline":
            valField = conversion_list[1, i]
            map_raster = arcpy.PolylineToRaster_conversion(inFeatures, valField, outRaster, assignmentType,
priorityField, cell_size)
        elif shp_type == "Point":
            valField = conversion_list[1, i]
            map_raster = arcpy.PointToRaster_conversion(inFeatures, valField, outRaster, assignmentType,
priorityField, cell_size)
        else:
            *****
# Data is read from work_space and the saved into work_space too
import os.path
# Clip land cover data
*****
out_raster = land_cover + "_c"

print(os.path.exists(out_raster))

if os.path.exists(work_space + "/" + out_raster) is False: # check if land_cover is already
clipped.
    lc_extent = arcpy.Describe(land_cover).Extent
    print(lc_extent)
    print(arcpy.Describe(study_area).ShapeType)
    print(arcpy.Describe(study_area).spatialReference)
    sa_geo = arcpy.Geometry(arcpy.Describe(study_area).ShapeType,
arcpy.Describe(study_area).spatialReference)
    print(sa_geo)
    print(lc_extent.contains(sa_geo))
    if lc_extent.contains(sa_geo) is True:
        arcpy.Clip_management(land_cover, "", out_raster, study_area, "", "ClippingGeometry",

```

```

"MAINTAIN_EXTENT")
    print(out_raster + " clipped")

# Reclassify types of land uses
*****
inRaster = "lc_c"
out_raster1 = "lc_sc01"
out_raster2 = "lc_sc02"
imp = 10 # impervious lands
perv = 20 # pervious lands
water = 30 # water bodies

if os.path.exists(work_space + "/" + out_raster1) is False:
    if os.path.exists(out_raster1) is False: # check if the file is already generated
        temp1 = Reclassify(inRaster, "VALUE", RemapValue([[0, "NoDATA"], [1, imp], [2, perv], [3,
imp], [4, imp], [5, imp], [6, imp], [7, water], [8, imp]]), "NoDATA")
        temp1.save(out_raster1)
        print(out_raster1 + " layer created")
    else:
        print(out_raster1 + " exists")

if os.path.exists(work_space + "/" + out_raster2) is False:
    if os.path.exists(out_raster2) is False: # check if the file is already generated
        temp2 = Reclassify(inRaster, "VALUE", RemapValue([[0, "NoDATA"], [1, imp], [2, imp], [3,
imp], [4, imp], [5, imp], [6, imp], [7, water], [8, imp]]), "NoDATA")
        temp2.save(out_raster2)
        print(out_raster2 + " layer created")
    else:
        print(out_raster2 + " exists")

*****
# Data is read from work_space and the saved into work_space too
# The toclip_list is updated here to replace new file names
print(dist_list)
if len(dist_list) != 0:
    print("Euclidean distance is calculated within: " + study_area_t)
    env.mask = study_area_t
    for i in range(len(dist_list)): # Iterate through dist_list
        in_data = dist_list[i]
        out_data = in_data.replace(".shp", "") + "_d"
        toclip_list.remove(in_data)
        toclip_list.insert(i+5, out_data)
        if os.path.exists(work_space + "/" + out_data) is False: # Check if file already exists
            temp = EucDistance(in_data)
            temp.save(out_data)
            print(out_data)
        else:
            print(out_data + " exists")

*****
# Data is read from work_space and the clipped data is saved into my_path,
# The name of the clipped data is as original data (but saved in the my_path folder)
print(toclip_list)
if len(toclip_list) != 0:
    for k in range(len(toclip_list)):
        in_data = toclip_list[k]
        print(in_data)
        out_data = in_data + "_c"
        x_extent = arcpy.Describe(in_data).Extent
        print(x_extent)
        sa_geo = arcpy.Geometry(arcpy.Describe(study_area).ShapeType,
arcpy.Describe(study_area).spatialReference)
        print(x_extent.contains(sa_geo))
        if x_extent.contains(sa_geo) is True: # check if the data layer needs clip (the extent of
the data contains the study area extent)

```



```

        if os.path.exists(work_space + out_data) is False: # check if the data is already
clipped due to previous runs
            arcpy.Clip_management(in_data, "", out_data, study_area, "", "ClippingGeometry",
"MAINTAIN_EXTENT")
            print(out_data + " created!")
        else:
            print(out_data + " exist!")

*****
# The resolution of all data in my_path is checked and if need justification they will be justified
print(toclip_list)
for i in range(len(toclip_list)):
    in_data = toclip_list[i]
    data_resolution = arcpy.Describe(in_data).children[0].meanCellHeight
    print(in_data + " resolution is: " + str(data_resolution))
    out_data = in_data + "_r"
    if data_resolution > cell_size:
        print(os.path.exists(my_path + "/" + out_data))
        if os.path.exists(my_path + "/" + out_data) is False: # Check if resolution already changed
            arcpy.Resample_management(in_data, out_data, cell_size, "NEAREST")
            print(out_data + " created: resolution changed from " + str(data_resolution) + " to " +
str(cell_size))
            toclip_list.remove(in_data)
            toclip_list.insert(i, out_data)
        else:
            print(out_data + " with resolution of " + str(cell_size) + " exists")
            toclip_list.remove(in_data)
            toclip_list.insert(i, out_data)
    else:
        print(out_data + " with resolution of " + str(cell_size) + " cell size is fine")

print(toclip_list)

*****
print(os.path.exists(work_space + "/" + "slope"))
if os.path.exists(work_space + "/" + "slope") is False:
    slope = Slope(dem, "DEGREE", 1)
    slope.save("slope")
    print("slope layer created")
else:
    print("slope exists")

end_time = time.time() - start_time
print(time.time())
print("run time =" + str(end_time) + " seconds")

```

This code is to remap a list of raster data located in a workplace and write the results in the same folder

```

*****
from arcpy import env
from arcpy.sa import *
env.overwriteOutput = True # Allow to overwrite new files on the old files
#work_spaces = ["E:/Sarah/01/Toronto/", "E:/Sarah/01/Montreal/", "E:/Sarah/01/Vancouver/"]
work_spaces = ["E:/Sarah/01/Vancouver/"]

in_rasters = ["hhi_00_sc0", "hhi_00_sc1", "hhi_00_sc2", "hhi_36_sc0", "hhi_36_sc1", "hhi_36_sc2",
"hhi_66_sc0",
                "hhi_66_sc1", "hhi_66_sc2", "hhi_96_sc0", "hhi_96_sc1", "hhi_96_sc2"]

#in_rasters= ["idf_00", "idf_36", "idf_66", "idf_96"]
#myRemapRange = RemapRange([[0, 10, 5], [10, 20, 15], [20, 30, 25],[30, 40, 35], [40, 50, 45], [50,
60, 55],
#
#                [60, 70, 65], [70, 80, 75], [80, 90, 85], [90, 100, 95]])
#myRemapRange = RemapRange([[0, 25, 1], [25, 50, 2], [50, 75, 3], [75, 100, 4]])
myRemapRange = RemapRange([[0, 15, 10], [15, 25, 20], [25, 35, 30],[35, 45, 40], [45, 55, 50],
[55, 65, 60]])
for work_space in work_spaces:
    for in_raster in in_rasters:
        env.workspace = work_space
        temp = Reclassify(in_raster, "VALUE", myRemapRange)
        temp.save(str(in_raster) + "_rn")
        print(str(in_raster) + "_rn is created")

    This script calculates HHI
    # IMPORTANT!!!!!! Items to check: 1- Work_space 2- Name of each single variable 3- Unit_factor of
    Variables
    # Import system modules
    *****
import arcpy
from arcpy import env
from arcpy.sa import *
import time
import os

#os.system("C:/Users/Sarah/01/HGML/HGML_DataPreparation.py")
#open(r"C:/Users/Sarah/01/HGML/HGML_DataPreparation.py").read()
#from HGML.HGML_DataPreparation import *
start_time = time.time()

# Set the variables
*****
# Select the variables from the my_path of HGML_DataPreparation
*****
# If there is a file with "_r" suffix, it is preferred to the original name of the file
*****
work_space = "C:/Users/Sarah/01/Toronto/my_py_Toronto"
env.workspace = work_space
env.overwriteOutput = True # Allow to overwrite new files on the old files
rainfall = "int" # the rainfall intensity raster (mm/hr)::: if unit is not correct set the unit
factor in the code
ks = "ks" # the hydraulic conductivity raster (mm/hr)::: if unit is not correct set the unit
factor in the code
groundwater = "gw" # in mm ::: if unit is not correct set the unit factor in the code
bedrock = "" # the depth to impermeable layer raster (mm) ::: if unit is not correct set the unit
factor in the code
dem = "gta_dem5m"
# if change if unit is needed enter the unit change factor below in each section
hhi_list = [rainfall, ks, bedrock, groundwater, dem]
# Rainfall

```

```

*****
print("rainfall is: " + rainfall)
unit_factor = 1
r_mm_hr = Times(rainfall, unit_factor) # change the unit to mm/hr is required
r_mm_hr.save("r_mm_hr")
# return ks (cm/hr)
*****
if ks != "": # Check if ks data exist
    print("ks is: " + ks)
    unit_factor = 10
    ks_mm_hr = Times(ks, unit_factor) # return ks (mm/hr)
    ks_mm_hr.save("ks_mm_hr")
# groundwater
*****
if groundwater != "": # Check if gw data exist
    print("groundwater is: " + groundwater)
    unit_factor = 1000
    gw_t = Times(groundwater, unit_factor)
    gw_mm = Con(gw_t, 0, gw_t, "VALUE < 0")
    gw_mm.save("gw_mm")
# Bedrock
*****
if bedrock != "": # Check if bedrock data exist
    print("Bedrock is: " + bedrock)
    unit_factor = 1000
    br_mm = Times(bedrock, unit_factor)
    br_mm.save("br_mm")
    if groundwater != '': # Check if groundwater exist
        *****
        impermeable = [gw_mm, Times(br_mm, 0.5)] # list of gw and bedrock (porosity considered)
        min_br_gw = FuzzyOverlay(impermeable, "AND") # Set min_br_gw as minimum of gw and bedrock
        (porosity considered)
        min_br_gw.save("min_br_gw")
    else:
        min_br_gw = Times(br_mm, 0.5)
        min_br_gw.save("min_br_gw") # Set min_br_gw as only bedrock (porosity considered)
else:
    if groundwater != '' and bedrock != '':
        min_br_gw = gw_mm
        min_br_gw.save("min_br_gw") # Set min_br_gw as only groundwater
    else: # none of bedrock and groundwater exists
        min_br_gw = ""

# check if the depth is over 3 m
*****
if min_br_gw != "":
    imprmbl_con = Con(min_br_gw, "3", min_br_gw, "VALUE > 3") # check if the depth is over 3 m
    imprmbl_con.save("imprmb1_con")
    print("imprmb1_con created!")
else:
    imprmbl_con = ""
# Calculate the min of Ks and br and gw
*****
if ks != "":
    if imprmbl_con != "":
        # imprmbl_exists
        depth_min = FuzzyOverlay([imprmb1_con, ks_mm_hr], "AND") # minimum ks and impermeable
        depth_min.save("depth_min")
        print("Both Ks and impemle exist and depth_min created!")
    else:
        depth_min = ks_mm_hr
        depth_min.save("depth_min")
        print("Ks exists, impemle does not exist and depth_min created!")
else:
    # ks does not exist
    if imprmbl_con != "":
        depth_min = imprmb1_con
        depth_min.save("depth_min")

```

```

        print("Ks does not exist, impemle exists and depth_min created!")
    else:
        depth_min = ""
        print("Both Ks and impemle does not exist and depth_min not created!")
# Calculate runoff
*****
print(os.path.exists(work_space + "/" + "depth_min"))
if os.path.exists(work_space + "/" + "depth_min") is True:
    runoff_temp = Minus(r_mm_hr, depth_min)
else:
    runoff_temp = r_mm_hr
runoff_temp.save("runoff_temp")
runoff = Con("runoff_temp", "runoff_temp", 0, "VALUE > 0")
runoff_temp.save("runoff")
print("runoff created!")
# Calculate Slope factor
*****
slope_con = Con("slope", 45, "slope", "VALUE > 45")
slope_nonlinear = 1 + Power(Tan(Times(slope_con, 3.14 / 180)), 0.385)
print("slope nonlinear created!")
# Calculate HHI
*****
HHI = Times(slope_nonlinear, runoff)
HHI.save("HHI")
print("HHI created")
#
*****
end_time = time.time() - start_time
print("run time =" + str(end_time) + " seconds")
This script generates LIDDI
# IMPORTANT!!!!!! Items to check: 1- Work_space 2- seeni list 3- invers distance list 4- weight
list 4- HHI variable name
# Import system modules
*****
import arcpy
from arcpy import env
from arcpy.sa import *
import time
import os
work_space = "E:/Sarah/01/Toronto/"
env.workspace = work_space
env.overwriteOutput = True # Allow to overwrite new files on the old files
start_time = time.time()
#os.system("C:/Users/Sarah/01/HGML/HGML_DataPreparation.py")
#open(r"C:/Users/Sarah/01/HGML/HGML_HHI.py").read()
#from HGML.HGML_HHI import *

# Create list of variables
*****
# Enter the list of criteria, clipped and resampled in HGML_DataPreparation
# Criteria with _d are distance to the source files
seeni_list = ["air", "biodiv", "strms_d", "pavement_d", "pop_dens", "green_d", "school_d",
"hospital_d"]
# This list determines if items in seeni list needs invers distance or not
# Enter 0 if not required, 1 if required, the order should follow the seeni_list
inverse_dist = ["0", "0", "0", "1", "0", "0", "1", "1"]
# Enter the weight of input criteria, the order should follow the seeni_list
weight = ["0.125", "0.125", "0.125", "0.125", "0.125", "0.125", "0.125", "0.125"]
*****
if len(seeni_list) != 0:
    criwei_list = []
    print(seeni_list)
    for i in range(len(seeni_list)): # Iterate through seeni and weight list to rescale all data
        in_raster = seeni_list[i]
        print(in_raster)

```

```

std_name = in_raster + "_s"
if os.path.exists(work_space + "/" + std_name) is False:
    from_scale = "0"
    to_scale = "1"
    minimum = "0"
    lowerThreshold = "0"
    valueBelowThreshold = ""
    maximum = str( arcpy.GetRasterProperties_management(in_raster, "MAXIMUM"))
    print("maximum of " + in_raster + " is: " + maximum) # Extract the maximum of the
raster data
    upperThreshold = ""
    valueAboveThreshold = ""
    x = inverse_dist[i]
    if x == "1":
        from_scale = "1"
        to_scale = "0"
    my_TfLinear = TfLinear(minimum, maximum, lowerThreshold, valueBelowThreshold,
upperThreshold, valueAboveThreshold)
    rescaled = RescaleByFunction(in_raster, my_TfLinear, from_scale, to_scale) # Rescale
the raster between from_scale and to_scale
    rescaled.save(std_name)
    w = weight[i]
    criwei_list.append([std_name, "VALUE", w])

*****

SEENI = WeightedSum(WSTable(criwei_list))
print(SEENI)
SEENI.save("SEENI")
print("SEENI created")
*****

LIDDI = Times("HHI", Plus("SEENI", 1))
LIDDI.save("LIDDI")
print("LIDDI created")

*****

stat_list = ["LIDDI", "HHI", "SEENI"]
for item in stat_list:
    in_zone_data = "C:/Users/Sarah/01/Toronto/Toronto.shp"
    zone_field = "FID"
    in_value_raster = item
    out_table = item + "_tbl"
    out_graph = item + "_gra"
    ZonalHistogram(in_zone_data, zone_field, in_value_raster, out_table, out_graph)
    mean = str(arcpy.GetRasterProperties_management(item, "MEAN"))
    maximum = str(arcpy.GetRasterProperties_management(item, "MAXIMUM"))
    minimum = str(arcpy.GetRasterProperties_management(item, "MINIMUM"))
    print(item + " mean is: " + mean + " and maximum is: " + maximum + " and minimum is: " +
minimum)

# eliminating existing lid
# exist_lid = input("Existing LID layer name : ")

end_time = time.time() - start_time
print("run time = " + str(end_time) + " seconds")
*****

```

This code is to calculate and graph the statistics of the results

```
# This code is to derive the statistics for a list of raster data located in a workplace
# including mean, minimum, and maximum values; derive the histogram based on customized bins;
# plot the histogram; and write the results in a text file
*****
import arcpy
from arcpy import env
from arcpy.sa import *
arcpy.CheckOutExtension("Spatial")
import numpy as np
import matplotlib.pyplot as plt

# This example uses an 8bit unsigned format TIFF image
work_spaces = ["E:/Sarah/01/Vancouver/"]
data_list = ["hhi_00_sc0_rn", "hhi_00_sc1_rn", "hhi_00_sc2_rn", "hhi_36_sc0_rn", "hhi_36_sc1_rn",
            "hhi_36_sc2_rn",
            "hhi_66_sc0_rn", "hhi_66_sc1_rn", "hhi_66_sc2_rn", "hhi_96_sc0_rn", "hhi_96_sc1_rn",
            "hhi_96_sc2_rn"]

bin_hhi = [0,10,20,30,40,50,60,70,80,90,100]

*****

for work_space in work_spaces:
    hist_list = []
    file1 = open("E:/Sarah/01/hist.txt", "a")
    file1.write(str(work_space) + "\r\n")
    for data in data_list:
        # Convert raster to numpy array and calculate histogram
        tiff = work_space + data
        print(tiff)
        array = arcpy.RasterToNumPyArray(tiff)
        # numpy.histogram(a, bins=10, range=None, normed=None, weights=None, density=None)[source]
        # https://numpy.org/doc/1.18/reference/generated/numpy.histogram.html#numpy.histogram
        hist, bins = np.histogram(array, bins=bin_hhi)
        hist_list.append(hist)
        maximum = max(hist)
        print(maximum)
        """in_raster = arcpy.sa.RoundUp(tiff)
        mean = str(arcpy.GetRasterProperties_management(in_raster, "MEAN"))
        maximum = str(arcpy.GetRasterProperties_management(in_raster, "MAXIMUM"))
        minimum = str(arcpy.GetRasterProperties_management(in_raster, "MINIMUM"))
        print(data + " mean is: " + mean + " and maximum is: " + maximum + " and minimum is: " +
        minimum)"""

        # Plot the histogram
        # plot(x, y, color='green', marker='o', linestyle='dashed', linewidth=2, markersize=12)
        """plt.plot(bins[:-1], hist, "-b")
        plt.xlim(min(bins), max(bins))
        plt.ylabel('Pixel Count')
        plt.xlabel('Pixel Values')
        #plt.save()"""
*****
    # Program to show various ways to read and
    # write data in a file.
    file1 = open("E:/Sarah/01/hist.txt", "a")
    file1.write(str(data) + " " + str(hist) + "\n")
    #file1.write(" minimum : " + str(minimum) + "\n")
    #file1.write(" mean : " + str(mean) + "\n")
    #file1.write(" maximum : " + str(maximum) + "\n")
    file1.close() # to change file access modes
```

APPENDIX B: PYTHON CODE FOR CHAPTER 3

This script calculates HHI for a list of land cover and a list of rainfall scenarios and generates the combined HHI

```
# This script calculates HHI for a list of land cover and a list of rainfall scenarios and generates
the combined HHI
# scenarios and write the generated HHI as a raster
file*****

# Import system modules
*****

import arcpy
from arcpy import env
from arcpy.sa import *
import time
import os
#os.system("C:/Users/Sarah/01/HGML/HGML_DataPreparation.py")
#open(r"C:/Users/Sarah/01/HGML/HGML_DataPreparation.py").read()
#from HGML.HGML_DataPreparation import *
start_time = time.time()
work_space = "E:/Sarah/01/Vancouver"
study_area = "city.shp"
env.workspace = work_space
env.overwriteOutput = True # Allow to overwrite new files on the old files
env.cellSize = 5 # cell size of the results
env.extent = study_area

# Set the variables
*****

# Select the variables from the my_path of HGML_DataPreparation
*****
# If there is a file with "_r" suffix, it is preferred to the original name of the file
*****

toronto_data = ["ks_c", "gw_c", "bdrck_c", "dem_c"]
toronto_unit = [{"rainfall", 1}, {"ks", 10}, {"gw", 1000}, {"bdrck", 1000}] # change the unit to
mm/hr is required

montreal_data = ["ks_c", "gw_c", "bdrck_virt", "dem_con"]
montreal_unit = [{"rainfall", 1}, {"ks", 1}, {"gw", 1000}, {"bdrck", 1000}] # change the unit to
mm/hr is required

vancouver_data = ["ks_c", "gw", "bdrck", "dem_con"]
vancouver_unit = [{"rainfall", 1}, {"ks", 0.01}, {"gw", 1000}, {"bdrck", 1000}] # change the unit
to mm/hr is required

#idf_list = ["idf_00", "idf_36", "idf_66", "idf_96"]
idf_list = ["idf_66", "idf_96"]
develop_list = ["ks_zero0", "ks_zero1", "ks_zero2"] # ks_zero is extracted paved areas from the lc
scenarios

city_data = vancouver_data
city_unit = vancouver_unit

print("Slope calculation
*****")
dem = city_data[3]
print(os.path.exists(work_space + "/" + "slope"))
if os.path.exists(work_space + "/" + "slope") is False:
    slope = Slope(dem, "DEGREE", 1)
```

```

    slope.save("slope")
    print("slope layer created")
else:
    print("slope exists")
# Calculate Slope factor
*****
slope_con = Con("slope", 45, "slope", "VALUE > 45")
slope_nonlinear = 1 + Power(Tan(Times(slope_con, 3.14 / 180)), 0.385)
print("slope nonlinear created!")

#
*****
ks = city_data[0] # the hydraulic conductivity raster (mm/hr)::: if unit is not correct set the
unit factor in the code
groundwater = city_data[1] # in mm ::: if unit is not correct set the unit factor in the code
bedrock = city_data[2] # the depth to impermeable layer raster (mm) ::: if unit is not correct set
the unit factor in the code
dem = city_data[3]

# ks (cm/hr)
*****
if ks != "": # Check if ks data exist
    print("ks is: " + ks + str(arcpy.GetRasterProperties_management(ks, "BANDCOUNT")))
    unit_factor = city_unit[1][1]
    ks_mm_hr = Times(ks, unit_factor) # return ks (mm/hr)
    ks_mm_hr.save("ks_mm_hr")
# groundwater
*****
if groundwater != "": # Check if gw data exist
    print("groundwater is: " + groundwater + str(arcpy.GetRasterProperties_management(groundwater,
"BANDCOUNT")))
    unit_factor = city_unit[2][1]
    gw_t = Times(groundwater, unit_factor)
    gw_mm = Con(gw_t, 0, gw_t, "VALUE < 0")
    gw_mm.save("gw_mm")
# Bedrock
*****
*
if bedrock != "": # Check if bedrock data exist
    print("Bedrock is: " + bedrock + str(arcpy.GetRasterProperties_management(bedrock,
"BANDCOUNT")))
    unit_factor = city_unit[3][1]
    br_mm = Times(bedrock, unit_factor/2)
    br_mm.save("br_mm")

for impervious in develop_list:
    print("calculation for impervious: " + impervious +
str(arcpy.GetRasterProperties_management(impervious, "BANDCOUNT")))
    for idf in idf_list:
        print("calculation for climate: " + idf)
        #
Rainfall*****
*****
        rainfall = idf
        print("rainfall is: " + rainfall + str(arcpy.GetRasterProperties_management(rainfall,
"BANDCOUNT")))
        unit_factor = city_unit[0][1]
        r_mm_hr = Times(rainfall, unit_factor) # change the unit to mm/hr
        r_mm_hr.save("r_mm_hr")
        # Minimum depth to restrictive layer
*****
        impermeable = ["ks_mm_hr", "gw_mm", "br_mm", impervious]
        temp = FuzzyOverlay(impermeable, "AND")
        temp.save("depth_min")
        # check if the depth is over 3 m

```



```

*****
temp = Con("depth_min", "3", "depth_min", "VALUE > 3") # check if the depth is over 3 m
temp.save("depth_con")
print("depth_con created!")
# Calculate runoff
*****
runoff_temp = Minus("r_mm_hr", "depth_con")
runoff_temp.save("runoff_temp")
temp = Con("runoff_temp", "runoff_temp", 0, "VALUE > 0")
temp.save("runoff")
print("runoff created!")
# Calculate HHI
*****
HHI = Times(slope_nonlinear, "runoff")
HHI.save("HHI_" + idf[-2:] + "_Sc" + impervious[-1:])
print("HHI created")
print(idf)
print(impervious)
#
*****
*****
end_time = time.time() - start_time
print("run time =" + str(end_time) + " seconds")

```

APPENDIX C: PYTHON CODE FOR CHAPTER 4

This script IDENTIFY FEASIBLE SITES

```
# Import system modules
*****
import arcpy
from arcpy import env
from arcpy.sa import *
import time
import os
os.system("C:/Users/Sarah/01/HGML/HGML_DataPreparation.py")
exec(open(r"C:/Users/Sarah/01/HGML/HGML_DataPreparation.py").read())
from HGML.HGML_DataPreparation import *
start_time = time.time()

print("Calculate required criteria *****")

print("Create a buffer around buildings to exclude from the feasible cells*****")
building_buff = 4
cell_num = building_buff / cell_size
building_buff = Expand("building", cell_num, [1]) # create the buffer
building_buff.save("building_buff")
print("building_buff layer created")
arcpy.RasterToPolygon_conversion(building_buff, "building_buff", "NO_SIMPLIFY", "VALUE") # convert
to polygon
print("building_buff.shp layer created")
con0_complementary = arcpy.Erase_analysis(study_area, "building_buff.shp") # create the
complementary polygon
print("con0_complementary layer created")
con0_temp = arcpy.PolygonToRaster_conversion(con0_complementary, "id", "con0_building") # convert
to raster
print("con0_building layer created")

print("Extract cells which has pass the limitation of sub-basin area*****")
flow_dir = FlowDirection(dem + "_c", "", "", "")
flow_dir.save("flow_dir")
print("flow_dir layer created")
flow_acc = FlowAccumulation(flow_dir, "", "FLOAT")
flow_acc.save("flow_acc")
print("flow_acc layer created")
con1_flow_acc = Con(flow_acc, flow_acc, "", "VALUE >=" + str(sheet1.cell_value(19, 1)))
con1_flow_acc.save("con1_flow_acc")
print("con1_flow_acc layer created")

print("Extract the cells which have suitable slope *****")
gr_slope = "VALUE <" + str(sheet1.cell_value(20, 1))
pv_slope = "VALUE <" + str(sheet1.cell_value(21, 1))
con2_slope = Con(slope, slope, "", gr_slope) # Extract the cells which have suitable slope
(slope<10%) for green roof
con2_slope.save("con2_slope")
print("con2_slope layer created")
con3_slope = Con(slope, slope, "", pv_slope) # Extract the cells which have suitable slope
(slope<10%) for green roof
con3_slope.save("con3_slope")
print("con3_slope layer created")

print("# Find cells with groundwater (gw) depth of 3m (1m distance+2 m LID thickness) and less
****")
gw_shallow = Minus(sheet1.cell_value(4, 1) + "_c", sheet1.cell_value(18, 1) + 2)
```

```

gw_shallow.save("gw_shallow")
print("gw_shallow layer created")
con4_gw = Con(gw_shallow, gw_shallow, "", "VALUE > 0")
con4_gw.save("con4_gw")
print("con4_gw layer created")

print("Identify feasible cells *****")
# for green roof
con_list1 = ["building", "con2_slope"]
# for porous pavement
con_list2 = ["pavement", "con0_building", "con1_flow_acc", "con3_slope", "con4_gw"]
# for open space lids
con_list3 = ["open_space", "con0_building", "con1_flow_acc", "con4_gw"]
fuzzy_list = [con_list1, con_list2, con_list3]

for con_list in fuzzy_list:
    feasible = FuzzyOverlay(con_list, "AND") # intersect the condition to find feasible cells
    print(fuzzy_list.index(con_list))
    if fuzzy_list.index(con_list) == 0:
        x = "feasible_gr"
        print("feasible_gr layer created")
    elif fuzzy_list.index(con_list) == 1:
        x = "feasible_pv"
        print("feasible_pv layer created")
    else:
        x = "feasible_os"
        print("feasible_os layer created")
    feasible.save(x)

end_time = time.time() - start_time
print("run time =" + str(end_time) + " seconds")

```

APPENDIX D: THE PROOF OF CONCEPT OF CHAPTER 4

We have proved the concept of SERA using the model used in Section 5.3 and generating 100 random scenarios. To do so, the input data were included in three categories: i) data for generating the hydraulic-hydrological index (HHI), ii) data used for generating socioeconomic-environmental demand-benefit index (SE), and iii) data related to the cost and benefits of the four LID types. These data were differently and randomly generated for the 100 scenarios, the normalized range of these data for all scenarios is presented in Figure D 1, which shows a good variety of data for all inputs all ranged from 0 to 1. This variety increases the reliability of the model in terms of its applicability in all possible scenarios in contrast to only some specific scenarios.

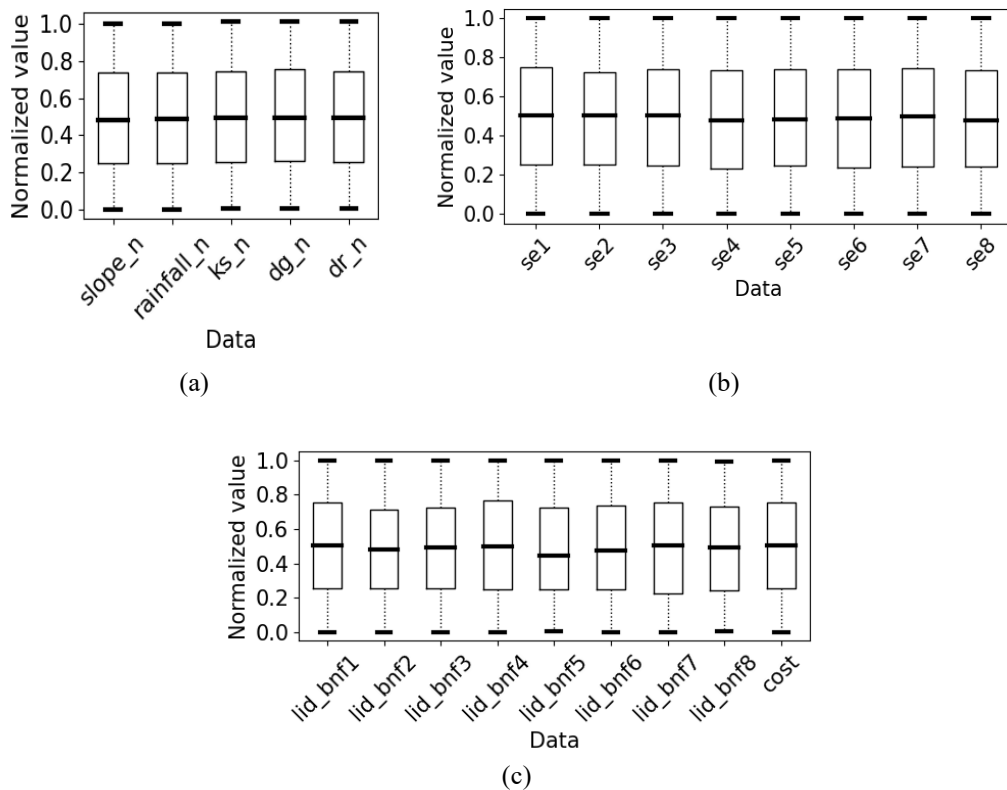


Figure D 1 Box plot of the input data for 100 scenarios including (a) data for generating hydrological-hydraulic index (HHI), (b) data for generating socioeconomic-environmental index (denoted as se1 to se8), and (c) data related to the LID benefit and LID cost (denoted as lid_bnf1 to lid_bnf8 and cost)

We also assessed the spatial distribution of the random input data in the sites of the catchment (C01 to C25). This was to increase the reliability and robustness of the model by using a good random spatial distribution of the data. The radar plot of input data for a sample of 10 scenarios are presented in Figure D 2. In these plots each radius represents one site so the plot has 25 radii, the normalized value of the input data is shown along the radius (the center of the plot shows zero and the circumference is 1).

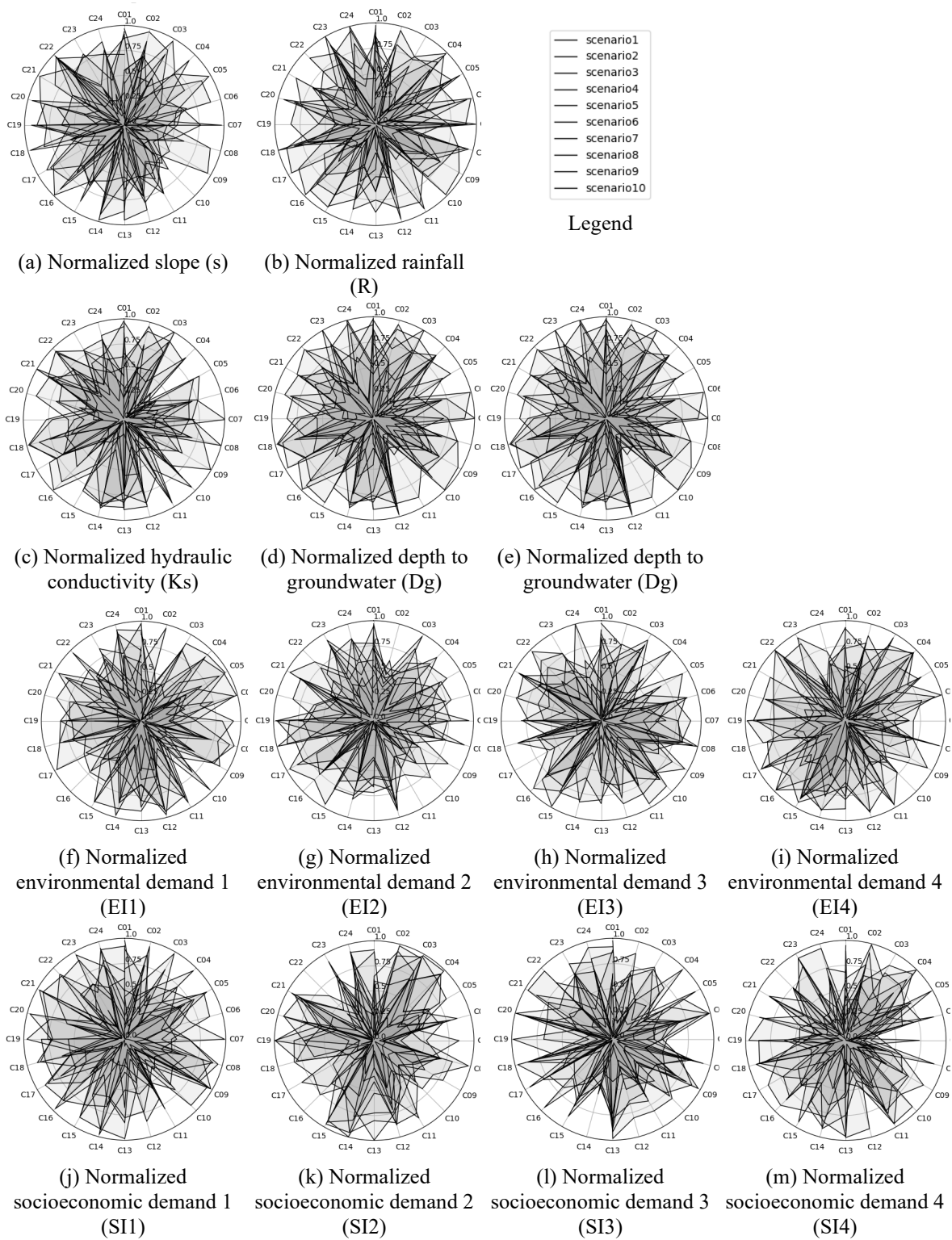
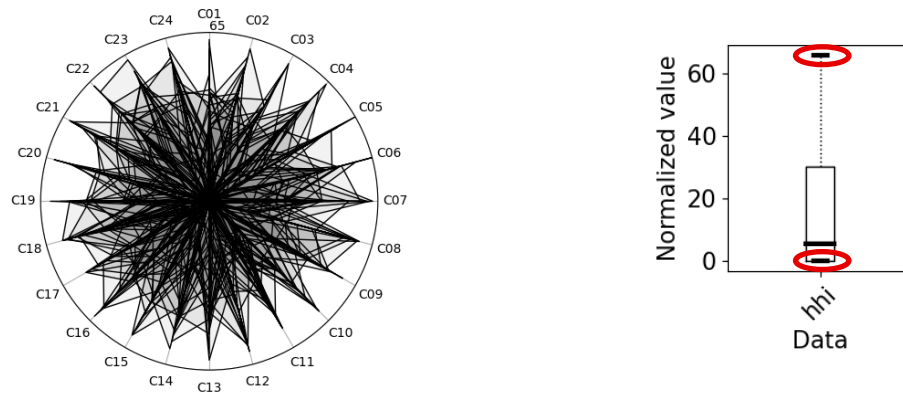


Figure D 2 The spatial distribution of input data for 10 sample scenarios

The input data were used for step b-1 of component (b). In this step, these data geospatially were overlaid using Eq. 4.1. As a result, the catchment was indexed based on its hydrological-hydraulic demand for LID for all 100 scenarios. Figure D 4 presents the actual and normalized values of HHI for all 100 scenarios using a radar plot and box plot, respectively.



(a) The radar plot for generated hydrological-hydraulic index (HHI) of 100 different scenarios, each radii axis representing one site

(b) The box plot for generated hydrological-hydraulic index (HHI) of 100 different scenarios, representing the range of this index before normalization

Figure D 3 The result of the component (b) step b-3 showing the value and range of the Hydrological-hydraulic demand for LID Types at different sites for all 100 scenarios

The HHCI was generated for each LID type. It was conducted by geospatial overlaying of HHI with the cost of each type of LID through a geospatial division operation. This overlaying process resulted in four geospatial data layers (corresponding to each LID type) per scenario (400 data layers overall). In the next step, the data layers of hydrological-hydraulic demand for LID Types in feasible sites were generated. To do this, first, the sub-catchments were delineated by considering feasible sites as pour point (outfall), as is demonstrated in Figure D 4. Then the value of HHCI at each feasible site was estimated through a geospatial zonal (subcatchments were the zones) statistic operation, for which the statistical operation was considered to be the sum of HHCI within the catchment of the feasible site. The value of HHCI for the infeasible sites was assigned to be No-Data.

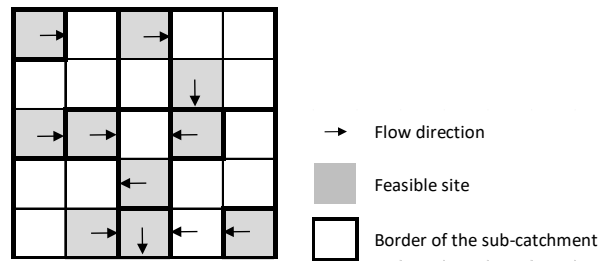


Figure D 4 Delineated sub-catchments based on the flow direction and the geographical location of the feasible sites

For component (c) were overlaid to their corresponding benefits using Eq. 4.3 to Eq. 4.6. The weights used in the weighted sum method were considered equal in this study. However other weighting methods (such as pairwise comparison, ranking, Delphi, etc.) are suggested for future investigations. The result indexed the catchment representing its demand for each type of LID, which led to four data layers corresponding to the four LID types. These indices were generated for all 100 scenarios (400 data layers overall). To demonstrate the application of the method a sample of distribution of the value of input data (environmental demand indices (EI) and benefit (EB), socioeconomic demand indices (SI) and benefit (SB), and output data (socioeconomic and environmental demand of each type of LID (SE)) are presented in Figure D 5. This figure shows the variation of SE for all four types of LID (plots (a) to (d)). Based on these plots it is evident the overall demand for LID3 and 4 is higher than LID 1 and 2. Also, each plot presents that wherein all eight demands and corresponding benefits are high at a specific site e.g., FigureD6 (a) C19, C21), and wherein both are low SE is low (e.g., Figure D 5(a) C11, C22).

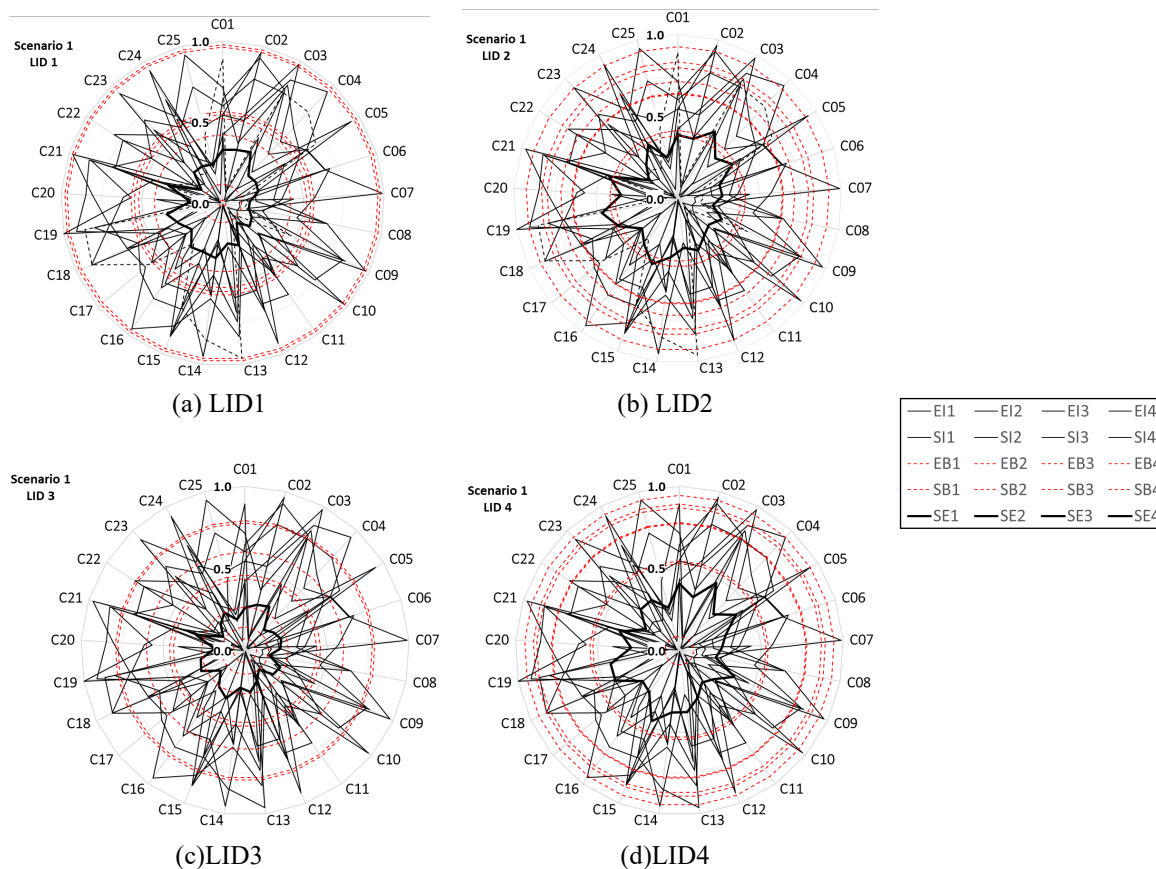


Figure D 5 The socioeconomic and environmental demand of each type of LID (SE): (a) LID 1 (b) LID2 (c) LID3 (d) LID4 derived from the environmental demand indices (EI) and benefit (EB), socioeconomic demand indices (SI) and benefit (SB)

In the next step, the data layers of Socioeconomic and Environmental demand for LID types in feasible sites were assumed. To do this, first, the value of SE at each feasible site was estimated through a geospatial focal weighted mean operation, for which the kernel array (weight array) was assumed to have a window size of 5 x 5 with values showed in Figure D 7 (a). In Figure D 7 (b), one corner site (C01) is highlighted as an example. The cells that are involved in the calculation of SE of this site are shown in grey shade. The weights of the kernel array also have been presented in the Figure D 7 (b). Like HHI, the value of SE for the infeasible sites was assigned to No-Data.

It is important to be noted that the size of the kernel array and the assigned weights to the neighborhood cells are an assumption in this study to demonstrate how the suggested

model works. The size of the kernel array physically represents the radial influence of the implemented LID on the neighboring cells (e.g., how far C01 can influence surrounding sites in terms of decreasing air pollution or increasing access to amenities). The maximum distance needs to be investigated in future studies for individual socioeconomic and environmental impacts of LID.

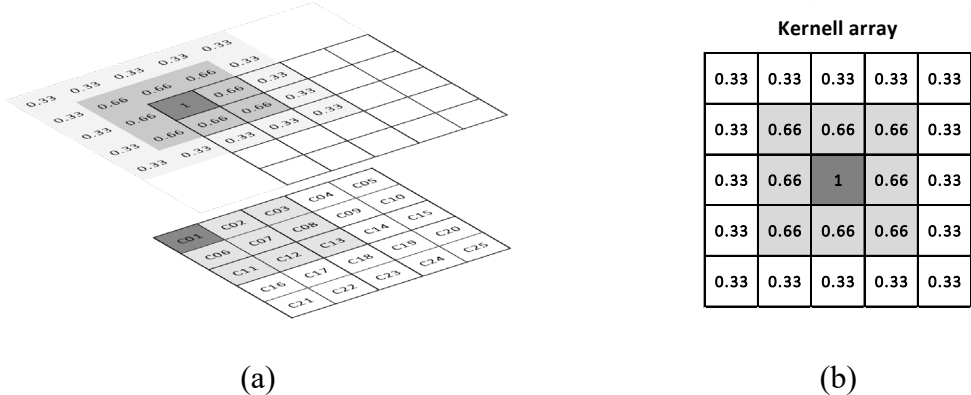


Figure D 6 Estimating the socioeconomic and environmental demand for LID types in feasible sites, using (b) focal weighted mean (C01 as an example) and (a) kernel array weights

The results of component (b) and (c) were overlaid using the method demonstrated in component (d) of this study. We considered that the level of importance for both components are equal in the weighted sum overlaying method. However, it is noteworthy that this assumption was made for the demonstration of the framework and actual weights need to be determined for each specific catchment according to the catchment needs, preferences, and priorities. This process (component (d)) was performed for all 100 scenarios.

The result agreed with initial assumptions and allowed us to rank the sites within the catchment for implementing LID as well as providing us the rank of LID types at each site. The numerical result of three sample catchments (01, 50, 99) are randomly selected and presented using bar and line graphs (see Figure D8). In these graphs, the x-axis shows the feasible sites (10 out of 25 sites), and the y axis presents the value of modified HHI based on cost (HHCI), socioeconomic-environmental demand (SE), cost of each LID type, and the result index, HSE. Overall, these graphs show that wherein both demands (HHCI, SE) are high, and the cost is low the HSE is higher (e.g., Scenario 01 at C09; Scenario 25 at C22,

Scenario 50 at C23, Scenario 75 at C11, and Scenario 99 at C09). In contrast where both demands are low the HSE value and rank of sites are low (e.g., Scenario 01 at C25; Scenario 25 at C03, Scenario 50 at C18, Scenario 75 at C25, and Scenario 99 at C01). Whereas other sites are ranked in between. Therefore, based on the HSE value sites of the catchments (scenarios) were ranked. On this basis, sites with high HSE values are assigned the highest rank for implementing LID and this trend continued for the lower ranks. These results confirmed that in ranking the sites of a given catchment not only the feasibility of the site (here 10 feasible sites out of 25 sites) were considered but also the demand of sites for LID were integrated into site selection process with high demand for LID. These demands for LID included the hydrological-hydraulic demand of the feasible site and its catchment along with the socioeconomic-environmental demand of the feasible site and its neighborhood.

In addition to the rank of sites within the catchment, the second valuable and important information that can be derived from Figure D 7, HSE values, is the rank of different types of LID at each site. In this figure, each line plot represents the HSE value for each type of LID. Comparing these plots at each feasible site reveals the rank of the LID types at the site. For example, for scenario 50, if we decide to implement a unit of LID at the first rank site (C23) the highest suggested LID for the site is LID type 2 (dashed black line with black square shape marker) and the least suggested is LID type 4 (dashed red line with red square shape marker), and other two types are in between. The high rank of LID type 1 is due to its low price leading to a high HHCI2 (bar plot, dark grey shade) as well as high SE2, which is an indicator of the demand at this site for the benefits that this certain type of LID offers.

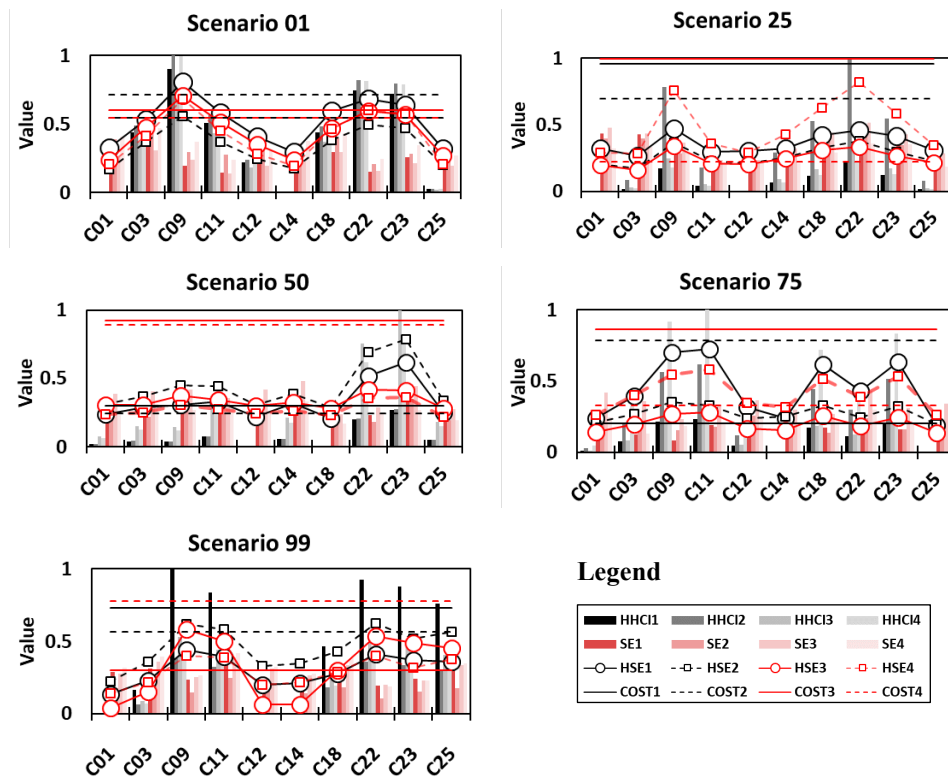


Figure D 7 The values of modified HHI based on cost (HHCI), socioeconomic-environmental demand (SE), cost of each LID type, and the result index, HSE for identifying optimized layout (site and type) for implementing LID for five sample scenarios (scenario 01, 25, 50, 75 and 99)

APPENDIX E: CODE AND INPUT DATA USED FOR THE SENSITIVITY ANALYSIS

Sensitivity analysis of HHI, LIDDI, and HSE to input parameters

```
# "This program creates a conceptual model to estimate HSE, adding the sensitivity ratio to the
parameter can produce data for sensitivity analysis purposes"
# help([object])
from typing import List

import numpy as np
import os
import pandas

import matplotlib
import matplotlib.pyplot as plt
from matplotlib import animation

import math
from math import pi
#import altair as alt

from matplotlib.patches import Circle, RegularPolygon
from matplotlib.path import Path
from matplotlib.projections.polar import PolarAxes
from matplotlib.projections import register_projection
from matplotlib.spines import Spine
from matplotlib.transforms import Affine2D

# -----input necessary values-----
-----
sc_num = 35
path = "C:/Users/kaykh/Google Drive/Sarah/YU/Research/Papers/Paper5/"
m = 5 # number of rows in the catchment
n = 5 # number of cols in the catchment
se_num = 8 # number of LID demanded benefit for catchment
lid_num = 3 # number of LID types

# set dynamic variables )list, arrays, dataframes-----
-----
test_list = []
my_cells = []
my_lid = []
lid_df1 = pandas.DataFrame()
lid_df = pandas.DataFrame()
df = pandas.DataFrame()
df1 =pandas.DataFrame()

# generate a list of cell names and lid types-----
-----
for i in range(m*n):
    if i <= 8:
        cell = 'C0' + str(i+1)
    else:
        cell = 'C' + str(i + 1)
    my_cells.append(cell)
for i in range(lid_num):
```

```

if i <= 8:
    lid = 'lid0' + str(i + 1)
else:
    lid = 'lid' + str(i+1)
my_lid.append(lid)
# add two columns to df: 'sc_id' and 'cell_id'-----
-----
for sc in range(sc_num):
    rnd_seed = 1
    #create "Scenario id" column in df-----
    df1 = pandas.DataFrame(index=my_cells)
    lid_df1 = pandas.DataFrame(index=my_lid)
    sc_data = []
    for i in range(m*n):
        if sc <= 8:
            name = 'sc0' + str(sc + 1)
        else:
            name = 'sc' + str(sc + 1)
        sc_data.append(name)
    df1['sc_id'] = sc_data
    df1['cell_id'] = my_cells
    # create "Scenario id" column in lid_df-----
    lid_data = []
    for j in range(lid_num):
        if sc <= 8:
            name = 'sc0' + str(sc + 1)
        else:
            name = 'sc' + str(sc + 1)
        lid_data.append(name)
    lid_df1['sc_id']=lid_data
    lid_df1['lid_id']=my_lid

# generate random input variables-----
-----
#-----##### lid_df variables #####-----
-----#
# Lid_arr is the array of benefits of different lid types-----
np.random.seed(rnd_seed)
lid_arr = np.random.random((se_num, lid_num)) # row=8 and col=4
for i in range(se_num):
    lid_df1['lid_bnf' + str(i + 1)]= lid_arr[i]
print(lid_df1)
# Cost generation-----
np.random.seed(rnd_seed)
cost_arr = np.random.random(lid_num) # rows:lid_num cols:1 (1d array)
lid_df1['cost'] = cost_arr

#-----##### df variables #####-----
-----#
# generate seeni for all cells and all SE and EN variables-----
np.random.seed(rnd_seed)
seeni_arr = np.random.random((m * n, se_num)) # row=25 and col=8
seeni_temp = np.hsplit(seeni_arr, se_num)
for i in range(se_num):
    df1['se' + str(i+1)] = seeni_temp[i]
# Slope generation-----
np.random.seed(rnd_seed+1)
min_slope = 0
max_slope = 0.5
slope_norm = np.random.random(m*n)
slope = slope_norm * max_slope

# rainfall generation-----
np.random.seed(rnd_seed+25)
min_rainfall = 35.2
max_rainfall = 40.0

```

```

rainfall = np.full(m*n, min_rainfall) + np.random.random(m*n) * (max_rainfall - min_rainfall)
rainfall_norm = np.divide(rainfall-min_rainfall, max_rainfall-min_rainfall)

# ks generation-----
np.random.seed(rnd_seed+15)
min_ks = 0.01
max_ks = 69
ks_norm = np.full(m*n, min_ks) + np.random.random(m*n)
ks = ks_norm * (max_ks - min_ks)

# Dg generation-----
np.random.seed(rnd_seed+20)
min_dg = 0.01
max_dg = 117
dg_norm = np.full(m*n, min_dg) + np.random.random(m*n)
dg = dg_norm * (max_dg - min_dg)

# Dr generation-----
np.random.seed(rnd_seed+10)
min_dr = 0.01
max_dr = 117
dr_norm = np.full(m*n, min_dr) + np.random.random(m*n)
dr = dr_norm * (max_dr - min_dr)

#write input file-----
-----
#sns_ratio = 0.6+ sc*0.1
sns_ratio = 1
df1['rainfall'] = rainfall
df1['slope'] = slope
df1['ks'] = ks
df1['dg'] = dg.reshape(m * n)
df1['dr'] = dr.reshape(m * n)* sns_ratio
df1['slope_n'] = slope_norm
df1['rainfall_n'] = rainfall_norm
df1['ks_n'] = ks_norm
df1['dg_n'] = dg_norm.reshape(m * n)
df1['dr_n'] = dr_norm.reshape(m * n)
df = pandas.concat([df, df1], axis=0)
lid_df = pandas.concat([lid_df, lid_df1], axis=0)

df.to_csv(path + "input_site.csv")
lid_df.to_csv(path + "iput_lid.csv")

# Result generation-----
-----
#-----reading inputs-----
-----
my_input = path + 'input_site.csv'
df = pandas.read_csv(my_input)
ks=np.array(df['ks'])
dr=np.array(df['dr'])
dg=np.array(df['dg'])
rainfall=np.array(df['rainfall'])
slope=np.array(df['slope'])

my_input = path + 'iput_lid.csv'
lid_df = pandas.read_csv(my_input)

# -----HHI generation-----
-----
depth = np.minimum(ks, dr,dg)
runoff_temp = rainfall - ks
runoff = np.where(runoff_temp < 0, 0, runoff_temp)
s_nonlin = 1 + np.power(slope, 0.368)

```

```

hhi_temp = np.multiply(runoff, s_nonlin)
df['hhi'] = hhi_temp
df['runoff'] = runoff_temp
hhi = hhi_temp.reshape(sc_num, m, n)
#df['hhi'] = df['hhi'].replace(0 ,np.nan)
# -----Feasibility-----
feasible_num = 10 # number of feasible cells
feasible_row1 = [1,0,1,0,0]
feasible_row2 = [0,0,0,1,0]
feasible_row3 = [1,1,0,1,0]
feasible_row4 = [0,0,1,0,0]
feasible_row5 = [0,1,1,0,1]
feasible_cells = pandas.DataFrame([1,0,1,0,0, 0,0,0,1,0, 1,1,0,1,0, 0,0,1,0,0,0,1,1,0,1])

fsbl_cells = []
x= pandas.DataFrame()
for i in range(sc_num):
    x = pandas.concat([x, feasible_cells])

df['feasible'] = np.array(x)
df['feasible'] = df['feasible'].replace(0 ,np.nan)
# -----Catchment HHI generation-----
# sum of hhi for each feasible cell:
hhi_catch = np.zeros_like(hhi) # (sc_num, m, n)
for sc in range(sc_num):
    fsbl1_catch = hhi[sc][0, 0]
    fsbl2_catch = hhi[sc][2, 0] + hhi[sc][0, 1] + hhi[sc][1, 1] + hhi[sc][1, 0]
    fsbl3_catch = hhi[sc][2, 1]
    fsbl4_catch = hhi[sc][0, 2] + hhi[sc][1,2]
    fsbl5_catch = hhi[sc][3, 2] + hhi[sc][2, 2]
    fsbl6_catch = hhi[sc][1, 3] + hhi[sc][1, 4] + hhi[sc][0, 3]+ hhi[sc][0, 4]
    fsbl7_catch = hhi[sc][2, 3]
    fsbl8_catch = hhi[sc][4, 1] + hhi[sc][4, 0] + hhi[sc][3, 0] + hhi[sc][3, 1]
    fsbl9_catch = hhi[sc][4, 2] + hhi[sc][4, 3] + hhi[sc][3, 3] + hhi[sc][3, 4]+ hhi[sc][2, 4]
    fsbl10_catch = hhi[sc][4, 4]
    # Calculating sum of hhi based on catchment of each cell:
    for i in range(m):
        for j in range(n):
            if i == 0 and j == 0:
                hhi_catch[sc][i][j] = fsbl1_catch
            elif i == 2 and j == 0:
                hhi_catch[sc][i][j] = fsbl2_catch
            elif i == 2 and j == 1:
                hhi_catch[sc][i][j] = fsbl3_catch
            elif i == 0 and j == 2:
                hhi_catch[sc][i][j] = fsbl4_catch
            elif i == 3 and j == 2:
                hhi_catch[sc][i][j] = fsbl5_catch
            elif i == 1 and j == 3:
                hhi_catch[sc][i][j]= fsbl6_catch
            elif i == 2 and j == 3:
                hhi_catch[sc][i][j]= fsbl7_catch
            elif i == 4 and j == 1:
                hhi_catch[sc][i][j] = fsbl8_catch
            elif i == 4 and j == 2:
                hhi_catch[sc][i][j] = fsbl9_catch
            elif i == 4 and j == 4:
                hhi_catch[sc][i][j] = fsbl10_catch
hhi_catch_flat = np.ndarray.flatten(hhi_catch)
df['hhi_catch']=hhi_catch_flat
df['hhi_catch'] = df['hhi_catch'].replace(0 ,np.nan)
#-----HHCI generation-----
hhci_catch = np.zeros(shape=(lid_num, sc_num, m, n))

```



```

for sc in range(sc_num):
#-----Reading data
cost_col = lid_df.iloc[:, 11:12]
cost_arr = np.array(cost_col).reshape(sc_num, lid_num) # (sc_num, lid_num)
# -----hhci calculation
for i in range(lid_num):
    hhci_catch[i][sc] = np.divide(hhi_catch[sc], cost_arr[sc][i]) #(lid_num, sc_num, m, n)

# flatten hhci_catch into lid_num number of columns array
hhci_flat = np.zeros(shape=(lid_num, sc_num * m * n))
for j in range(lid_num):
    hhci_flat[j] = np.ndarray.flatten(hhci_catch[j]) #(lid_num, sc_num* m* n)
hhci = np.array(hhci_flat).T # (sc_num* m* n, lid_num)
hhci_n_arr = np.zeros_like(hhci) # (sc_num* m* n)

hhci_n_lid = []
for j in range(sc_num):
    start_r = j*25
    step = m*n
    end_r = start_r+step
    hhci_sel = hhci[start_r:end_r, 0:lid_num]
    hhci_max = np.nanmax(hhci_sel)
    hhci_n = hhci_sel/hhci_max
    hhci_n_arr[start_r:end_r, 0:lid_num] = hhci_n

# store hhci array in df
for k in range(lid_num):
    hhci_temp = hhci[:,k]
    df['hhci_lid' + str(k+1)]=hhci_temp

# store the normalized hhci array in df
for k in range(lid_num):
    hhci_n_temp = hhci_n_arr[:, k]
    df['hhci_norm' + str(k + 1)] = hhci_n_temp

# -----sei generation-----
-----

# seeni_arr (sc_num*m*n, seeni_num)-----
seeni_sel = df.iloc[:, 3: 3 + se_num] # (sc_num*m*n, seeni_num) for sc_num=2 is (50, 8)
seeni_arr = np.reshape(seeni_sel.to_numpy(), (sc_num, m*n, 8) ) # (50, 8) for sc_num=2
# lid_arr (seeni_num, lid_num)-----
lid_sel = lid_df.iloc[:, 3: 3 + se_num] # (sc_num*lid_num, seeni_num)
lid_arr1 = lid_sel.to_numpy() # (seeni_num, lid_num*sc_num)
lid_arr = np.reshape(lid_arr1, (sc_num, lid_num, se_num))

sei_list = []
for i in range(sc_num):
    lid_arr_t = lid_arr[i].T
    sei_temp1=np.dot(seeni_arr[i], lid_arr_t) # (25, 8).(8, 4)
    sei_temp2=np.divide(np.array(sei_temp1), se_num)
    sei_list.append(sei_temp2)
a = np.array(sei_list)
c = []
for i in range(sc_num):
    b = np.hsplit(a[i], lid_num)
    c.append(b)
d = np.array(c) #(sc_num, lid_num , m*n)
sei = np.reshape(d, (sc_num, lid_num, m , n))
#add sei to df-----
x = a.reshape(sc_num*m*n, lid_num)
for i in range(lid_num):
    name = 'sei' + str(i+1)
    y = x.T
    df[name] = y[i]

```

```

# -----Estimation of sei_neighbour-----
-----
sei_nei = np.full_like(sei, 0) #(sc_num, lid_num, m, n)
sei_nei_flat = []
indices1 = []
indices = np.full_like(sei, 0)
test_nei = np.full_like(sei, 0)
#iterate through sei_neigh
kernel_arr = [0.33, 0.66] # weight of neighbour cells
for l in range(sc_num):
    for k in range(lid_num):
        for i in range(m): # iterate through rows
            for j in range(n): # iterate through columns
                right2 = j + 3
                left2 = j - 2
                right1 = j + 2
                left1 = j - 1 # left and right neighbour indices
                top2 = i - 2
                bot2 = i + 3
                top1 = i - 1
                bot1 = i + 2 # top and bottom neighbour indices
                indices1.append([left1, right1, top1, bot1, left2, right2, top2, bot2]) # list of
index of neighbour cells
                if right1 > n-1 : # check if each boundary is in range and define the range
                    right1 = None
                if right2 > n-1:
                    right2 = None
                if bot1 > m-1 :
                    bot1 = None
                if bot2 > m-1 :
                    bot2 = None
                if left1 <= 0 :
                    left1 = None
                if left2 <= 0 :
                    left2 = None
                if top1 <= 0 :
                    top1 = None
                if top2 <= 0:
                    top2 = None
                indices[l][k][i][j] = left1
                center_val = sei[l][k][i][j]
                test = np.full_like(sei, 1)
                test_nei1= np.sum(test[l][k][left1:right1, top1:bot1])
                test_nei2 = np.sum(test[l][k][left2:right2, top2:bot2])
                test_nei[l][k][i][j] = test_nei2
                sei_nei1 = np.sum(sei[l][k][left1:right1, top1:bot1])
                sei_nei2 = np.sum(sei[l][k][left2:right2, top2:bot2])
                sei_nei3 = center_val + ((sei_nei2 - sei_nei1) * kernel_arr[0] + (sei_nei1 -
center_val)*kernel_arr[1])/((test_nei2-test_nei1)*0.66+(test_nei1-1)*0.33)
                sei_nei[l,k,i,j] = sei_nei3

e = np.reshape(sei_nei, (sc_num, lid_num, m*n))
e_list = []
for i in range(sc_num):
    e_t = e[i].T
    e_list.append(e_t)

f = np.array(e_list)
sei_df = pandas.DataFrame()
for i in range(sc_num):
    name = 'sei_nei_' + str(i + 1)
    g = pandas.DataFrame(f[i])
    sei_df = pandas.concat([g, sei_df], axis=0)

for i in range(lid_num):

```

```

name = 'sei_nei_' + str(i+1)
h = np.array(sei_df[i])
df[name] = h

# -----generating hse-----
-----
hse_temp1 = np.full_like(sei_nei, 0.00) # (sc_num, lid_num, m, n)

for lid in range(lid_num):
    hhci_temp2 = df['hhci_norm' + str(lid+1)]
    sei_temp3 = df['sei_nei_' + str(lid+1)]
    hse = (hhci_temp2+sei_temp3)/2
    col_name = 'hse_lid' + str(lid+1)
    df[col_name] = hse
    #hse_max = df.max(col_name)
    #hse_norm = np.divide(hse, hse_max)
    #df['hse_norm_lid' + str(lid + 1)] = hse_norm

for i in range(lid_num):
    name1 = 'hhci_lid' + str(i+1)
    name2 = 'sei_nei_' +str(i+1)
    name3 = 'hse_lid' + str(i+1)
    df[name1] = df[name1].replace(0, np.nan)
    df[name2] = df[name2].replace(0, np.nan)
    df[name3] = df[name3].replace(0, np.nan)

# -----generating Type_rnk-----
-----
df_sel = df[['hse_lid1', 'hse_lid2', 'hse_lid3']]
Type_rnk1 = df_sel.rank(axis=1, method='first', numeric_only=None, na_option='keep',
ascending=False, pct=False)
Type_rnk = Type_rnk1.rename(columns = {'hse_lid1':'Type_rnk1', 'hse_lid2':'Type_rnk2',
'hse_lid3':'Type_rnk3'}, inplace = False)
df = pandas.concat([df, Type_rnk], axis=1)
#-----Adding coordinates-----
-----
x = []
y = []
for sc in range(sc_num):
    for i in range(m):
        xi = i + 1
        for j in range(n):
            yj = j+1
            y.append(yj)
            x.append(xi)
x_arr = np.array(x)
y_arr = np.array(y)
df['x'] = x_arr
df['y'] = y_arr
# -----saving all results in one data frame-----
-----
df.to_csv(path+'output.csv')
df_feasible = df.dropna(how='all', subset=['feasible'])
df_feasible.to_csv(path + 'output_fsbl.csv')

```

Modified section of the code for sensitivity analysis of HSE to weights of HHCI and SEI

```
#By modifying this part of the previous code the weight sensitivity analysis can be performed
# -----generating hse-----
-----
hse_temp1 = np.full_like(sei_nei, 0.00) # (sc_num, lid_num, m, n)
for w in range(1,11):
    w_hhi = w*0.1
    w_sei = 1-w_hhi
    for lid in range(lid_num):
        hhci_temp2 = df['hhci_norm' + str(lid+1)]
        sei_temp3 = df['sei_nei_' + str(lid+1)]
        hse = w_hhi * hhci_temp2 + w_sei * sei_temp3
        col_name = 'hse_lid' + str(lid+1) + "w" + str(w)
        df[col_name] = hse
        #df = pandas.concat([df, df2], axis=0)
        #hse_max = df.max(col_name)
        #hse_norm = np.divide(hse, hse_max)
        #df['hse_norm_lid' + str(lid + 1)] = hse_norm
```

Model data (input and outputs)

1. Sensitivity analysis of HHI, LIDDI and HSE to the inputs

	Unnamed: 0	Sc_id	cell_id	se1	se2	se3	se4	se5	se6	se7	se8	rainfall	slope
	ks	dg	dr	n	LIDDI	hhi	runoff	feasible	hhi_catch	hhci_lid1	hhci_lid2	hhci_lid3	hhci_norm1
	hhci_norm2	hhci_norm3	sei1	sei2	sei3	sei_nei_1	sei_nei_2	sei_nei_3	hse_lid1	hse_lid2	hse_lid3		
	Type_rnk1	Type_rnk2	Type_rnk3	x	y								
0	C01	Sc01	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891					
	0.092338595		0.186260211	0.345560727	33.00685266	0.217997451	16.09475155	6.870223806					
	22.2596509		0.033847058	33.90848661	26.56699905	16.91210111	1	26.56699905					
	22.13916588		44.27833175	221.3916588	0.025272231	0.050544461	0.252722307	0.125908042					
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.167907644	0.162990632					
	0.258030216		2	3	1	1	1						
1	C02	Sc01	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436				
	0.027387593		0.67046751	33.61584746	0.012963116	36.78293892	34.9928391	3.448308502					
	0.172396809		0	-3.16709146			0	0					
	0.257404041		0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	0.222682445					
	0.189169138		0.193388639	1	3	2	1	2					
2	C03	Sc01	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569					
	0.968261576		0.313424178	0.692322616	34.33269727	0.274831239	38.68279349	85.51575292					
	55.36183542		0.421304567	0	0	-4.35009622	1	35.57040589	29.64200491				
	59.28400982		296.4200491	0.033836848	0.067673696	0.338368478	0.25038454	0.237553697					
	0.192031501		0.413221665	0.397937162	0.354009513	0.223529256	0.232805429	0.346188996					
	3	2	1	1	3								
3	C04	Sc01	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042					
	0.878142503		0.098346834	0.421107625	34.39295572	0.217661196	3.83597854	3.698785078					
	85.97992038		0.01822255	68.76316915	47.99165001	30.55697718							
	0	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941					
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1	4				
4	C05	Sc01	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928					
	0.834625672		0.018288277	0.750144315	34.62721874	0.210183901	25.57658235	25.26080431					
	50.3295197		0.124450664	22.61652996	14.14858807	9.05063639							
	0	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602					
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3	1	5			
5	C06	Sc01	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007					
	0.447893526		0.908595503	0.293614148	32.66121361	0.165167411	16.08025417	7.109863301					
	57.96001621		0.035027674	39.4509017	25.12780432	16.58095944							
	0	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035					
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2	2	1			

6	C07	Sc01	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	32.89617511	0.102324317	48.2051179	36.53268887
	2.665127499		0.179983081	0	-15.30894279			0
	0	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
7	C08	Sc01	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	33.54903337	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	51.73217517	35.57040589	21.56330236		
	0	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
8	C09	Sc01	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	34.24867063	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	66.28286726	42.98304685	28.70705807	1	105.1232849
	87.60273744		175.2054749	876.0273744	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4			0.716039279
9	C10	Sc01	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	32.68146174	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-32.92877751			0
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
10	C11	Sc01	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	32.63766631	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	0	-6.94061211	1	25.12780432	20.93983693
	41.87967387		209.3983693	0.023903176	0.047806353	0.239031765	0.316867923	0.266455347
	0.264174875		0.486389832	0.435666719	0.417511021	0.255146504	0.241736536	0.328271393
	2	3	1	3	1			
11	C12	Sc01	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	33.67181962	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	66.91032207	44.52214838	27.60122813	1	44.52214838
	37.10179032		74.20358064	371.0179032	0.042352318	0.084704637	0.423523184	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.227590998	0.249292262
	0.398354	3	2	1	3	2		
12	C13	Sc01	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	32.93436494	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-17.61050392			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
13	C14	Sc01	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	34.31150682	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	56.83555941	36.44809226	22.68999137	1	36.44809226
	30.37341021		60.74682043	303.7341021	0.034671759	0.069343518	0.346717592	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236884791	0.268492897
	0.358819046		3	2	1	3	4	
14	C15	Sc01	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	32.89671567	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	34.27952698	21.15436922	14.93990832		

	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
15	0.38826343 C16 Sc01 0.538831064 75.14665628 0 0.376351488	0.210827114 C16 0.019880134 0.552821979 0.503571269 0 0.204734808	0.230986491 0.026210987 0.842030892 28.55622033 0.198021052 0.200350357	0.194131715 0.028306488 32.96533619 20.55454145 0.185581091 0.188175744	2 1 0.392667574 12.02775039 0.191572754 1	3 3 20.9375858 0.409469615 2 3	5 0.860027949 102.2141214 0.400700715 0.561030219
16	C17 Sc01 0.018647289 3.56627786 0 0.195078226	0.124173315 C17 0.800632673 0.443193522 0.154114011 0.211045796	0.279183679 0.232974274 0 0.183917483 0.212449365	0.585759271 34.89172787 -13.8573453 0.218846089 3	0.969595748 0.426987646 0.390156452 0.422091592 2	4 48.74907317 0.422091592 0.424898731 2	1 89.95873932 0 0.424898731 4
17	C18 Sc01 0.136455226 14.82699307 2.703791649 0.230647918 0.178941928	0.807105196 C18 0.05991769 0.56511885 5.407583298 0.139241534	0.387860644 0.121343456 4.736875041 27.03791649 0.36632712	0.863541855 34.75005726 3.244549979 0.003086424 0.427568554	0.747121643 0.247118419 2.03057783 0.006172847 0.327019619	0.556240234 32.71947943 1 3.244549979 0.030864237	0.168545737 0.216870701 114.7069548 0.168545737 0.216870701
18	C19 Sc01 0.01255598 38.18171179 0 0.385127801	0.044551879 C19 0.07197428 0.443400275 0 0.208198327	0.107494129 0.96727633 42.15964078 0.19335296 0.194126634	0.225709339 33.75634355 31.51454714 0.154863434 0.192563901	0.71298898 0.423280743 18.22930626 0.16721044 1	0.559716982 15.52703729 0.416396653 0.195429481 2	0.00070565 90.00070565 0.388253269 0.195429481 4
19	C20 Sc01 0.581358927 19.64406076 0 0.473734591	0.568100462 C20 0.970019989 0.227232539 0 0.23140003	0.203293235 0.846828801 4.03760526 0.266503103 0.208910304	0.252325745 33.51821798 2.613086741 0.213730709 0.236867296	0.743825854 0.039822739 2.00177416 0.290225506 2	0.195429481 31.51644382 0.462800059 0.156791395 1	0.417820608 46.12331125 0.417820608 0.156791395 4
20	C21 Sc01 0.070022144 0.241335248 0 0.184443254	0.239847759 C21 0.486345111 54.60566745 0.167087112 0.17732464	0.493769714 0.025266859 40.02508472 0.139838178 0.165746932	0.619955718 0.252623045 24.97334352 0.158385453 1	0.8289809 9.029325069 0.368886507 0.35464928 2	0.156791395 48.98585736 0.35464928 0.156791395 5	0.018576202 89.96292202 0 0.331493863 1
21	C22 Sc01 0.380141173 96.89993412 100.9660436 0.255171744	0.606329462 C22 0.550948219 0.41692077 504.8302181 0.482159781	0.568851437 0.745334431 0 0.05762722 0.476288524	0.317362409 33.66549267 -30.33563399 0.115254439 0.435601111	0.988616154 0.032643252 60.57962617 0.576272195 0.2698935	0.579745219 64.00112666 50.48302181 0.273632139 0.295771482	0.62593646 84.62593646 0.48302181 0.256849416 0.505936653
22	C23 Sc01 0.21017401 41.4875192 92.13667184 0.135993177	0.669232893 C23 0.752755554 0.161768675 460.6833592 0.31838757	0.264919558 0.066536481 0 0.052587781 0.379056788	0.066334834 34.98772802 -4.7813042 0.105175562 0.311830131	0.370084198 0.214061164 55.2820031 0.525877812 0.185487676	0.629717507 39.76903222 46.06833592 0.126338191 0.242116175	0.83555671 32.83555671 0.06833592 0.188706502 0.418853972
23	C24 Sc01 0.92480797	0.260315099 C24 0.26329677	0.804754564 0.065961091	0.193434283 32.5289095	0.639460881 0.048265458	0.524670309 33.25451259	0.524670309 101.091395

	38.46617124	0.49804001	0	0	-0.72560309				0
	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	0.377206528		
	0.204296641	0.204256539	0.188603264	1	2	3	4		
24	C25 Sc01	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573		
	0.234362086	0.616778357	0.949016321	34.92898391	0.063579986	22.39183764	108.0009528		
	14.23314753	0.532080852	28.10750344	17.08514789	12.53714627	1	17.08514789		
	14.23762324	28.47524648	142.3762324	0.016252487	0.032504973	0.162524867	0.297089204		
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.246390979	0.223666667		
	0.311566865	2	3	1	5	5			
25	C01 Sc02	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891		
	0.092338595	0.186260211	0.345560727	36.67466144	0.217997451	16.09475155	6.870223806		
	22.2596509	0.033847058	41.26238333	32.32871202	20.57990989	1	32.32871202		
	26.94059335	53.88118671	269.4059335	0.026239924	0.052479848	0.262399238	0.125908042		
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.168391491	0.163958325		
	0.262868682	2	3	1	1	1			
26	C02 Sc02	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436	
	0.027387593	0.67046751	37.38515537	0.012963116	36.78293892	34.9928391	3.448308502		
	0.172396809	1.069599618	0.723899385	0.60221645			0		
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277		
	0.222682445	0.189169138	0.193388639	1	3	2	1	2	
27	C03 Sc02	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569		
	0.968261576	0.313424178	0.692322616	38.22148014	0.274831239	38.68279349	85.51575292		
	55.36183542	0.421304567	0	-0.46131335	1	41.76981399	34.80817833		
	69.61635666	348.0817833	0.033902889	0.067805778	0.33902889	0.25038454	0.237553697		
	0.192031501	0.413221665	0.397937162	0.354009513	0.223562277	0.23287147	0.346519202		
	3	2	1	3					
28	C04 Sc02	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042		
	0.878142503	0.098346834	0.421107625	38.29178167	0.217661196	3.83597854	3.698785078		
	85.97992038	0.01822255	77.5367997	54.1150008	34.45580313				
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941		
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1	4
29	C05 Sc02	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928		
	0.834625672	0.018288277	0.750144315	38.56508853	0.210183901	25.57658235	25.26080431		
	50.3295197	0.124450664	32.45682696	20.30454165	12.98850618				
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602		
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1	5
30	C06 Sc02	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007		
	0.447893526	0.908595503	0.293614148	36.27141588	0.165167411	16.08025417	7.109863301		
	57.96001621	0.035027674	48.04061783	30.59892658	20.19116171				
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035		
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2	1
31	C07 Sc02	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116		
	0.265546659	0.491573159	0.053362545	36.54553763	0.102324317	48.2051179	36.53268887		
	2.665127499	0.179983081	0	-11.65958027			0		
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132		
	0.168102684	0.166496609	0.169732566	2	3	1	2	2	

32	C08	Sc02	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	37.30720559	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	60.74834627	41.76981399	25.32147458		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
33	C09	Sc02	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	38.12344907	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	75.2294972	48.7847484	32.58183651	1	123.2042908
	102.6702424		205.3404847	1026.702424	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
34	C10	Sc02	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	36.29503869	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-29.31520056			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
35	C11	Sc02	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	36.24394403	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	0	-3.33433439	1	31.32282596	26.10235497
	52.20470993		261.0235497	0.025423486	0.050846973	0.254234863	0.316867923	0.266455347
	0.264174875		0.486389832	0.435666719	0.417511021	0.255906659	0.243256846	0.335872942
	2	3	1	3	1			
36	C12	Sc02	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	37.45045623	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	76.0704142	50.61727644	31.37986473	1	50.61727644
	42.1810637		84.3621274	421.810637	0.041084021	0.082168042	0.410840208	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226956849	0.248023965
	0.392012512		3	2	1	3	2	
37	C13	Sc02	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	36.59009243	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-13.95477643			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
38	C14	Sc02	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	38.19675796	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	66.56762226	42.68916964	26.57524251	1	42.68916964
	35.57430803		71.14861607	355.7430803	0.034649093	0.069298187	0.346490933	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236873458	0.268470231
	0.358705716		3	2	1	3	4	
39	C15	Sc02	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	36.54616828	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	42.65317336	26.32186197	18.58936093		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
40	C16	Sc02	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	36.62622555	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	37.24788417	26.81073231	15.68863975		

	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
41	C17 Sc02	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	38.87368252	0.426987646	48.74907317	89.95873932	
	3.56627786	0.443193522	0	-9.87539065			0	
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731	
	0.195078226	0.211045796	0.212449365	3	2	1	4	2
42	C18 Sc02	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	38.70840014	0.247118419	32.71947943	114.7069548	
	14.82699307	0.56511885	13.97078635	9.569370982	5.98892071	1	9.569370982	
	7.974475818	15.94895164	79.74475818	0.007767076	0.015534152	0.077670761	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.187047098	0.221551353	
	0.20234519	3	1	2	4	3		
43	C19 Sc02	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	37.54906748	0.423280743	15.52703729	90.00070565	
	38.18171179	0.443400275	50.93122409	38.07135054	22.02203019			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
44	C20 Sc02	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	37.27125431	0.039822739	31.51644382	46.12331125	
	19.64406076	0.227232539	11.60752974	7.512245531	5.75481049			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
45	C21 Sc02	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	37.83644669	0.252623045	9.029325069	48.98585736	89.96292202	
	0.241335248	62.98844615	46.16952802	28.80712162			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
46	C22 Sc02	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	37.44307478	0.032643252	64.00112666	84.62593646	
	96.89993412	0.41692077	0	-26.55805188	1	72.98026033	60.81688361	
	121.6337672	608.1688361	0.059235161	0.118470322	0.592351612	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.270697471	0.297379423	0.513976362	
	3	2	1	5	2			
47	C23 Sc02	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	38.9856827	0.214061164	39.76903222	32.83555671	
	41.4875192	0.161768675	0	-0.78334952	1	75.7062835	63.08856958	
	126.1771392	630.8856958	0.061447765	0.122895531	0.614477653	0.126338191	0.188706502	
	0.135993177	0.31838757	0.379056788	0.311830131	0.189917668	0.250976159	0.463153892	
	3	2	1	5	3			
48	C24 Sc02	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	36.11706108	0.048265458	33.25451259	101.091395	
	38.46617124	0.49804001	5.547637798	3.800825465	2.86254849			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
49	C25 Sc02	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	38.9171479	0.063579986	22.39183764	108.0009528	

	14.23314753	0.532080852	37.04871946	22.52006665	16.52531026	1	22.52006665	
	18.76672221	37.53344442	187.6672221	0.018278638	0.036557277		0.182786383	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863		0.247404055	0.225692819
	0.321697623	2	3	1	5	5		
50	C01 Sc03	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	40.34247022	0.217997451	16.09475155	6.870223806	
	22.2596509	0.033847058	48.61628005	38.090425	24.24771867	1	38.090425	31.74202083
	63.48404166	317.4202083	0.026959936	0.053919871	0.269599356		0.125908042	0.105685808
	0.089720661	0.310543058	0.275436802	0.263338126	0.168751497		0.164678336	0.266468741
	2	3	1	1	1			
51	C02 Sc03	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	41.15446328	0.012963116	36.78293892	34.9928391	3.448308502	
	0.172396809	7.76428606	5.254827887	4.37152436				0
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	2
52	C03 Sc03	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	42.11026302	0.274831239	38.68279349	85.51575292	
	55.36183542	0.421304567	8.399457673	5.558305041	3.42746953	1	53.52752715	
	44.60627262	89.21254525	446.0627262	0.037886127	0.075772254	0.378861271	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.225553896	0.236854708	
	0.366435392	3	2	1	3			
53	C04 Sc03	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	42.19060763	0.217661196	3.83597854	3.698785078	
	85.97992038	0.01822255	86.31043026	60.23835161	38.35462909			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
54	C05 Sc03	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	42.50295832	0.210183901	25.57658235	25.26080431	
	50.3295197	0.124450664	42.29712396	26.46049523	16.92637597			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
55	C06 Sc03	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	39.88161814	0.165167411	16.08025417	7.109863301	
	57.96001621	0.035027674	56.63033395	36.07004882	23.80136397			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
56	C07 Sc03	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	40.19490014	0.102324317	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-8.01021776			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
57	C08 Sc03	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	41.06537782	0.309635483	11.98573101	78.84076537	
	58.18750434	0.388419366	69.7645174	47.96922211	29.07964681			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2

58	C09	Sc03	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	41.99822751	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	84.17612713	54.58644995	36.45661495	1	141.2852968
	117.7377473		235.4754946	1177.377473	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
59	C10	Sc03	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	39.90861565	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-25.7016236			0
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
60	C11	Sc03	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	39.85022175	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	0.738568111	0.448787815	0.27194333	1	41.77366452
	34.8113871		69.6227742	348.113871	0.029566887	0.059133775	0.295668873	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.25797836	0.247400247
	0.356589947		2	3	1	3	5	
61	C12	Sc03	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	41.22909283	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	85.23050631	56.71240447	35.15850134	1	56.71240447
	47.26033706		94.52067412	472.6033706	0.040140344	0.080280688	0.401403442	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226485011	0.247080288
	0.387294129		3	2	1	3	2	
62	C13	Sc03	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	40.24581992	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-10.29904894			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
63	C14	Sc03	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	42.0820091	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	76.29968511	48.93024703	30.46049365	1	48.93024703
	40.77520585		81.55041171	407.7520585	0.034632229	0.069264457	0.346322286	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236865026	0.268453367
	0.358621393		3	2	1	3	4	
64	C15	Sc03	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	40.1956209	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	51.02681976	31.48935473	22.23881355		
	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
65	C16	Sc03	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	40.28711492	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	45.93954804	33.06692319	19.34952912		
	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
66	C17	Sc03	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	42.85563716	0.426987646	48.74907317	89.95873932
	3.56627786		0.443193522	0	-5.89343601			0

	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
67	C18	Sc03	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	42.66674301	0.247118419	32.71947943	114.7069548
	14.82699307		0.56511885	23.20469764	15.89419197	9.94726358	1	15.89419197
	13.24515997		26.49031995	132.4515997	0.011249714	0.022499428	0.112497141	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.188788417	0.225033991
	0.21975838		3	1	2	4	3	
68	C19	Sc03	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	41.34179141	0.423280743	15.52703729	90.00070565
	38.18171179		0.443400275	59.70280739	44.62815393	25.81475412		
	0		0	0	0.19335296	0.154863434	0.16721044	0.416396653
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
69	C20	Sc03	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	41.02429064	0.039822739	31.51644382	46.12331125
	19.64406076		0.227232539	19.17745423	12.41140432	9.50784682		
	0		0	0	0.266503103	0.213730709	0.290225506	0.462800059
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
70	C21	Sc03	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	41.67022478	0.252623045	9.029325069	48.98585736	0.018576202
	0.241335248		71.37122482	52.31397131	32.64089971			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
71	C22	Sc03	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	41.22065689	0.032643252	64.00112666	84.62593646
	96.89993412		0.41692077	0	-22.78046977	1	85.3808945	71.15074541
	142.3014908		711.5074541	0.06043155	0.1208631	0.604315498	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271295665	0.298575812	0.519958305
	3	2	1	5	2			
72	C23	Sc03	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	42.98363737	0.214061164	39.76903222	32.83555671
	41.4875192		0.161768675	6.945321784	5.037516617	3.21460515	1	102.1315195
	85.10959956		170.2191991	851.0959956	0.072287437	0.144574873	0.722874367	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.195337503	0.26181583
	0.517352249		3	2	1	5	3	
73	C24	Sc03	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	39.70521266	0.048265458	33.25451259	101.091395
	38.46617124		0.49804001	12.50149916	8.565089876	6.45070007		
	0		0	0	0.195074589	0.194999729	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
74	C25	Sc03	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	42.90531188	0.063579986	22.39183764	108.0009528
	14.23314753		0.532080852	45.98993546	27.95498541	20.51347424	1	27.95498541
	23.29582117		46.59164235	232.9582117	0.019786196	0.039572392	0.197861958	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248157833	0.227200376
	0.329235411		2	3	1	5	5	

75	C01	Sc04	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	22.2596509		0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906		2	3	1	1		
76	C02	Sc04	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	0.878117436
	0.172396809		14.4589725	9.78575639	8.14083227			3.448308502
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
77	C03	Sc04	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	55.36183542		0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511		3	2	1	3		
78	C04	Sc04	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	85.97992038		0.01822255	95.08406081	66.3617024	42.25345504		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
79	C05	Sc04	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	50.3295197		0.124450664	52.13742096	32.61644881	20.86424576		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
80	C06	Sc04	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301
	57.96001621		0.035027674	65.22005008	41.54117107	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
81	C07	Sc04	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887
	2.665127499		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
82	C08	Sc04	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
83	C09	Sc04	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
								0.232017403

	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	1	4				
84	C10 Sc04	C10 0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	100.7044175	0.342126169	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
85	C11 Sc04	C11 0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	86.56844337	0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2	3	1	3		
86	C12 Sc04	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	13.89093305	0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401	3	2	1	3	2	
87	C13 Sc04	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	105.7477489	0.082559047	0	-6.64332145			0
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2	1	3	3
88	C14 Sc04	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	101.4483754	0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204	3	2	1	3	4	
89	C15 Sc04	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	20.48338339	0.29160088	59.40046614	36.65684749	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
90	C16 Sc04	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	75.14665628	0.503571269	54.63121188	39.32311405	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
91	C17 Sc04	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	3.56627786	0.443193522	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
92	C18 Sc04	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548

	14.82699307	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379	
	0.233220321	3	2	1	4	3		
93	C19 Sc04	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	38.18171179	0.443400275	68.47439068	51.1849573	29.60747804			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
94	C20 Sc04	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	19.64406076	0.227232539	26.74737871	17.31056311	13.26088315			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
95	C21 Sc04	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	89.96292202	
	0.241335248	79.75400352	58.45841461	36.47467781			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
96	C22 Sc04	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	96.89993412	0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2			
97	C23 Sc04	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	41.4875192	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781	3	2	1	5	3		
98	C24 Sc04	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	
	38.46617124	0.49804001	19.45536051	13.32935429	10.03885165			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
99	C25 Sc04	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528	
	14.23314753	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789	2	3	1	5	5		
100	C01 Sc05	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	47.67808777	0.217997451	16.09475155	6.870223806	
	22.2596509	0.033847058	63.32407347	49.61385093	31.58333622	1	49.61385093	
	41.34487577	82.68975155	413.4487577	0.027959765	0.05591953	0.279597652	0.125908042	

	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169251412	0.165678166	
	0.271467889	2	3	1	1	1		
101	C02 Sc05	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	48.6930791	0.012963116	36.78293892	34.9928391	3.448308502	
	0.172396809	21.15365894	14.31668489	11.91014018			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	
102	C03 Sc05	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	49.88782878	0.274831239	38.68279349	85.51575292	
	55.36183542	0.421304567	27.45938916	18.17113284	11.20503529	1	78.53917118	
	65.44930932	130.8986186	654.4930932	0.044260559	0.088521119	0.442605593	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.228741112	0.24322914	
	0.398307553	3	2	1	3			
103	C04 Sc05	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	49.98825953	0.217661196	3.83597854	3.698785078	
	85.97992038	0.01822255	103.8576914	72.48505319	46.15228099			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	
104	C05 Sc05	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	50.3786979	0.210183901	25.57658235	25.26080431	
	50.3295197	0.124450664	61.97771796	38.7724024	24.80211555			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	
105	C06 Sc05	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	47.10202268	0.165167411	16.08025417	7.109863301	
	57.96001621	0.035027674	73.80976622	47.01229332	31.02176851			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	
106	C07 Sc05	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	47.49362518	0.102324317	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-0.71149272			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	
107	C08 Sc05	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	48.58172228	0.309635483	11.98573101	78.84076537	
	58.18750434	0.388419366	87.79685965	60.36803834	36.59599127			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	
108	C09 Sc05	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	49.74778439	0.149827337	5.541612561	37.21620286	
	111.3518603	0.183350502	102.069387	66.18985304	44.20617183	1	177.4473086	
	147.8727572	295.7455144	1478.727572	0.1	0.2	1	0.178780994	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403	
	3	2	1	2	4			
109	C10 Sc05	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	47.13576956	0.133413638	65.61023925	69.4442434	
	100.7044175	0.342126169	0	0	-18.47446969		0	

	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
110	C11	Sc05	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	47.06277718	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	20.32707371	12.35166108	7.48449876	1	73.6806393
	61.40053275		122.8010655	614.0053275	0.041522545	0.083045091	0.415225454	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.263956189	0.259355905
	0.416368238		2	3	1	3	5	
111	C12	Sc05	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	48.78636604	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	103.5506905	68.90266056	42.71577454	1	68.90266056
	57.4188838		114.8377676	574.188838	0.038829927	0.077659854	0.388299271	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.225829802	0.245769871
	0.380742043		3	2	1	3	2	
112	C13	Sc05	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	47.5572749	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-2.98759396			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
113	C14	Sc05	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	49.85251137	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	95.76381078	61.41240178	38.23099592	1	61.41240178
	51.17700148		102.354003	511.7700148	0.03460881	0.06921762	0.346088099	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236853316	0.268429948
	0.3585043		2	1	3	4		
114	C15	Sc05	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	47.49452612	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	67.77411252	41.82434024	29.53771877		
	0		0	0	0.251517278	0.292575574	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
115	C16	Sc05	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	47.60889364	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	63.32287572	45.57930492	26.67130784		
	0		0	0	0.198021052	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
116	C17	Sc05	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	50.81954646	0.426987646	48.74907317	89.95873932
	3.56627786		0.443193522	5.184619305	3.584252256	2.07047329		
	0		0	0	0.154114011	0.183917483	0.218846089	0.422091592
	0.424898731		0.195078226	0.211045796	0.212449365	3	2	1
117	C18	Sc05	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	50.58342877	0.247118419	32.71947943	114.7069548
	14.82699307		0.56511885	41.67252026	28.54383398	17.86394934	1	28.54383398
	23.78652831		47.57305663	237.8652831	0.016085808	0.032171617	0.160858083	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.191206464	0.229870085
	0.243938851		3	2	1	4	3	

118	C19	Sc05	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
				0.01255598	0.07197428	0.96727633	48.92723926	0.423280743	15.52703729
				38.18171179	0.443400275	77.24597398	57.74176069	33.40020197	90.00070565
				0	0	0.19335296	0.154863434	0.16721044	0.416396653
				0.385127801	0.208198327	0.194126634	0.192563901	1	2
								3	4
119	C20	Sc05	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
				0.581358927	0.970019989	0.846828801	48.5303633	0.039822739	31.51644382
				19.64406076	0.227232539	34.3173032	22.2097219	17.01391948	46.12331125
				0	0	0.266503103	0.213730709	0.290225506	0.462800059
				0.473734591	0.23140003	0.208910304	0.236867296	2	3
								1	4
120	C21	Sc05	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
				0.070022144	0.486345111	49.33778098	0.252623045	9.029325069	48.98585736
				0.241335248	88.13678221	64.6028579	40.30845591		89.96292202
				0	0	0.167087112	0.139838178	0.158385453	0.35464928
				0.184443254	0.17732464	0.165746932	1	2	3
								5	1
121	C22	Sc05	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
				0.380141173	0.550948219	0.745334431	48.77582111	0.032643252	64.00112666
				96.89993412	0.41692077	0	-15.22530555	1	113.7664151
				189.6106918	948.053459	0.064112787	0.128225574	0.64112787	0.273632139
				0.255171744	0.482159781	0.476288524	0.435601111	0.273136284	0.302257049
				3	2	1	5	1	0.538364491
122	C23	Sc05	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
				0.21017401	0.752755554	0.066536481	50.97954671	0.214061164	39.76903222
				41.4875192	0.161768675	24.22090019	17.56767951	11.21051449	157.4371211
				131.1976009	262.3952018	1311.976009	0.088723307	0.177446615	0.887233074
				0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.126338191
				0.599531603	3	2	1	5	0.278251701
123	C24	Sc05	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
				0.92480797	0.26329677	0.065961091	46.88151583	0.048265458	33.25451259
				38.46617124	0.49804001	26.40922189	18.09361871	13.62700324	101.091395
				0	0	0.195074589	0.194999729	0.172101157	0.408593283
				0.377206528	0.204296641	0.204256539	0.188603264	1	2
								3	5
124	C25	Sc05	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
				0.234362086	0.616778357	0.949016321	50.88163986	0.063579986	22.39183764
				14.23314753	0.532080852	63.8723675	38.82482294	28.48980222	108.0009528
				32.35401912	64.70803824	323.5401912	0.021879635	0.043759269	0.218796347
				0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.297089204
				0.339702605	2	3	1	5	0.229293815
125	C01	Sc06	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
				0.092338595	0.186260211	0.345560727	51.34589655	0.217997451	16.09475155
				22.2596509	0.033847058	70.67797019	55.3755639	35.251145 1	55.3755639
				92.29260651	461.4630325	0.028320995	0.05664199	0.283209949	0.125908042
				0.089720661	0.310543058	0.275436802	0.263338126	0.169432027	0.105685808
				2	3	1	1	0.166039396	0.273274037
126	C02	Sc06	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
				0.027387593	0.67046751	52.46238701	0.012963116	36.78293892	34.9928391
				0.172396809	27.84834538	18.84761339	15.67944809		3.448308502
									0

	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445		0.189169138	0.193388639	1	3	2	1
127	C03	Sc06	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	53.77661165	0.274831239	38.68279349	85.51575292
	55.36183542		0.421304567	36.98935487	24.47754673	15.09381816	1	91.04499316
	75.87082764		151.7416553	758.7082764	0.046563585	0.09312717	0.465635851	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.229892625	0.245532166
	0.409822682		3	2	1	1	3	
128	C04	Sc06	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	53.88708549	0.217661196	3.83597854	3.698785078
	85.97992038		0.01822255	112.6313219	78.608404	50.05110695		
	0	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249		0.189644971	0.16330745	1	2	3
129	C05	Sc06	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	54.31656769	0.210183901	25.57658235	25.26080431
	50.3295197		0.124450664	71.81801496	44.92835598	28.73998534		
	0	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
130	C06	Sc06	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	50.71222495	0.165167411	16.08025417	7.109863301
	57.96001621		0.035027674	82.39948235	52.48341558	34.63197078		
	0	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
131	C07	Sc06	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	51.1429877	0.102324317	48.2051179	36.53268887
	2.665127499		0.179983081	5.332117802	4.207580453	2.9378698		
	0	0	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219
	0.339465132		0.168102684	0.166496609	0.169732566	2	3	1
132	C08	Sc06	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	52.3398945	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	96.81303075	66.56744644	40.35416349		
	0	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
133	C09	Sc06	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	53.62256282	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	111.0160169	71.99155458	48.08095026	1	195.5283146
	162.9402621		325.8805243	1629.402621	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
134	C10	Sc06	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	50.74934652	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-14.86089273			0
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
135	C11	Sc06	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	50.6690549	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	30.12132653	18.30309773	11.09077648	1	93.84170715

	78.20142263	156.4028453	782.0142263	0.047993922	0.095987844	0.479939222	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.267191877	0.265827282
	0.448725122	2	3	1	1		
136	C12 Sc06	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	52.56500265	0.264571047	6.070591495	102.6475506
	13.89093305	0.505706614	112.7107827	74.99778862	46.49441115	1	74.99778862
	62.49815718	124.9963144	624.9815718	0.038356485	0.07671297	0.38356485	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.225593081	0.245296429
	0.378374833	3	2	1	3	2	
137	C13 Sc06	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102	0.885942099	0.35726976	51.21300239	0.067289973	50.54486886	16.75770835
	105.7477489	0.082559047	1.395630399	0.915618596	0.66813353		
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791
	0.373298543	0.193600456	0.194835395	0.186649271	2	1	3
138	C14 Sc06	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285	0.172340508	0.13713575	53.73776251	0.256789061	11.62151545	22.00870416
	101.4483754	0.108428766	105.4958736	67.65347916	42.11624706	1	67.65347916
	56.3778993	112.7557986	563.778993	0.034600349	0.069200698	0.34600349	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236849086	0.268421487
	0.358461995	3	2	1	3	4	
139	C15 Sc06	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536	0.711524759	0.124270962	51.14397873	0.092219933	17.95680735	59.18869803
	20.483383339	0.29160088	76.1477589	46.99183299	33.18717138		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
140	C16 Sc06	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064	0.552821979	0.842030892	51.26978301	0.392667574	20.9375858	102.2141214
	75.14665628	0.503571269	72.01453959	51.8354958	30.33219721		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
141	C17 Sc06	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289	0.800632673	0.232974274	54.8015011	0.426987646	48.74907317	89.95873932
	3.56627786	0.443193522	15.15573026	10.47752152	6.05242793		
	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592
	0.424898731	0.195078226	0.211045796	0.212449365	3	2	1
142	C18 Sc06	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226	0.05991769	0.121343456	54.54177164	0.247118419	32.71947943	114.7069548
	14.82699307	0.56511885	50.90643155	34.86865496	21.82229221	1	35.78427356
	29.82022797	59.64045593	298.2022797	0.018301326	0.036602651	0.183013256	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.192314223	0.232085603
	0.255016438	3	2	1	4	3	
143	C19 Sc06	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598	0.07197428	0.96727633	52.71996318	0.423280743	15.52703729	90.00070565
	38.18171179	0.443400275	86.01755727	64.29856406	37.19292589		
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
						4	4

144	C20	Sc06	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
				0.970019989	0.846828801	52.28339963	0.039822739	31.51644382	46.12331125
				0.227232539	41.88722768	27.10888069	20.76695581		
				0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
				0.473734591	0.23140003	0.208910304	0.236867296	2	3
								1	4
									5
145	C21	Sc06	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
				0.070022144	0.486345111	53.17155908	0.252623045	9.029325069	48.98585736
				0.241335248	96.51956091	70.7473012	44.14223401		89.96292202
				0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928
				0.184443254	0.17732464	0.165746932	1	2	3
								5	1
146	C22	Sc06	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
				0.380141173	0.550948219	0.745334431	52.55340322	0.032643252	64.00112666
				96.89993412	0.41692077	0	-11.44772344	1	133.0603185
				221.7671975	1108.835988	0.068051688	0.136103376	0.68051688	0.273632139
				0.255171744	0.482159781	0.476288524	0.435601111	0.275105734	0.30619595
				3	2	1			0.558058996
147	C23	Sc06	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
				0.21017401	0.752755554	0.066536481	54.97750138	0.214061164	39.76903222
				41.4875192	0.161768675	32.8586894	23.83276096	15.20846916	1
				154.2416015	308.483203	1542.416015	0.094661442	0.189322884	0.946614419
				0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.206524506
				0.629222275	3	2	1	5	3
148	C24	Sc06	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
				0.92480797	0.26329677	0.065961091	50.46966741	0.048265458	33.25451259
				38.46617124	0.49804001	33.36308325	22.85788312	17.21515482	101.091395
				0	0	0.195074589	0.194999729	0.172101157	0.408593283
				0.377206528	0.204296641	0.204256539	0.188603264	1	2
								3	5
									4
149	C25	Sc06	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
				0.234362086	0.616778357	0.949016321	54.86980384	0.063579986	22.39183764
				14.23314753	0.532080852	72.8135835	44.2597417	32.4779662	1
				36.88311808	73.76623616	368.8311808	0.022635976	0.045271951	44.2597417
				0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.226359757
				0.34348431	2	3	1	5	5
150	C01	Sc07	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
				0.092338595	0.186260211	0.345560727	55.01370533	0.217997451	16.09475155
				22.2596509	0.033847058	78.03186691	61.13727688	38.91895378	1
				50.94773073	101.8954615	509.4773073	0.028621072	0.057242143	61.13727688
				0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.286210717
				0.274774422	2	3	1	1	0.169582065
									0.125908042
									0.166339473
151	C02	Sc07	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
				0.027387593	0.67046751	56.23169492	0.012963116	36.78293892	34.9928391
				0.172396809	34.54303182	23.3785419	19.448756		0
				0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276
				0.222682445	0.189169138	0.193388639	1	3	2
									1
152	C03	Sc07	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
				0.968261576	0.313424178	0.692322616	57.66539453	0.274831239	38.68279349
				55.36183542	0.421304567	46.51932062	30.78396063	18.98260104	1
									103.5508152

	86.29234598	172.584692	862.9234598	0.048476731	0.096953462	0.484767308	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.230849198	0.247445312
	0.41938841	3	2	1	3		
153	C04 Sc07	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	57.78591144	0.217661196	3.83597854	3.698785078
	85.97992038	0.01822255	121.4049525	84.73175479	53.9499329		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
154	C05 Sc07	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	58.25443748	0.210183901	25.57658235	25.26080431
	50.3295197	0.124450664	81.65831195	51.08430956	32.67785513		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
155	C06 Sc07	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	54.32242722	0.165167411	16.08025417	7.109863301
	57.96001621	0.035027674	90.98919849	57.95453783	38.24217305		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
156	C07 Sc07	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	54.79235021	0.102324317	48.2051179	36.53268887
	2.665127499	0.179983081	11.95556681	9.434151883	6.58723231		
	0	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219
	0.339465132	0.168102684	0.166496609	0.169732566	2	3	1
157	C08 Sc07	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	56.09806673	0.309635483	11.98573101	78.84076537
	58.18750434	0.388419366	105.8292019	72.76685455	44.11233572		
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1
158	C09 Sc07	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	57.49734126	0.149827337	5.541612561	37.21620286
	111.3518603	0.183350502	119.9626468	77.79325612	51.9557287	1	213.6093205
	178.0077671	356.0155341	1780.077671	0.1	0.2	1	0.178780994
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4		
159	C10 Sc07	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	54.36292347	0.133413638	65.61023925	69.4442434
	100.7044175	0.342126169	0	-11.24731578			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
160	C11 Sc07	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	54.27533262	0.310566916	39.57827842	9.30900598
	86.56844337	0.045862038	39.91557934	24.25453437	14.6970542	1	115.021766
	95.85147165	191.7029433	958.5147165	0.053846792	0.107693584	0.538467918	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.270118312	0.271680151
	0.477989469	3	2	1	3		
161	C12 Sc07	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	56.34363925	0.264571047	6.070591495	102.6475506

	13.89093305	0.505706614	121.8708748	81.09291665	50.27304776	1	81.09291665	
	67.57743054	135.1548611	675.7743054	0.037963192	0.075926384	0.379631921	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.225396435	0.244903136	
	0.376408368	3	2	1	3	2		
162	C13 Sc07	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	54.86872988	0.067289973	50.54486886	16.75770835	
	105.7477489	0.082559047	9.031894986	5.925473545	4.32386102			
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	
	0.373298543	0.193600456	0.194835395	0.186649271	2	1	3	3
163	C14 Sc07	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	57.62301365	0.256789061	11.62151545	22.00870416	
	101.4483754	0.108428766	115.2279365	73.89455655	46.0014982	1	73.89455655	
	61.57879712	123.1575942	615.7879712	0.03459332	0.069186641	0.345933204	0.254748757	
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236845571	0.268414458	
	0.358426852	3	2	1	3	4		
164	C15 Sc07	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	54.79343134	0.092219933	17.95680735	59.18869803	
	20.48338339	0.29160088	84.52140528	52.15932574	36.83662399			
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982	
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3	3
165	C16 Sc07	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	54.93067237	0.392667574	20.9375858	102.2141214	
	75.14665628	0.503571269	80.70620343	58.09168666	33.99308657			
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715	
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
166	C17 Sc07	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	58.78345575	0.426987646	48.74907317	89.95873932	
	3.56627786	0.443193522	25.12684124	17.37079081	10.03438258			
	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	
	0.424898731	0.195078226	0.211045796	0.212449365	3	2	1	4
167	C18 Sc07	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	58.50011452	0.247118419	32.71947943	114.7069548	
	14.82699307	0.56511885	60.14034286	41.19347597	25.78063509	1	47.11894951	
	39.26579126	78.53158252	392.6579126	0.022058471	0.044116942	0.220584708	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.194192795	0.235842748	
	0.273802164	3	2	1	4	3		
168	C19 Sc07	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	56.51268711	0.423280743	15.52703729	90.00070565	
	38.18171179	0.443400275	94.78914057	70.85536745	40.98564982			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
169	C20 Sc07	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	56.03643596	0.039822739	31.51644382	46.12331125	
	19.64406076	0.227232539	49.45715216	32.00803948	24.51999214			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4

170	C21	Sc07	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	57.00533717	0.252623045	9.029325069	48.98585736	89.96292202	0
	0.241335248		104.9023396	76.89174449	47.9760121				0
	0	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
171	C22	Sc07	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	56.33098534	0.032643252	64.00112666	84.62593646	
	96.89993412		0.41692077	0	-7.67014132	1	152.354222	126.9618516	
	253.9237033		1269.618516	0.071323771	0.142647541	0.713237707	0.273632139	0.256849416	
	0.255171744		0.482159781	0.476288524	0.435601111	0.276741776	0.309468033	0.574419409	
	3	2	1	5	2				
172	C23	Sc07	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	58.97545605	0.214061164	39.76903222	32.83555671	
	41.4875192		0.161768675	41.4964786	30.09784241	19.20642383	1	212.7427226	
	177.2856022		354.5712044	1772.856022	0.099594307	0.199188614	0.995943071	0.126338191	
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.208990939	0.289122701	
	0.653886601		3	2	1	5	3		
173	C24	Sc07	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	54.05781899	0.048265458	33.25451259	101.091395	
	38.46617124		0.49804001	40.31694461	27.62214754	20.8033064			
	0	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
									4
174	C25	Sc07	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	58.85796783	0.063579986	22.39183764	108.0009528	
	14.23314753		0.532080852	81.75479952	49.69466047	36.46613019	1	49.69466047	
	41.41221705		82.82443411	414.1221705	0.023264275	0.046528551	0.232642753	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.249896873	0.230678456	
	0.346625808		2	3	1	5	5		
175	C01	Sc08	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595		0.186260211	0.345560727	44.010279	0.152598216	16.09475155	6.870223806	
	22.2596509		0.033847058	53.46814953	41.89182178	27.91552745	1	41.89182178	
	34.90985148		69.81970297	349.0985148	0.027472193	0.054944385	0.274721927	0.125908042	
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169007626	0.165190594	
	0.269030027		2	3	1	1			
176	C02	Sc08	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593		0.67046751	44.92377119	0.009074181	36.78293892	34.9928391	3.448308502	
	0.172396809		14.16000836	9.583419037	8.14083227			0	
	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445		0.189169138	0.193388639	1	3	2	1	2
177	C03	Sc08	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576		0.313424178	0.692322616	45.9990459	0.192381867	38.68279349	85.51575292	
	55.36183542		0.421304567	17.08394204	11.30522527	7.31625241	1	62.85001433	
	52.37501194		104.7500239	523.7501194	0.041216343	0.082432687	0.412163433	0.25038454	
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227219004	0.240184924	
	0.383086473		3	2	1	1			
178	C04	Sc08	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503		0.098346834	0.421107625	46.08943358	0.152362837	3.83597854	3.698785078	

	85.97992038	0.01822255	90.83506783	63.39621686	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	4
179	C05	Sc08	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.147128731	25.57658235	25.26080431	
	50.3295197	0.124450664	49.82662114	31.17084444	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
180	C06	Sc08	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.115617187	16.08025417	7.109863301	
	57.96001621	0.035027674	62.49130739	39.80312937	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
181	C07	Sc08	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	43.84426266	0.071627022	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
182	C08	Sc08	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	44.82355005	0.216744838	11.98573101	78.84076537	
	58.18750434	0.388419366	74.9646789	51.54478905	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
183	C09	Sc08	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	45.87300595	0.104879136	5.541612561	37.21620286	
	111.3518603	0.183350502	89.31827978	57.92102791	40.33139339	1	152.4880892	
	127.0734077	254.1468153	1270.734077	0.1	0.2	1	0.232017403	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4			
184	C10	Sc08	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	43.5221926	0.093389546	65.61023925	69.4442434	
	100.7044175	0.342126169	0	-22.08804665			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
185	C11	Sc08	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	43.45649947	0.217396841	39.57827842	9.30900598	
	86.56844337	0.045862038	10.02228614	6.090000138	3.87822105	1	55.47654854	
	46.23045712	92.46091423	462.3045712	0.036380906	0.072761812	0.363809061	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261385369	0.254214266	
	0.390660041	2	3	1	3	1		
186	C12	Sc08	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	45.00772944	0.185199733	6.070591495	102.6475506	
	13.89093305	0.505706614	89.97787433	59.87130458	38.93713794	1	59.87130458	
	49.89275382	99.78550764	498.9275382	0.039262938	0.078525877	0.392629384	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226046308	0.246202882	
	0.3829071	3	1	3	2			

187	C13	Sc08	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.047102981	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
188	C14	Sc08	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.179752342	11.62151545	22.00870416
	101.4483754		0.108428766	82.03715428	52.60963029	34.34574479	1	52.60963029
	43.84135857		87.68271714	438.4135857	0.034500813	0.069001626	0.345008129	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236799318	0.268321951
	0.357964314		3	2	1	3	4	
189	C15	Sc08	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.064553953	17.95680735	59.18869803
	20.48338339		0.29160088	57.25400315	35.33223555	25.88826616		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
190	C16	Sc08	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.274867302	20.9375858	102.2141214
	75.14665628		0.503571269	51.84349392	37.31653673	23.01041848		
	0		0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
191	C17	Sc08	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.298891352	48.74907317	89.95873932
	3.56627786		0.443193522	0	-1.91148136			0
	0		0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
192	C18	Sc08	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.172982893	32.71947943	114.7069548
	14.82699307		0.56511885	30.94565418	21.19640496	13.90560646	1	21.19640496
	17.6636708		35.32734161	176.636708	0.013900368	0.027800735	0.139003676	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190113744	0.227684645
	0.233011648		3	2	1	4	3	
193	C19	Sc08	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.29629652	15.52703729	90.00070565
	38.18171179		0.443400275	64.92366836	48.53077421	29.60747804		
	0		0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
194	C20	Sc08	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.027875917	31.51644382	46.12331125
	19.64406076		0.227232539	25.97767972	16.81242372	13.26088315		
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
195	C21	Sc08	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.176836132	9.029325069	48.98585736	89.96292202
	0.241335248		76.06476153	55.75425897	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5

196	C22	Sc08	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.022850277	64.00112666	84.62593646
	96.89993412		0.41692077	0	-19.00288766	1	93.0707957	77.55899642
	155.1179928		775.5899642	0.061034797	0.122069594	0.61034797	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271597289	0.299179059	0.522974541
	3	2	1	5	2			
197	C23	Sc08	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.149842815	39.76903222	32.83555671
	41.4875192		0.161768675	14.88947213	10.79949433	7.21255982	1	124.3995269
	103.6662724		207.3325448	1036.662724	0.081579832	0.163159664	0.815798319	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199983701	0.271108226
	0.563814225		3	2	1	5	3	
198	C24	Sc08	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.03378582	33.25451259	101.091395
	38.46617124		0.49804001	18.86458484	12.92459909	10.03885165		
	0		0	0	0.194999729	0.172101157	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
								5
199	C25	Sc08	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.04450599	22.39183764	108.0009528
	14.23314753		0.532080852	53.13248457	32.29658437	24.50163823	1	32.29658437
	26.91382031		53.82764061	269.1382031	0.021179742	0.042359485	0.211797423	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248854607	0.228593923
	0.336203143		2	3	1	5	5	
200	C01	Sc09	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.174397961	16.09475155	6.870223806
	22.2596509		0.033847058	54.36661906	42.5957647	27.91552745	1	42.5957647
	35.49647058		70.99294117	354.9647058	0.027488581	0.054977163	0.274885813	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.16901582	0.165206982
	0.26911197		2	3	1	1	1	
201	C02	Sc09	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.010370493	36.78293892	34.9928391	0.878117436
	0.172396809		14.2673654	9.656077715	8.14083227			3.448308502
	0		0	0	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
202	C03	Sc09	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.219864991	38.68279349	85.51575292
	55.36183542		0.421304567	17.38755155	11.50613756	7.31625241	1	63.99313913
	53.32761594		106.6552319	533.2761594	0.041297078	0.082594156	0.412970778	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227259371	0.240265659
	0.383490145		3	2	1	1	3	
203	C04	Sc09	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.174128957	3.83597854	3.698785078
	85.97992038		0.018222255	92.36086687	64.46111271	42.25345504		
	0		0	0	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
								4
204	C05	Sc09	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.168147121	25.57658235	25.26080431

	50.3295197	0.124450664	50.65642155	31.68995608	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	5
205	C06 Sc09	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.132133928	16.08025417	7.109863301	
	57.96001621	0.035027674	63.47118965	40.42725426	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	1
206	C07 Sc09	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.081859454	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
207	C08 Sc09	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.247708387	11.98573101	78.84076537	
	58.18750434	0.388419366	76.33499509	52.48700157	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
208	C09 Sc09	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.119861869	5.541612561	37.21620286	
	111.3518603	0.183350502	90.68445466	58.80696361	40.33139339	1	154.9580324	
	129.1316937	258.2633873	1291.316937	0.1	0.2	0.178780994	0.232017403	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4			
209	C10 Sc09	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.10673091	65.61023925	69.4442434	
	100.7044175	0.342126169	0	-22.08804665			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
210	C11 Sc09	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.248453533	39.57827842	9.30900598	
	86.56844337	0.045862038	10.20561746	6.201400644	3.87822105	1	56.28473262	
	46.90394385	93.80788769	469.0394385	0.036322565	0.072645131	0.363225654	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261356199	0.254155925	
	0.390368337	2	3	1	3			
211	C12 Sc09	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.211656838	6.070591495	102.6475506	
	13.89093305	0.505706614	91.56246866	60.92569413	38.93713794	1	60.92569413	
	50.77141177	101.5428235	507.7141177	0.039317545	0.07863509	0.39317545	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226073611	0.246257489	
	0.383180133	3	2	1	3			
212	C13 Sc09	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.053831978	50.54486886	16.75770835	
	105.7477489	0.082559047	0	-6.64332145			0	
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543	
	0.193600456	0.194835395	0.186649271	2	1	3	3	

213	C14	Sc09	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.205431249	11.62151545	22.00870416
	101.4483754		0.108428766	83.47159941	53.52952601	34.34574479	1	53.52952601
	44.60793834		89.21587669	446.0793834	0.034544531	0.069089063	0.345445313	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236821177	0.268365669
	0.358182907		3	2	1	3	4	
214	C15	Sc09	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.073775946	17.95680735	59.18869803
	20.48338339		0.29160088	58.02479073	35.8078992	25.88826616		
	0		0	0	0.251517278	0.292575574	0.225051384	0.421654228
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
								3
								5
215	C16	Sc09	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.314134059	20.9375858	102.2141214
	75.14665628		0.503571269	52.84455401	38.03709186	23.01041848		
	0		0	0	0.198021052	0.185581091	0.191572754	0.409469615
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
								4
								1
216	C17	Sc09	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.341590117	48.74907317	89.95873932
	3.56627786		0.443193522	0	-1.91148136			0
	0		0	0	0.154114011	0.183917483	0.218846089	0.390156452
	0.195078226		0.211045796	0.212449365	3	2	1	4
								2
								2
217	C18	Sc09	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.197694735	32.71947943	114.7069548
	14.82699307		0.56511885	31.4817692	21.56362004	13.90560646	1	21.56362004
	17.96968337		35.93936674	179.6968337	0.013915781	0.027831561	0.139157807	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.19012145	0.227700058
	0.233088713		3	2	1	4	3	
								3
218	C19	Sc09	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.338624594	15.52703729	90.00070565
	38.18171179		0.443400275	66.19872074	49.48388238	29.60747804		
	0		0	0	0.19335296	0.154863434	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
								4
								4
219	C20	Sc09	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.031858191	31.51644382	46.12331125
	19.64406076		0.227232539	26.25407603	16.99130389	13.26088315		
	0		0	0	0.266503103	0.213730709	0.290225506	0.462800059
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
								4
								5
220	C21	Sc09	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.202098436	9.029325069	48.98585736	89.96292202
	0.241335248		77.38955584	56.72531211	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
								1
221	C22	Sc09	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.026114602	64.00112666	84.62593646
	96.89993412		0.41692077	0	-19.00288766	1	94.76240397	78.96866997
	157.9373399		789.6866997	0.061153593	0.122307185	0.611535927	0.273632139	0.256849416

	0.255171744	0.482159781	0.476288524	0.435601111	0.271656687	0.299297855	0.523568519
	3	2	1	5	2		
222	C23 Sc09	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401	0.752755554	0.066536481	46.98159204	0.171248931	39.76903222	32.83555671
	41.4875192	0.161768675	15.13855549	10.98015718	7.21255982	1	126.333188
	105.2776566	210.5553133	1052.776566	0.081527357	0.163054714	0.815273568	0.126338191
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199957463	0.271055751
	0.56355185	3	2	1	5	3	
223	C24 Sc09	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.038612366	33.25451259	101.091395
	38.46617124	0.49804001	19.07673039	13.06994531	10.03885165		
	0	0	0	0.195074589	0.172101157	0.408593283	0.408513079
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
						5	4
224	C25 Sc09	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086	0.616778357	0.949016321	46.89347587	0.050863989	22.39183764	108.0009528
	14.23314753	0.532080852	53.77837981	32.68919184	24.50163823	1	32.68919184
	27.2409932	54.48198639	272.409932	0.021095513	0.042191026	0.21095513	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248812492	0.228509694
	0.335781997	2	3	1	5	5	
225	C01 Sc10	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595	0.186260211	0.345560727	44.010279	0.196197706	16.09475155	6.870223806
	22.2596509	0.033847058	55.19661429	43.24605862	27.91552745	1	43.24605862
	36.03838218	72.07676437	360.3838218	0.027503263	0.055006527	0.275032633	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169023161	0.165221664
	0.26918538	2	3	1	1		
226	C02 Sc10	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593	0.67046751	44.92377119	0.011666804	36.78293892	34.9928391	3.448308502
	0.172396809	14.36654045	9.723198867	8.14083227			0
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445	0.189169138	0.193388639	1	3	2	1
227	C03 Sc10	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576	0.313424178	0.692322616	45.9990459	0.247348115	38.68279349	85.51575292
	55.36183542	0.421304567	17.66802232	11.69173789	7.31625241	1	65.04914391
	54.20761993	108.4152399	542.0761993	0.041369405	0.082738811	0.413694054	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227295535	0.240337987
	0.383851784	3	2	1	1	3	
228	C04 Sc10	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.195895077	3.83597854	3.698785078
	85.97992038	0.01822255	93.7703815	65.44485057	42.25345504		
	0	0	0	0.214732899	0.18442312	0.126095549	0.407884499
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
						1	4
229	C05 Sc10	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.189165511	25.57658235	25.26080431
	50.3295197	0.124450664	51.42298108	32.16950512	20.86424576		
	0	0	0	0.286047241	0.291180307	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
						1	5

230	C06	Sc10	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.148650669	16.08025417	7.109863301
	57.96001621		0.035027674	64.37639299	41.00381325	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
						2	2	1
231	C07	Sc10	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.092091885	48.2051179	36.53268887
	2.665127499		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
						2	2	
232	C08	Sc10	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.278671935	11.98573101	78.84076537
	58.18750434		0.388419366	77.6008765	53.35740602	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
						2	2	3
233	C09	Sc10	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.134844603	5.541612561	37.21620286
	111.3518603		0.183350502	91.9465105	59.62538031	40.33139339	1	157.239736
	131.0331133		262.0662267	1310.331133	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3		2	4				0.716039279
234	C10	Sc10	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.120072274	65.61023925	69.4442434
	100.7044175		0.342126169	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
						3	2	5
235	C11	Sc10	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.279510225	39.57827842	9.30900598
	86.56844337		0.045862038	10.3749767	6.304311078	3.87822105	1	57.0313232
	47.52610267		95.05220533	475.2610267	0.0362703	0.072540599	0.362702995	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261330066	0.254103659
	0.390107008		2	3	1	3	1	
236	C12	Sc10	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.238113942	6.070591495	102.6475506
	13.89093305		0.505706614	93.02629761	61.89972635	38.93713794	1	61.89972635
	51.58310529		103.1662106	515.8310529	0.039366465	0.078732931	0.393664655	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226098071	0.246306409
	0.383424735		3	2	1	3	2	
237	C13	Sc10	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.060560975	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
238	C14	Sc10	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.231110155	11.62151545	22.00870416
	101.4483754		0.108428766	84.79672234	54.37931448	34.34574479	1	54.37931448
	45.3160954		90.6321908	453.160954	0.034583697	0.069167395	0.345836974	0.254748757

	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.23684076	0.268404836
	0.358378737	3	2	1	3	4	
239	C15 Sc10	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536	0.711524759	0.124270962	43.84507351	0.08299794	17.95680735	59.18869803
	20.48338339	0.29160088	58.73683501	36.24731156	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
240	C16 Sc10	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064	0.552821979	0.842030892	43.94800428	0.353400817	20.9375858	102.2141214
	75.14665628	0.503571269	53.76932119	38.70273195	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
241	C17 Sc10	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289	0.800632673	0.232974274	46.83759181	0.384288882	48.74907317	89.95873932
	3.56627786	0.443193522	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
242	C18 Sc10	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226	0.05991769	0.121343456	46.62508589	0.222406577	32.71947943	114.7069548
	14.82699307	0.56511885	31.97702573	21.90284888	13.90560646	1	21.90284888
	18.25237406	36.50474813	182.5237406	0.013929589	0.027859178	0.139295889	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190128354	0.227713866
	0.233157754	3	2	1	4	3	
243	C19 Sc10	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598	0.07197428	0.96727633	45.13451533	0.380952668	15.52703729	90.00070565
	38.18171179	0.443400275	67.37659864	50.36435213	29.60747804		
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
244	C20 Sc10	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927	0.970019989	0.846828801	44.77732697	0.035840465	31.51644382	46.12331125
	19.64406076	0.227232539	26.50940758	17.15655122	13.26088315		
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1
245	C21 Sc10	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144	0.486345111	45.50400288	0.227360741	9.029325069	48.98585736	0.018576202
	0.241335248	78.61338479	57.62235924	36.47467781			89.96292202
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0
	0.184443254	0.17732464	0.165746932	1	2	3	5
246	C22 Sc10	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173	0.550948219	0.745334431	44.998239	0.029378927	64.00112666	84.62593646
	96.89993412	0.41692077	0	-19.00288766	1	96.3250912	80.27090933
	160.5418187	802.7090933	0.061260018	0.122520037	0.612600184	0.273632139	0.256849416
	0.255171744	0.482159781	0.476288524	0.435601111	0.2717099	0.299404281	0.524100648
	2	1	5	2			3
247	C23 Sc10	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401	0.752755554	0.066536481	46.98159204	0.192655047	39.76903222	32.83555671
	41.4875192	0.161768675	15.36865568	11.14705132	7.21255982	1	128.1194806

	106.7662339	213.5324677	1067.662339	0.081480346	0.162960692	0.814803458	0.126338191
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199933958	0.27100874
	0.563316795	3	2	1	5	3	
248	C24 Sc10	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.043438912	33.25451259	101.091395
	38.46617124	0.49804001	19.27270787	13.20421439	10.03885165		
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
249	C25 Sc10	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086	0.616778357	0.949016321	46.89347587	0.057221987	22.39183764	108.0009528
	14.23314753	0.532080852	54.3750499	33.05187779	24.50163823	1	33.05187779
	27.54323149	55.08646299	275.4323149	0.021020054	0.042040108	0.210200542	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248774763	0.228434235
	0.335404703	2	3	1	5	5	
250	C01 Sc11	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	22.2596509	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906	2	3	1	1		
251	C02 Sc11	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	0.878117436
	0.172396809	14.4589725	9.78575639	8.14083227			3.448308502
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445	0.189169138	0.193388639	1	3	2	0.386777277
252	C03 Sc11	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	55.36183542	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511	3	2	1	3		
253	C04 Sc11	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	85.97992038	0.01822255	95.08406081	66.3617024	42.25345504		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
254	C05 Sc11	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	50.3295197	0.124450664	52.13742096	32.61644881	20.86424576		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
255	C06 Sc11	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301
	57.96001621	0.035027674	65.22005008	41.54117107	27.41156624		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
						2	1

256	C07	Sc11	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887
	2.665127499		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
257	C08	Sc11	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
258	C09	Sc11	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4			0.716039279
259	C10	Sc11	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
260	C11	Sc11	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3	5	
261	C12	Sc11	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3	2	
262	C13	Sc11	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
263	C14	Sc11	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
264	C15	Sc11	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	59.40046614	36.65684749	25.88826616		

		0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
		0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
265	C16	Sc11	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
		0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
		75.14665628	0.503571269	54.63121188	39.32311405	23.01041848		
		0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
		0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
266	C17	Sc11	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
		0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
		3.56627786	0.443193522	0	-1.91148136			0
		0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
		0.195078226	0.211045796	0.212449365	3	2	1	4
267	C18	Sc11	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
		0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
		14.82699307	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
		18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
		0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
		0.233220321	3	2	1	4	3	
268	C19	Sc11	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
		0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565
		38.18171179	0.443400275	68.47439068	51.1849573	29.60747804		
		0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
		0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
269	C20	Sc11	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
		0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125
		19.64406076	0.227232539	26.74737871	17.31056311	13.26088315		
		0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
		0.473734591	0.23140003	0.208910304	0.236867296	2	3	1
270	C21	Sc11	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
		0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	0.018576202
		0.241335248	79.75400352	58.45841461	36.47467781			89.96292202
		0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0
		0.184443254	0.17732464	0.165746932	1	2	3	5
271	C22	Sc11	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
		0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646
		96.89993412	0.41692077	0	-19.00288766	1	97.78152866	81.48460722
		162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
		0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
		3	2	1	5	2		
272	C23	Sc11	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
		0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671
		41.4875192	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202
		108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
		0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
		0.563103781	3	2	1	5	3	
273	C24	Sc11	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
		0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395

	38.46617124	0.49804001	19.45536051	13.32935429	10.03885165				
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079		
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5	4
274	C25 Sc11	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573		
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528		
	14.23314753	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418		
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204		
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852		
	0.335062789	2	3	1	5	5			
275	C01 Sc12	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891		
	0.092338595	0.186260211	0.345560727	44.010279	0.239797196	16.09475155	6.870223806		
	22.2596509	0.033847058	56.69626181	44.42101917	27.91552745	1	44.42101917		
	37.01751597	74.03503195	370.1751597	0.027528738	0.055057476	0.275287382	0.125908042		
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169035898	0.165247139		
	0.269312754	2	3	1	1	1			
276	C02 Sc12	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436	
	0.027387593	0.67046751	44.92377119	0.014259428	36.78293892	34.9928391	3.448308502		
	0.172396809	14.54573152	9.844474439	8.14083227			0		
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277		
	0.222682445	0.189169138	0.193388639	1	3	2	1	2	
277	C03 Sc12	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569		
	0.968261576	0.313424178	0.692322616	45.9990459	0.302314363	38.68279349	85.51575292		
	55.36183542	0.421304567	18.174781	12.02708327	7.31625241	1	66.95714877	55.79762397	
	111.5952479	557.9762397	0.041494902	0.082989803	0.414949015	0.25038454	0.237553697		
	0.192031501	0.413221665	0.397937162	0.354009513	0.227358283	0.240463483	0.384479264		
	3	2	1	3					
278	C04 Sc12	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042		
	0.878142503	0.098346834	0.421107625	46.08943358	0.239427316	3.83597854	3.698785078		
	85.97992038	0.01822255	96.31711303	67.22228244	42.25345504				
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941		
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1	4
279	C05 Sc12	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928		
	0.834625672	0.018288277	0.750144315	46.44082811	0.231202291	25.57658235	25.26080431		
	50.3295197	0.124450664	52.80801205	33.03596132	20.86424576				
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602		
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1	5
280	C06 Sc12	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007		
	0.447893526	0.908595503	0.293614148	43.49182041	0.181684152	16.08025417	7.109863301		
	57.96001621	0.035027674	66.01192763	42.04554849	27.41156624				
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035		
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2	1
281	C07 Sc12	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116		
	0.265546659	0.491573159	0.053362545	43.84426266	0.112556749	48.2051179	36.53268887		
	2.665127499	0.179983081	0	-4.36085524			0		
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132		
	0.168102684	0.166496609	0.169732566	2	3	1	2	2	

282	C08	Sc12	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.340599031	11.98573101	78.84076537
	58.18750434		0.388419366	79.88808952	54.93006549	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
283	C09	Sc12	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.164810071	5.541612561	37.21620286
	111.3518603		0.183350502	94.22681143	61.10410755	40.33139339	1	161.3623513
	134.4686261		268.9372522	1344.686261	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
284	C10	Sc12	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.146755001	65.61023925	69.4442434
	100.7044175		0.342126169	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
285	C11	Sc12	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.341623608	39.57827842	9.30900598
	86.56844337		0.045862038	10.68097745	6.49025115	3.87822105	1	58.38027408
	48.6502284		97.3004568	486.502284	0.036179613	0.072359226	0.361796129	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261284722	0.254012973
	0.389653575		2	3	1	3	1	
286	C12	Sc12	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.291028152	6.070591495	102.6475506
	13.89093305		0.505706614	95.67116522	63.65962205	38.93713794	1	63.65962205
	53.04968504		106.0993701	530.4968504	0.039451348	0.078902695	0.394513476	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226140512	0.246391291
	0.383849146		3	2	1	3	2	
287	C13	Sc12	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.07401897	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
288	C14	Sc12	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.282467967	11.62151545	22.00870416
	101.4483754		0.108428766	87.1909738	55.91472469	34.34574479	1	55.91472469
	46.59560391		93.19120781	465.9560391	0.034651655	0.069303309	0.346516546	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236874739	0.268472793
	0.358718523		3	2	1	3	4	
289	C15	Sc12	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.101441926	17.95680735	59.18869803
	20.48338339		0.29160088	60.02336688	37.04124812	25.88826616		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
290	C16	Sc12	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.431934331	20.9375858	102.2141214
	75.14665628		0.503571269	55.44020398	39.90542017	23.01041848		

		0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
		0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
291	C17	Sc12	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
		0.018647289	0.800632673	0.232974274	46.83759181	0.469686411	48.74907317	89.95873932
		3.56627786	0.443193522	0	-1.91148136			0
		0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
		0.195078226	0.211045796	0.212449365	3	2	1	4
292	C18	Sc12	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
		0.136455226	0.05991769	0.121343456	46.62508589	0.271830261	32.71947943	114.7069548
		14.82699307	0.56511885	32.87186247	22.51577248	13.90560646	1	22.51577248
		18.76314373	37.52628747	187.6314373	0.013953548	0.027907095	0.139535476	0.168545737
		0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190140334	0.227737825
		0.233277548	3	2	1	4	3	
293	C19	Sc12	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
		0.01255598	0.07197428	0.96727633	45.13451533	0.465608817	15.52703729	90.00070565
		38.18171179	0.443400275	69.50480564	51.95519776	29.60747804		
		0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
		0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
294	C20	Sc12	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
		0.581358927	0.970019989	0.846828801	44.77732697	0.043805012	31.51644382	46.12331125
		19.64406076	0.227232539	26.9707443	17.45512248	13.26088315		
		0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
		0.473734591	0.23140003	0.208910304	0.236867296	2	3	1
295	C21	Sc12	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
		0.070022144	0.486345111	45.50400288	0.27788535	9.029325069	48.98585736	89.96292202
		0.241335248	80.82461675	59.24315706	36.47467781			0
		0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
		0.184443254	0.17732464	0.165746932	1	2	3	5
296	C22	Sc12	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
		0.380141173	0.550948219	0.745334431	44.998239	0.035907577	64.00112666	84.62593646
		96.89993412	0.41692077	0	-19.00288766	1	99.14857722	82.62381435
		165.2476287	826.2381435	0.061444678	0.122889356	0.61444678	0.273632139	0.256849416
		0.255171744	0.482159781	0.476288524	0.435601111	0.271802229	0.29958894	0.525023946
		3	2	1	5	2		
297	C23	Sc12	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
		0.21017401	0.752755554	0.066536481	46.98159204	0.23546728	39.76903222	32.83555671
		41.4875192	0.161768675	15.78440408	11.44859811	7.21255982	1	131.3469802
		109.4558168	218.9116336	1094.558168	0.081398777	0.162797554	0.813987768	0.126338191
		0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199893173	0.270927171
		0.56290895	3	2	1	5	3	
298	C24	Sc12	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
		0.92480797	0.26329677	0.065961091	43.29336424	0.053092004	33.25451259	101.091395
		38.46617124	0.49804001	19.62680284	13.44681372	10.03885165		
		0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079
		0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
299	C25	Sc12	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
		0.234362086	0.616778357	0.949016321	46.89347587	0.069937984	22.39183764	108.0009528

	14.23314753	0.532080852	55.45312222	33.70718412	24.50163823	1	33.70718412	
	28.0893201	56.1786402	280.893201	0.020889126	0.041778251	0.208891255	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248709298	0.228303306	
	0.334750059	2	3	1	5	5		
300	C01 Sc13	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.261596941	16.09475155	6.870223806	
	22.2596509	0.033847058	57.38173406	44.95808061	27.91552745	1	44.95808061	
	37.46506718	74.93013435	374.6506718	0.027539954	0.055079908	0.275399539	0.125908042	
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169041506	0.165258355	
	0.269368833	2	3	1	1	1		
301	C02 Sc13	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.015555739	36.78293892	34.9928391	3.448308502	
	0.172396809	14.62763771	9.899908116	8.14083227			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	2
302	C03 Sc13	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.329797487	38.68279349	85.51575292	
	55.36183542	0.421304567	18.40641478	12.18036593	7.31625241	1	67.82927666	
	56.52439722	113.0487944	565.2439722	0.041550154	0.083100307	0.415501536	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227385909	0.240518735	
	0.384755525	3	2	1	3			
303	C04 Sc13	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.261193436	3.83597854	3.698785078	
	85.97992038	0.01822255	97.48119582	68.03472687	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
304	C05 Sc13	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.252220681	25.57658235	25.26080431	
	50.3295197	0.124450664	53.44109435	33.43200884	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
305	C06 Sc13	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.198200893	16.08025417	7.109863301	
	57.96001621	0.035027674	66.75951236	42.5217141	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
306	C07 Sc13	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.12278918	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
307	C08 Sc13	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.37156258	11.98573101	78.84076537	
	58.18750434	0.388419366	80.93354926	55.64891073	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2

308	C09	Sc13	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.179792804	5.541612561	37.21620286
	111.3518603		0.183350502	95.26911163	61.78001734	40.33139339	1	163.246753
	136.0389609		272.0779217	1360.389609	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
309	C10	Sc13	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.160096365	65.61023925	69.4442434
	100.7044175		0.342126169	0	-22.08804665			0
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
							5	
310	C11	Sc13	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.3726803	39.57827842	9.30900598
	86.56844337		0.045862038	10.82084701	6.575242297	3.87822105	1	58.99686452
	49.16405376		98.32810753	491.6405376	0.036139686	0.072279373	0.361396863	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261264759	0.253973046
	0.389453942		2	3	1			
311	C12	Sc13	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.317485257	6.070591495	102.6475506
	13.89093305		0.505706614	96.88010489	64.46405087	38.93713794	1	64.46405087
	53.72004239		107.4400848	537.2004239	0.039488719	0.078977437	0.394887186	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226159198	0.246428662
	0.384036001		3	2	1	3	2	
312	C13	Sc13	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.080747967	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
313	C14	Sc13	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.308146873	11.62151545	22.00870416
	101.4483754		0.108428766	88.2853596	56.61654367	34.34574479	1	56.61654367
	47.18045306		94.36090612	471.8045306	0.034681574	0.069363148	0.346815741	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236889698	0.268502712
	0.358868121		3	2	1	3	4	
314	C15	Sc13	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.110663919	17.95680735	59.18869803
	20.48338339		0.29160088	60.61142633	37.40414773	25.88826616		
	0	0	0	0	0.251517278	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
							3	5
315	C16	Sc13	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.471201089	20.9375858	102.2141214
	75.14665628		0.503571269	56.203946	40.45515563	23.01041848		
	0	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
							4	1
316	C17	Sc13	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.512385176	48.74907317	89.95873932
	3.56627786		0.443193522	0	0	-1.91148136		0

	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
317	C18	Sc13	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.296542102	32.71947943	114.7069548
	14.82699307		0.56511885	33.28088241	22.79593305	13.90560646	1	22.79593305
	18.99661088		37.99322176	189.9661088	0.013964096	0.027928192	0.139640958	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190145608	0.227748373
	0.233330289		3	2	1	4	3	
318	C19	Sc13	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.507936891	15.52703729	90.00070565
	38.18171179		0.443400275	70.47758546	52.68235565	29.60747804		
	0		0	0	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
319	C20	Sc13	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.047787286	31.51644382	46.12331125
	19.64406076		0.227232539	27.18161622	17.5915961	13.26088315		
	0		0	0	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
320	C21	Sc13	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.303147654	9.029325069	48.98585736	89.96292202
	0.241335248		81.83534635	59.98400576	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
321	C22	Sc13	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.039171903	64.00112666	84.62593646
	96.89993412		0.41692077	0	-19.00288766	1	100.4391614	83.69930116
	167.3986023		836.9930116	0.061525978	0.123051956	0.61525978	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271842879	0.29967024	0.525430446
	3	2	1	5	2			
322	C23	Sc13	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.256873397	39.76903222	32.83555671
	41.4875192		0.161768675	15.97443806	11.5864318	7.21255982	1	132.8222344
	110.6851954		221.3703907	1106.851954	0.081362864	0.162725729	0.813628645	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199875217	0.270891258
	0.562729388		3	2	1	5	3	
323	C24	Sc13	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.057918549	33.25451259	101.091395
	38.46617124		0.49804001	19.78865569	13.55770316	10.03885165		
	0		0	0	0.195074589	0.194999729	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
324	C25	Sc13	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.076295983	22.39183764	108.0009528
	14.23314753		0.532080852	55.94589716	34.0067174	24.50163823	1	34.0067174
	28.33893117		56.67786234	283.3893117	0.020831482	0.041662963	0.208314817	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248680476	0.228245662
	0.33446184		2	3	1	5	5	

325	C01	Sc14	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.283396686	16.09475155	6.870223806
	22.2596509		0.033847058	58.03198663	45.46754775	27.91552745	1	45.46754775
	37.88962312		75.77924624	378.8962312	0.027550357	0.055100713	0.275503567	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169046708	0.165268758
	0.269420847		2	3	1	1		
326	C02	Sc14	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.016852051	36.78293892	34.9928391	0.878117436
	0.172396809		14.70533561	9.952493641	8.14083227			3.448308502
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
327	C03	Sc14	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.357280611	38.68279349	85.51575292
	55.36183542		0.421304567	18.62614718	12.3257729	7.31625241	1	68.65659445
	57.21382871		114.4276574	572.1382871	0.041601401	0.083202801	0.416014006	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227411533	0.240569982
	0.38501176		3	2	1	3		
328	C04	Sc14	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.282959555	3.83597854	3.698785078
	85.97992038		0.01822255	98.58546778	68.80542772	42.25345504		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
329	C05	Sc14	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.273239071	25.57658235	25.26080431
	50.3295197		0.124450664	54.04164877	33.80770737	20.86424576		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
330	C06	Sc14	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.214717634	16.08025417	7.109863301
	57.96001621		0.035027674	67.46868606	42.97341425	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
331	C07	Sc14	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.133021612	48.2051179	36.53268887
	2.665127499		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
332	C08	Sc14	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.402526128	11.98573101	78.84076537
	58.18750434		0.388419366	81.92529308	56.33082155	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
333	C09	Sc14	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.194775538	5.541612561	37.21620286
	111.3518603		0.183350502	96.25785834	62.42119881	40.33139339	1	165.0343339
	137.5286116		275.0572232	1375.286116	0.1	0.2	1	0.178780994
								0.232017403

	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	4				
334	C10 Sc14	C10 0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.173437729	65.61023925	69.4442434
	100.7044175	0.342126169	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
335	C11 Sc14	C11 0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.403736991	39.57827842	9.30900598
	86.56844337	0.045862038	10.95353003	6.655866582	3.87822105	1	59.58177447
	49.65147873	99.30295746	496.5147873	0.036102654	0.072205308	0.36102654	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261246243	0.253936014
	0.38926878	2	3	1	3	1	
336	C12 Sc14	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.343942361	6.070591495	102.6475506
	13.89093305	0.505706614	98.02692899	65.22714797	38.93713794	1	65.22714797
	54.35595664	108.7119133	543.5595664	0.039523381	0.079046761	0.395233806	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226176529	0.246463324
	0.384209311	3	2	1	3	2	
337	C13 Sc14	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.087476965	50.54486886	16.75770835
	105.7477489	0.082559047	0	-6.64332145			0
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2	1	3	3
338	C14 Sc14	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.333825779	11.62151545	22.00870416
	101.4483754	0.108428766	89.32351568	57.28230308	34.34574479	1	57.28230308
	47.73525257	95.47050514	477.3525257	0.034709325	0.06941865	0.347093249	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236903574	0.268530463
	0.359006874	3	2	1	3	4	
339	C15 Sc14	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.119885913	17.95680735	59.18869803
	20.48338339	0.29160088	61.16927125	37.74840153	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
340	C16 Sc14	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.510467846	20.9375858	102.2141214
	75.14665628	0.503571269	56.92844681	40.97664558	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
341	C17 Sc14	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.55508394	48.74907317	89.95873932
	3.56627786	0.443193522	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
342	C18 Sc14	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.321253945	32.71947943	114.7069548

	14.82699307	0.56511885	33.66888687	23.06169895	13.90560646	1	23.06169895	
	19.21808246	38.43616492	192.1808246	0.013973879	0.027947759		0.139738795	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619		0.1901505	0.227758156
	0.233379207	3	2	1	4	3		
343	C19 Sc14	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.550264966	15.52703729	90.00070565	
	38.18171179	0.443400275	71.40038372	53.37215206	29.60747804			
	0	0	0.19335296	0.154863434	0.16721044		0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
344	C20 Sc14	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.051769561	31.51644382	46.12331125	
	19.64406076	0.227232539	27.38165357	17.72105772	13.26088315			
	0	0	0.266503103	0.213730709	0.290225506		0.462800059	0.417820608
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
345	C21 Sc14	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.328409959	9.029325069	48.98585736	89.96292202	
	0.241335248	82.79414453	60.68678955	36.47467781				0
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
346	C22 Sc14	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.042436228	64.00112666	84.62593646	
	96.89993412	0.41692077	0	-19.00288766	1	101.6634351	84.71952928	
	169.4390586	847.1952928	0.061601385	0.12320277	0.616013848	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.271880583	0.299745647	0.52580748	
	3	2	1	5	2			
347	C23 Sc14	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.278279513	39.76903222	32.83555671	
	41.4875192	0.161768675	16.15470806	11.71718357	7.21255982	1	134.22169	111.8514083
	223.7028167	1118.514083	0.081329555	0.162659111	0.813295554	0.126338191	0.188706502	
	0.135993177	0.31838757	0.379056788	0.311830131	0.199858563	0.270857949	0.562562843	
	3	2	1	5	3			
348	C24 Sc14	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.062745095	33.25451259	101.091395	
	38.46617124	0.49804001	19.94219255	13.6628951	10.03885165			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
349	C25 Sc14	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.082653982	22.39183764	108.0009528	
	14.23314753	0.532080852	56.41335324	34.29086062	24.50163823	1	34.29086062	
	28.57571718	57.15143436	285.7571718	0.020778016	0.041556032	0.207780162	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248653744	0.228192197	
	0.334194513	2	3	1	5	5		
350	C01 Sc15	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806	
	15.58175563	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	

	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906	2	3	1	1	1		
351	C02 Sc15	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	2.413815951	
	0.172396809	14.4589725	9.78575639	8.14083227			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	
352	C03 Sc15	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292	
	38.75328479	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511	3	2	1	3			
353	C04 Sc15	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078	
	60.18594426	0.01822255	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	
354	C05 Sc15	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431	
	35.23066379	0.124450664	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	
355	C06 Sc15	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	40.57201135	0.035027674	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	
356	C07 Sc15	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	1.865589249	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	
357	C08 Sc15	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537	
	40.73125304	0.388419366	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	
358	C09 Sc15	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286	
	77.94630218	0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403	
	3	2	1	4			0.716039279	
359	C10 Sc15	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434	
	70.49309225	0.342126169	0	0	-22.08804665		0	

	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
360	C11	Sc15	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	60.59791036		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1			
361	C12	Sc15	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	9.723653134		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1			
362	C13	Sc15	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	74.02342422		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
363	C14	Sc15	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	71.01386276		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
364	C15	Sc15	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	14.33836837		0.29160088	59.40046614	36.65684749	25.88826616		
	0		0	0	0.251517278	0.292575574	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
365	C16	Sc15	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	52.60265939		0.503571269	54.63121188	39.32311405	23.01041848		
	0		0	0	0.198021052	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
366	C17	Sc15	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	2.496394502		0.443193522	0	-1.91148136			0
	0		0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
367	C18	Sc15	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	10.37889515		0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	

368	C19	Sc15	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	26.72719825		0.443400275	68.47439068	51.1849573	29.60747804			
	0		0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3	4
369	C20	Sc15	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	13.75084253		0.227232539	26.74737871	17.31056311	13.26088315			
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1	4
370	C21	Sc15	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	62.97404541	
	0.241335248		79.75400352	58.45841461	36.47467781			0	
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
371	C22	Sc15	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	67.82995388		0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2				
372	C23	Sc15	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	29.04126344		0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781		3	2	1	5	3		
373	C24	Sc15	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	
	26.92631987		0.49804001	19.45536051	13.32935429	10.03885165			
	0		0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
374	C25	Sc15	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528	
	9.963203272		0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789		2	3	1	5	5		
375	C01	Sc16	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806	
	17.80772072		0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906		2	3	1	1			
376	C02	Sc16	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	2.758646801	
	0.172396809		14.4589725	9.78575639	8.14083227			0	

	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445		0.189169138	0.193388639	1	3	2	1
377	C03	Sc16	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	44.28946833		0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511		3	2	1	3		
378	C04	Sc16	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	68.7839363		0.01822255	95.08406081	66.3617024	42.25345504		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
379	C05	Sc16	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	40.26361576		0.124450664	52.13742096	32.61644881	20.86424576		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
380	C06	Sc16	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301
	46.36801297		0.035027674	65.22005008	41.54117107	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
381	C07	Sc16	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887
	2.132101999		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
382	C08	Sc16	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	46.55000347		0.388419366	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
383	C09	Sc16	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	89.08148821		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4			0.716039279
384	C10	Sc16	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	80.563534	0.342126169	0	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	0
	0.19878542		0.206429195	0.192206618	2	1	3	2
385	C11	Sc16	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	69.2547547		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192

	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2 3	1 3	1			
386	C12 Sc16	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	11.11274644	0.505706614	94.39059844	62.80753253	38.93713794	1 62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401	3 2	1 3	2			
387	C13 Sc16	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	84.59819911	0.082559047	0 0	-6.64332145			0
	0 0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2 1	3 3	3	
388	C14 Sc16	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	81.15870029	0.108428766	86.03174795	55.17132441	34.34574479	1 55.17132441	
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205 0.236858507	0.268440329	
	0.358556204	3 2	1 3	4			
389	C15 Sc16	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	16.38670671	0.29160088	59.40046614	36.65684749	25.88826616		
	0 0	0 0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2 1	3 3	5
390	C16 Sc16	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	60.11732502	0.503571269	54.63121188	39.32311405	23.01041848		
	0 0	0 0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1 2	3 4	1
391	C17 Sc16	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	2.853022288	0.443193522	0 0	-1.91148136			0
	0 0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3 2	1 4	2	
392	C18 Sc16	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	11.86159446	0.56511885	32.43860895	22.21901297	13.90560646	1 22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321	3 2	1 4	3			
393	C19 Sc16	C19 0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565
	30.54536943	0.443400275	68.47439068	51.1849573	29.60747804		
	0 0	0 0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1 2	3 4	4

394	C20	Sc16	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125
	15.71524861		0.227232539	26.74737871	17.31056311	13.26088315		
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
								4
								5
395	C21	Sc16	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	0.018576202
	0.241335248		79.75400352	58.45841461	36.47467781			71.97033762
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0
	0.184443254		0.17732464	0.165746932	1	2	3	5
								1
396	C22	Sc16	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646
	77.51994729		0.41692077	0	-19.00288766	1	97.78152866	81.48460722
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2			
397	C23	Sc16	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671
	33.19001536		0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781		3	2	1	5	3	
398	C24	Sc16	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395
	30.772937	0.49804001	19.45536051	13.32935429	10.03885165			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
								5
								4
399	C25	Sc16	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528
	11.38651802		0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789		2	3	1	5	5	
400	C01	Sc17	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	20.03368581		0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906		2	3	1	1		
401	C02	Sc17	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	0.878117436
	0.172396809		14.4589725	9.78575639	8.14083227			3.103477651
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	1
								2
402	C03	Sc17	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	49.82565187		0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916

	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511	3	2	1	3		
403	C04 Sc17	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	77.38192834	0.01822255	95.08406081	66.3617024	42.25345504		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
404	C05 Sc17	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	45.29656773	0.124450664	52.13742096	32.61644881	20.86424576		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
405	C06 Sc17	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301
	52.16401459	0.035027674	65.22005008	41.54117107	27.41156624		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
406	C07 Sc17	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887
	2.398614749	0.179983081	0	-4.36085524			0
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684	0.166496609	0.169732566	2	3	1	2
407	C08 Sc17	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	52.36875391	0.388419366	78.78068852	54.16863022	32.83781904		
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1
408	C09 Sc17	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	100.2166742	0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4		
409	C10 Sc17	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	90.63397576	0.342126169	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
410	C11 Sc17	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	77.91159903	0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2	3	1	3		
411	C12 Sc17	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506

	12.50183974	0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742	
	0.383646401	3	2	1	3	2		
412	C13 Sc17	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835	
	95.17297399	0.082559047	0	-6.64332145			0	
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543	
	0.193600456	0.194835395	0.186649271	2	1	3	3	
413	C14 Sc17	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416	
	91.30353783	0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441	
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757	
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329	
	0.358556204	3	2	1	3	4		
414	C15 Sc17	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803	
	18.43504505	0.29160088	59.40046614	36.65684749	25.88826616			
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982	
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3	5
415	C16 Sc17	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214	
	67.63199065	0.503571269	54.63121188	39.32311405	23.01041848			
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715	
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
416	C17 Sc17	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932	
	3.209650074	0.443193522	0	-1.91148136			0	
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731	
	0.195078226	0.211045796	0.212449365	3	2	1	4	
417	C18 Sc17	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548	
	13.34429377	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379	
	0.233220321	3	2	1	4	3		
418	C19 Sc17	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	34.36354061	0.443400275	68.47439068	51.1849573	29.60747804			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
	0.233220321	3	2	1	4	3	4	
419	C20 Sc17	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	17.67965468	0.227232539	26.74737871	17.31056311	13.26088315			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
								5

420	C21	Sc17	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	80.96662982	
	0.241335248		79.75400352	58.45841461	36.47467781			0	
	0	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
421	C22	Sc17	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	87.2099407		0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2				
422	C23	Sc17	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	37.33876728		0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781		3	2	1	5	3		
423	C24	Sc17	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	
	34.61955412		0.49804001	19.45536051	13.32935429	10.03885165			
	0	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
								4	
424	C25	Sc17	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528	
	12.80983278		0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789		2	3	1	5	5		
425	C01	Sc18	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806	
	22.2596509		0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906		2	3	1	1			
426	C02	Sc18	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	3.448308502	
	0.172396809		14.4589725	9.78575639	8.14083227			0	
	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445		0.189169138	0.193388639	1	3	2	1	2
427	C03	Sc18	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292	
	55.36183542		0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511		3	2	1	1	3		
428	C04	Sc18	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078	

	85.97992038	0.01822255	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	4
429	C05	Sc18	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431	
	50.3295197	0.124450664	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
430	C06	Sc18	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	57.96001621	0.035027674	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
431	C07	Sc18	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
432	C08	Sc18	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537	
	58.18750434	0.388419366	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
433	C09	Sc18	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286	
	111.3518603	0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994	0.232017403
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4			
434	C10	Sc18	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434	
	100.7044175	0.342126169	0	-22.08804665			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
435	C11	Sc18	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598	
	86.56844337	0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192	
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294	
	0.389870185	2	3	1	3	1		
436	C12	Sc18	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506	
	13.89093305	0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742	
	0.383646401	3	2	1	3	2		

437	C13	Sc18	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
438	C14	Sc18	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
439	C15	Sc18	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	59.40046614	36.65684749	25.88826616		
	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
440	C16	Sc18	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	54.63121188	39.32311405	23.01041848		
	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
441	C17	Sc18	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	3.56627786		0.443193522	0	-1.91148136			0
	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
442	C18	Sc18	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	14.82699307		0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	
443	C19	Sc18	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565
	38.18171179		0.443400275	68.47439068	51.1849573	29.60747804		
	0	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
444	C20	Sc18	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125
	19.64406076		0.227232539	26.74737871	17.31056311	13.26088315		
	0	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
445	C21	Sc18	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	89.96292202
	0.241335248		79.75400352	58.45841461	36.47467781			0
	0	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5

446	C22	Sc18	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646
	96.89993412		0.41692077	0	-19.00288766	1	97.78152866	81.48460722
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2			
447	C23	Sc18	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671
	41.4875192		0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781		3	2	1	5	3	
448	C24	Sc18	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395
	38.46617124		0.49804001	19.45536051	13.32935429	10.03885165		
	0		0	0	0.194999729	0.172101157	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
								5
449	C25	Sc18	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528
	14.23314753		0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789		2	3	1	5	5	
450	C01	Sc19	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	24.48561599		0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906		2	3	1	1		
451	C02	Sc19	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	0.878117436
	0.172396809		14.4589725	9.78575639	8.14083227			3.793139352
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
452	C03	Sc19	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	60.89801896		0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511		3	2	1	3		
453	C04	Sc19	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	94.57791241		0.018222255	95.08406081	66.3617024	42.25345504		
	0		0	0	0.214732899	0.18442312	0.126095549	0.407884499
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
								4
454	C05	Sc19	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431

	55.36247167	0.124450664	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	5
455	C06 Sc19	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	63.75601784	0.035027674	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	1
456	C07 Sc19	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	2.931640249	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
457	C08 Sc19	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537	
	64.00625477	0.388419366	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
458	C09 Sc19	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286	
	122.4870463	0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523	265.6105045	1328.052523	0.1	0.2	0.178780994	0.232017403	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4			
459	C10 Sc19	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434	
	110.7748593	0.342126169	0	-22.08804665			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
460	C11 Sc19	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598	
	95.22528771	0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192	
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294	
	0.389870185	2	3	1	3	1		
461	C12 Sc19	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506	
	15.28002635	0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742	
	0.383646401	3	2	1	3	2		
462	C13 Sc19	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835	
	116.3225238	0.082559047	0	-6.64332145			0	
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543	
	0.193600456	0.194835395	0.186649271	2	1	3	3	

463	C14	Sc19	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	111.5932129		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
464	C15	Sc19	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	22.53172173		0.29160088	59.40046614	36.65684749	25.88826616		
	0		0	0	0.251517278	0.292575574	0.225051384	0.421654228
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
								3
								5
465	C16	Sc19	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	82.6613219		0.503571269	54.63121188	39.32311405	23.01041848		
	0		0	0	0.198021052	0.185581091	0.191572754	0.409469615
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
								4
								1
466	C17	Sc19	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	3.922905646		0.443193522	0	-1.91148136			0
	0		0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
								2
								4
467	C18	Sc19	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	16.30969238		0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	
								3
468	C19	Sc19	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565
	41.99988296		0.443400275	68.47439068	51.1849573	29.60747804		
	0		0	0	0.19335296	0.154863434	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
								4
								4
469	C20	Sc19	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125
	21.60846683		0.227232539	26.74737871	17.31056311	13.26088315		
	0		0	0	0.266503103	0.213730709	0.290225506	0.462800059
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
								4
								5
470	C21	Sc19	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	0.018576202
	0.241335248		79.75400352	58.45841461	36.47467781			98.95921422
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0
	0.184443254		0.17732464	0.165746932	1	2	3	5
								1
471	C22	Sc19	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646
	106.5899275		0.41692077	0	-19.00288766	1	97.78152866	81.48460722
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416

	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2		
472	C23 Sc19	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671
	45.63627112	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202
	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781	3	2	1	5	3	
473	C24 Sc19	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395
	42.31278837	0.49804001	19.45536051	13.32935429	10.03885165		
	0	0	0	0.195074589	0.172101157	0.408593283	0.408513079
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
474	C25 Sc19	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528
	15.65646228	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789	2	3	1	5	5	
475	C01 Sc20	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	26.71158108	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906	2	3	1	1		
476	C02 Sc20	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	4.137970202
	0.172396809	14.4589725	9.78575639	8.14083227			0
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445	0.189169138	0.193388639	1	3	2	1
477	C03 Sc20	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	66.4342025	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511	3	2	1	3		
478	C04 Sc20	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	103.1759045	0.01822255	95.08406081	66.3617024	42.25345504		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
479	C05 Sc20	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	60.39542364	0.124450664	52.13742096	32.61644881	20.86424576		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
						1	5

480	C06	Sc20	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	69.55201946		0.035027674	65.22005008	41.54117107	27.41156624			
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2	2
481	C07	Sc20	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	3.198152999		0.179983081	0	-4.36085524			0	
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684		0.166496609	0.169732566	2	3	1	2	2
482	C08	Sc20	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537	
	69.82500521		0.388419366	78.78068852	54.16863022	32.83781904			
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1	2
483	C09	Sc20	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286	
	133.6222323		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994	0.232017403
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4				
484	C10	Sc20	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434	
	120.845301		0.342126169	0	-22.08804665			0	
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542		0.206429195	0.192206618	2	1	3	2	5
485	C11	Sc20	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598	
	103.882132		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192	
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923	
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294	
	0.389870185		2	3	1	3	1		
486	C12	Sc20	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506	
	16.66911966		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253	
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508	
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742	
	0.383646401		3	2	1	3	2		
487	C13	Sc20	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835	
	126.8972987		0.082559047	0	-6.64332145			0	
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543	
	0.193600456		0.194835395	0.186649271	2	1	3	3	
488	C14	Sc20	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416	
	121.7380504		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441	
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757	

	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204	3	2	1	3	4	
489	C15 Sc20	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	24.58006007	0.29160088	59.40046614	36.65684749	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
490	C16 Sc20	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	90.17598753	0.503571269	54.63121188	39.32311405	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
491	C17 Sc20	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	4.279533433	0.443193522	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
492	C18 Sc20	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	17.79239169	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321	3	2	1	4	3	
493	C19 Sc20	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565
	45.81805414	0.443400275	68.47439068	51.1849573	29.60747804		
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
494	C20 Sc20	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125
	23.57287291	0.227232539	26.74737871	17.31056311	13.26088315		
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1
495	C21 Sc20	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	0.018576202
	0.241335248	79.75400352	58.45841461	36.47467781			107.9555064
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254	0.17732464	0.165746932	1	2	3	5
496	C22 Sc20	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646
	116.2799209	0.41692077	0	-19.00288766	1	97.78152866	81.48460722
	162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2		
497	C23 Sc20	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671
	49.78502304	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202

	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781	3	2	1	5	3	
498	C24 Sc20	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395
	46.15940549	0.49804001	19.45536051	13.32935429	10.03885165		
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
499	C25 Sc20	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528
	17.07977704	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789	2	3	1	5	5	
500	C01 Sc21	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806
	28.93754617	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906	2	3	1	1		
501	C02 Sc21	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	0.878117436
	0.172396809	14.4589725	9.78575639	8.14083227			4.482801053
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445	0.189169138	0.193388639	1	3	2	0.386777277
502	C03 Sc21	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292
	71.97038605	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511	3	2	1	3		
503	C04 Sc21	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078
	111.7738965	0.018222255	95.08406081	66.3617024	42.25345504		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
504	C05 Sc21	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431
	65.42837561	0.124450664	52.13742096	32.61644881	20.86424576		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
505	C06 Sc21	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301
	75.34802107	0.035027674	65.22005008	41.54117107	27.41156624		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
						2	2
							1

506	C07	Sc21	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887
	3.464665749		0.179983081	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
507	C08	Sc21	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	75.64375564		0.388419366	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
508	C09	Sc21	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	144.7574184		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4			0.716039279
509	C10	Sc21	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	130.9157428		0.342126169	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
510	C11	Sc21	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	112.5389764		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3	5	
511	C12	Sc21	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	18.05821297		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3	2	
512	C13	Sc21	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	137.4720736		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
513	C14	Sc21	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	131.882888		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
514	C15	Sc21	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	26.62839841		0.29160088	59.40046614	36.65684749	25.88826616		

	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3	3
515	C16 Sc21	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214	
	97.69065316	0.503571269	54.63121188	39.32311405	23.01041848			
	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
516	C17 Sc21	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932	
	4.636161218	0.443193522	0	-1.91148136			0	
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731	
	0.195078226	0.211045796	0.212449365	3	2	1	4	2
517	C18 Sc21	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548	
	19.27509099	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379	
	0.233220321	3	2	1	4	3		
518	C19 Sc21	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	49.63622533	0.443400275	68.47439068	51.1849573	29.60747804			
	0	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
519	C20 Sc21	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	25.53727899	0.227232539	26.74737871	17.31056311	13.26088315			
	0	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
520	C21 Sc21	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	116.9517986	
	0.241335248	79.75400352	58.45841461	36.47467781			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
521	C22 Sc21	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	125.9699144	0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2			
522	C23 Sc21	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	53.93377496	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781	3	2	1	5	3		
523	C24 Sc21	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	

	50.00602261	0.49804001	19.45536051	13.32935429	10.03885165				
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079		
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5	4
524	C25 Sc21	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573		
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528		
	18.50309179	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418		
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204		
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852		
	0.335062789	2	3	1	5	5			
525	C01 Sc22	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891		
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	4.809156664		
	22.2596509	0.023692941	55.97017677	43.85213797	27.91552745	1	43.85213797		
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042		
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969		
	0.269251906	2	3	1	1	1			
526	C02 Sc22	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436	
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	24.49498737	3.448308502		
	0.120677766	14.4589725	9.78575639	8.14083227			0		
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277		
	0.222682445	0.189169138	0.193388639	1	3	2	1	2	
527	C03 Sc22	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569		
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	59.86102704		
	55.36183542	0.294913197	17.92942341	11.86471894	7.31625241	1	66.03334916		
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454		
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532		
	0.384179511	3	2	1	3				
528	C04 Sc22	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042		
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	2.589149554		
	85.97992038	0.012755785	95.08406081	66.3617024	42.25345504				
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941		
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1	4
529	C05 Sc22	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928		
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	17.68256302		
	50.3295197	0.087115465	52.13742096	32.61644881	20.86424576				
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602		
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1	5
530	C06 Sc22	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007		
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	4.976904311		
	57.96001621	0.024519372	65.22005008	41.54117107	27.41156624				
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035		
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2	1
531	C07 Sc22	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116		
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	25.57288221		
	2.665127499	0.125988157	0	-4.36085524			0		
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132		
	0.168102684	0.166496609	0.169732566	2	3	1	2	2	

532	C08	Sc22	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	55.18853576
	58.18750434		0.271893556	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
533	C09	Sc22	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	26.05134201
	111.3518603		0.128345352	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
534	C10	Sc22	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	48.61097038
	100.7044175		0.239488318	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
535	C11	Sc22	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	6.516304186
	86.56844337		0.032103427	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3	1	
536	C12	Sc22	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	71.85328541
	13.89093305		0.35399463	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3	2	
537	C13	Sc22	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	11.73039584
	105.7477489		0.057791333	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
538	C14	Sc22	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	15.40609291
	101.4483754		0.075900136	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
539	C15	Sc22	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	41.43208862
	20.48338339		0.204120616	59.40046614	36.65684749	25.88826616		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
540	C16	Sc22	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	71.54988499
	75.14665628		0.352499888	54.63121188	39.32311405	23.01041848		

		0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
		0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
541	C17	Sc22	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
				0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	62.97111752
				3.56627786	0.310235466	0	-1.91148136		0
				0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592
				0.195078226	0.211045796	0.212449365	3	2	1
542	C18	Sc22	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
				0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943
				14.82699307	0.395583195	32.43860895	22.21901297	13.90560646	1
				18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023
				0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611
				0.233220321	3	2	1	4	2
543	C19	Sc22	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
				0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729
				38.18171179	0.310380192	68.47439068	51.1849573	29.60747804	63.00049396
				0	0	0.19335296	0.154863434	0.16721044	0.416396653
				0.385127801	0.208198327	0.194126634	0.192563901	1	2
544	C20	Sc22	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
				0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382
				19.64406076	0.159062778	26.74737871	17.31056311	13.26088315	32.28631788
				0	0	0.266503103	0.213730709	0.290225506	0.462800059
				0.473734591	0.23140003	0.208910304	0.236867296	2	3
545	C21	Sc22	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
				0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	34.29010015
				0.168934674	79.75400352	58.45841461	36.47467781		89.96292202
				0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928
				0.184443254	0.17732464	0.165746932	1	2	3
546	C22	Sc22	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
				0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666
				96.89993412	0.291844539	0	-19.00288766	1	97.78152866
				162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139
				0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727
				3	2	1	5	2	
547	C23	Sc22	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
				0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222
				41.4875192	0.113238072	15.58311099	11.30259806	7.21255982	1
				108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431
				0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657
				0.563103781	3	2	1	5	3
548	C24	Sc22	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
				0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259
				38.46617124	0.348628007	19.45536051	13.32935429	10.03885165	70.7639765
				0	0	0.195074589	0.194999729	0.172101157	0.408593283
				0.377206528	0.204296641	0.204256539	0.188603264	1	2
549	C25	Sc22	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
				0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764

	14.23314753	0.372456597	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789	2	3	1	5	5		
550	C01 Sc23	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	5.496179045	
	22.2596509	0.027077647	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906	2	3	1	1	1		
551	C02 Sc23	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	27.99427128	3.448308502	
	0.137917447	14.4589725	9.78575639	8.14083227			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	2
552	C03 Sc23	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	68.41260233	
	55.36183542	0.337043654	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511	3	2	1	3			
553	C04 Sc23	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	2.959028062	
	85.97992038	0.01457804	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
554	C05 Sc23	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	20.20864345	
	50.3295197	0.099560531	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
555	C06 Sc23	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	5.687890641	
	57.96001621	0.028022139	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
556	C07 Sc23	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	29.2261511	
	2.665127499	0.143986465	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
557	C08 Sc23	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	63.07261229	
	58.18750434	0.310735493	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2

558	C09	Sc23	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	29.77296229
	111.3518603		0.146680402	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
559	C10	Sc23	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	55.55539472
	100.7044175		0.273700935	0	-22.08804665			0
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
560	C11	Sc23	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	7.447204784
	86.56844337		0.036689631	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3		
561	C12	Sc23	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	82.11804047
	13.89093305		0.404565292	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3		
562	C13	Sc23	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	13.40616668
	105.7477489		0.066047238	0	-6.64332145			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
563	C14	Sc23	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	17.60696332
	101.4483754		0.086743013	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3		
564	C15	Sc23	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	47.35095843
	20.48338339		0.233280704	59.40046614	36.65684749	25.88826616		
	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
565	C16	Sc23	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	81.77129713
	75.14665628		0.402857015	54.63121188	39.32311405	23.01041848		
	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
566	C17	Sc23	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	71.96699145
	3.56627786		0.354554818	0	0	-1.91148136		0

	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
567	C18	Sc23	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	91.76556385
	14.82699307		0.45209508	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	
568	C19	Sc23	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	72.00056452
	38.18171179		0.35472022	68.47439068	51.1849573	29.60747804		
	0		0	0	0.19335296	0.154863434	0.16721044	0.416396653
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
569	C20	Sc23	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	36.898649
	19.64406076		0.181786031	26.74737871	17.31056311	13.26088315		
	0		0	0	0.266503103	0.213730709	0.290225506	0.462800059
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
570	C21	Sc23	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	39.18868589	89.96292202
	0.193068198		79.75400352	58.45841461	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
571	C22	Sc23	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	67.70074917
	96.89993412		0.333536616	0	0	-19.00288766	1	97.78152866
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2			
572	C23	Sc23	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	26.26844536
	41.4875192		0.12941494	15.58311099	11.30259806	7.21255982	1	129.7843202
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781		3	2	1	5	3	
573	C24	Sc23	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	80.873116
	38.46617124		0.398432008	19.45536051	13.32935429	10.03885165		
	0		0	0	0.195074589	0.194999729	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
574	C25	Sc23	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	86.40076224
	14.23314753		0.425664682	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789		2	3	1	5	5	

575	C01	Sc24	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.183201425
	22.2596509		0.030462352	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906		2	3	1	1		
576	C02	Sc24	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	31.49355519	0.878117436
	0.155157128		14.4589725	9.78575639	8.14083227			3.448308502
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
577	C03	Sc24	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	76.96417762
	55.36183542		0.379174111	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511		3	2	1	3		
578	C04	Sc24	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.32890657
	85.97992038		0.016400295	95.08406081	66.3617024	42.25345504		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
579	C05	Sc24	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	22.73472388
	50.3295197		0.112005598	52.13742096	32.61644881	20.86424576		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
580	C06	Sc24	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	6.398876971
	57.96001621		0.031524906	65.22005008	41.54117107	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
581	C07	Sc24	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	32.87941999
	2.665127499		0.161984773	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
582	C08	Sc24	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	70.95668883
	58.18750434		0.34957743	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
583	C09	Sc24	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	33.49458258
	111.3518603		0.165015452	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
								0.232017403

	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	1	2	4			
584	C10 Sc24	C10 0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	62.49981906
	100.7044175	0.307913552	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
585	C11 Sc24	C11 0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	8.378105382
	86.56844337	0.041275834	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2	3	1	3	1	
586	C12 Sc24	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	92.38279552
	13.89093305	0.455135953	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401	3	2	1	3	2	
587	C13 Sc24	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	15.08193751
	105.7477489	0.074303142	0	-6.64332145			0
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2	1	3	3
588	C14 Sc24	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	19.80783374
	101.4483754	0.09758589	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204	3	2	1	3	4	
589	C15 Sc24	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	53.26982823
	20.48338339	0.262440792	59.40046614	36.65684749	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
590	C16 Sc24	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	91.99270928
	75.14665628	0.453214142	54.63121188	39.32311405	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
591	C17 Sc24	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	80.96286538
	3.56627786	0.39887417	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
592	C18 Sc24	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	103.2362593

	14.82699307	0.508606965	32.43860895	22.21901297	13.90560646	1	22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379	
	0.233220321	3	2	1	4	3		
593	C19 Sc24	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	81.00063509	
	38.18171179	0.399060247	68.47439068	51.1849573	29.60747804			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
594	C20 Sc24	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	41.51098013	
	19.64406076	0.204509285	26.74737871	17.31056311	13.26088315			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
595	C21 Sc24	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	44.08727163	89.96292202	
	0.217201723	79.75400352	58.45841461	36.47467781				0
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
596	C22 Sc24	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	76.16334281	
	96.89993412	0.375228693	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2			
597	C23 Sc24	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	29.55200103	
	41.4875192	0.145591807	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781	3	2	1	5	3		
598	C24 Sc24	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	90.98225549	
	38.46617124	0.448236009	19.45536051	13.32935429	10.03885165			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
599	C25 Sc24	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	97.20085752	
	14.23314753	0.478872767	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789	2	3	1	5	5		
600	C01 Sc25	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806	
	22.2596509	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	

	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906	2	3	1	1	1		
601	C02 Sc25	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	3.448308502	
	0.172396809	14.4589725	9.78575639	8.14083227			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	
602	C03 Sc25	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292	
	55.36183542	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511	3	2	1	3			
603	C04 Sc25	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078	
	85.97992038	0.01822255	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	
604	C05 Sc25	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431	
	50.3295197	0.124450664	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	
605	C06 Sc25	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	57.96001621	0.035027674	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	
606	C07 Sc25	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	
607	C08 Sc25	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537	
	58.18750434	0.388419366	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	
608	C09 Sc25	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286	
	111.3518603	0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403	
	3	2	4				0.716039279	
609	C10 Sc25	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434	
	100.7044175	0.342126169	0	0	-22.08804665		0	

	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
610	C11	Sc25	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3	5	
611	C12	Sc25	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3	2	
612	C13	Sc25	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
613	C14	Sc25	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
614	C15	Sc25	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	59.40046614	36.65684749	25.88826616		
	0		0	0	0.251517278	0.292575574	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
615	C16	Sc25	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	54.63121188	39.32311405	23.01041848		
	0		0	0	0.198021052	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
616	C17	Sc25	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932
	3.56627786		0.443193522	0	-1.91148136			0
	0		0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
617	C18	Sc25	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548
	14.82699307		0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	

618	C19	Sc25	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	38.18171179		0.443400275	68.47439068	51.1849573	29.60747804			
	0		0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3	4
619	C20	Sc25	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	19.64406076		0.227232539	26.74737871	17.31056311	13.26088315			
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1	4
620	C21	Sc25	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	89.96292202	
	0.241335248		79.75400352	58.45841461	36.47467781			0	
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
621	C22	Sc25	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	96.89993412		0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2				
622	C23	Sc25	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	41.4875192		0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781		3	2	1	5	3		
623	C24	Sc25	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	
	38.46617124		0.49804001	19.45536051	13.32935429	10.03885165			
	0		0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
624	C25	Sc25	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528	
	14.23314753		0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789		2	3	1	5	5		
625	C01	Sc26	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	7.557246186	
	22.2596509		0.037231764	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906		2	3	1	1			
626	C02	Sc26	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	38.49212301	3.448308502	
	0.18963649		14.4589725	9.78575639	8.14083227			0	

	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445		0.189169138	0.193388639	1	3	2	1
627	C03	Sc26	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	94.06732821
	55.36183542		0.463435024	17.92942341	11.86471894	7.31625241	1	66.03334916
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511		3	2	1	3		
628	C04	Sc26	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	4.068663585
	85.97992038		0.020044805	95.08400681	66.3617024	42.25345504		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
629	C05	Sc26	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	27.78688474
	50.3295197		0.13689573	52.13742096	32.61644881	20.86424576		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
630	C06	Sc26	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.820849631
	57.96001621		0.038530441	65.22005008	41.54117107	27.41156624		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
631	C07	Sc26	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	40.18595776
	2.665127499		0.197981389	0	-4.36085524			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
632	C08	Sc26	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	86.7248419
	58.18750434		0.427261303	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
633	C09	Sc26	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	40.93782315
	111.3518603		0.201685552	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3	2	1	2	4			0.716039279
634	C10	Sc26	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	76.38866775
	100.7044175		0.376338786	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
635	C11	Sc26	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	10.23990658
	86.56844337		0.050448242	10.53282093	6.400224457	3.87822105	1	57.72715192

	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2 3	1 3	1			
636	C12 Sc26	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	112.9123056
	13.89093305	0.556277276	94.39059844	62.80753253	38.93713794	1 62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401	3 2	1 3	2			
637	C13 Sc26	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	18.43347918
	105.7477489	0.090814952	0 0	-6.64332145			0
	0 0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2 1	3 3	3	
638	C14 Sc26	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	24.20957457
	101.4483754	0.119271643	86.03174795	55.17132441	34.34574479	1 55.17132441	
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205 0.236858507	0.268440329	
	0.358556204	3 2	1 3	4			
639	C15 Sc26	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	65.10756784
	20.48338339	0.320760968	59.40046614	36.65684749	25.88826616		
	0 0	0 0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2 1	3 3	5
640	C16 Sc26	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	112.4355336
	75.14665628	0.553928396	54.63121188	39.32311405	23.01041848		
	0 0	0 0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1 2	3 4	1
641	C17 Sc26	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	98.95461325
	3.56627786	0.487512875	0 0	-1.91148136			0
	0 0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3 2	1 4	2	
642	C18 Sc26	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	126.1776503
	14.82699307	0.621630735	32.43860895	22.21901297	13.90560646	1 22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321	3 2	1 4	3			
643	C19 Sc26	C19 0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	99.00077622
	38.18171179	0.487740302	68.47439068	51.1849573	29.60747804		
	0 0	0 0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1 2	3 4	4

644	C20	Sc26	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	50.73564238
	19.64406076		0.249955793	26.74737871	17.31056311	13.26088315		
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
645	C21	Sc26	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	53.8844431	89.96292202
	0.265468773		79.75400352	58.45841461	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
646	C22	Sc26	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	93.0885301
	96.89993412		0	0	-19.00288766	1	97.78152866	81.48460722
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877
	3	2	1	5	2			
647	C23	Sc26	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	36.11911238
	41.4875192		0.177945542	15.58311099	11.30259806	7.21255982	1	129.7843202
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137
	0.563103781		3	2	1	5	3	
648	C24	Sc26	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	111.2005345
	38.46617124		0.547844011	19.45536051	13.32935429	10.03885165		
	0		0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
649	C25	Sc26	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	118.8010481
	14.23314753		0.585288938	54.93115148	33.38990418	24.50163823	1	33.38990418
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852
	0.335062789		2	3	1	5	5	
650	C01	Sc27	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	8.244268567
	22.2596509		0.04061647	55.97017677	43.85213797	27.91552745	1	43.85213797
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969
	0.269251906		2	3	1	1		
651	C02	Sc27	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	41.99140692	0.878117436
	0.206876171		14.4589725	9.78575639	8.14083227			3.448308502
	0		0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
652	C03	Sc27	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	102.6189035
	55.36183542		0.505565481	17.92942341	11.86471894	7.31625241	1	66.03334916

	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532
	0.384179511	3	2	1	3		
653	C04 Sc27	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	4.438542093
	85.97992038	0.021867059	95.08406081	66.3617024	42.25345504		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
654	C05 Sc27	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	30.31296517
	50.3295197	0.149340797	52.13742096	32.61644881	20.86424576		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
655	C06 Sc27	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	8.531835961
	57.96001621	0.042033208	65.22005008	41.54117107	27.41156624		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
656	C07 Sc27	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	43.83922665
	2.665127499	0.215979697	0	-4.36085524			0
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684	0.166496609	0.169732566	2	3	1	2
657	C08 Sc27	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	94.60891844
	58.18750434	0.466103239	78.78068852	54.16863022	32.83781904		
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1
658	C09 Sc27	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	44.65944344
	111.3518603	0.220020603	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4		
659	C10 Sc27	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	83.33309209
	100.7044175	0.410551403	0	-22.08804665			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
660	C11 Sc27	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	11.17080718
	86.56844337	0.055034446	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185	2	3	1	3	1	
661	C12 Sc27	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	123.1770607

	13.89093305	0.606847937	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401	3	2	1	3	2	
662	C13 Sc27	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	20.10925002
	105.7477489	0.099070856	0	-6.64332145			0
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2	1	3	3
663	C14 Sc27	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	26.41044499
	101.4483754	0.130114519	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368	91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204	3	2	1	3	4	
664	C15 Sc27	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	71.02643764
	20.48338339	0.349921056	59.40046614	36.65684749	25.88826616		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
665	C16 Sc27	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	122.6569457
	75.14665628	0.604285523	54.63121188	39.32311405	23.01041848		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
666	C17 Sc27	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	107.9504872
	3.56627786	0.531832227	0	-1.91148136			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
667	C18 Sc27	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	137.6483458
	14.82699307	0.67814262	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321	3	2	1	4	3	
668	C19 Sc27	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	108.0008468
	38.18171179	0.53208033	68.47439068	51.1849573	29.60747804		
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3
669	C20 Sc27	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	55.34797351
	19.64406076	0.272679047	26.74737871	17.31056311	13.26088315		
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1
						4	5

670	C21	Sc27	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	58.78302883		89.96292202
	0.289602298		79.75400352	58.45841461	36.47467781				0
	0	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928		0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
671	C22	Sc27	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	64.00112666	101.5511237	
	96.89993412		0.500304924	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144		814.8460722	0.061356464	0.122712929	0.613564643	0.273632139		0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271758123	0.299500727		0.524582877
	3	2	1	5	2				
672	C23	Sc27	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	39.40266805	
	41.4875192		0.19412241	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002		216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502		0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781		3	2	1	5	3		
673	C24	Sc27	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	121.309674	
	38.46617124		0.597648012	19.45536051	13.32935429	10.03885165			
	0	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
									4
674	C25	Sc27	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	129.6011434	
	14.23314753		0.638497023	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015		55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789		2	3	1	5	5		
675	C01	Sc28	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	16.09475155	8.931290948	
	22.2596509		0.044001176	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831		73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906		2	3	1	1			
676	C02	Sc28	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593		0.67046751	44.92377119	0.012963116	36.78293892	45.49069083	3.448308502	
	0.224115852		14.4589725	9.78575639	8.14083227			0	
	0	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445		0.189169138	0.193388639	1	3	2	1	2
677	C03	Sc28	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	111.1704788	
	55.36183542		0.547695938	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097		110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697		0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511		3	2	1	1	3		
678	C04	Sc28	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	4.808420601	

	85.97992038	0.023689314	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	4
679	C05	Sc28	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	32.8390456	
	50.3295197	0.161785863	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
680	C06	Sc28	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	9.242822291	
	57.96001621	0.045535976	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
681	C07	Sc28	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	47.49249553	
	2.665127499	0.233978005	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
682	C08	Sc28	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	102.492995	
	58.18750434	0.504945176	78.78068852	54.16863022	32.83781904			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
683	C09	Sc28	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	48.38106372	
	111.3518603	0.238355653	93.12275706	60.3881515	40.33139339	1	159.3663027	
	132.8052523	265.6105045	1328.052523	0.1	0.2	1	0.178780994	0.232017403
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4			
684	C10	Sc28	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	90.27751642	
	100.7044175	0.444764019	0	-22.08804665			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
685	C11	Sc28	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	12.10170777	
	86.56844337	0.05962065	10.53282093	6.400224457	3.87822105	1	57.72715192	
	48.10595993	96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294	
	0.389870185	2	3	1	3	1		
686	C12	Sc28	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	133.4418158	
	13.89093305	0.657418599	94.39059844	62.80753253	38.93713794	1	62.80753253	
	52.33961044	104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742	
	0.383646401	3	2	1	3	2		

687	C13	Sc28	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	21.78502086
	105.7477489		0.107326761	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
688	C14	Sc28	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	28.61131541
	101.4483754		0.140957396	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
689	C15	Sc28	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	76.94530744
	20.48338339		0.379081144	59.40046614	36.65684749	25.88826616		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
690	C16	Sc28	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	132.8783578
	75.14665628		0.654642649	54.63121188	39.32311405	23.01041848		
	0		0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
691	C17	Sc28	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	116.9463611
	3.56627786		0.576151579	0	-1.91148136			0
	0		0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
692	C18	Sc28	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	149.1190412
	14.82699307		0.734654505	32.43860895	22.21901297	13.90560646	1	22.21901297
	18.51584414		37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379
	0.233220321		3	2	1	4	3	
693	C19	Sc28	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	117.0009173
	38.18171179		0.576420357	68.47439068	51.1849573	29.60747804		
	0		0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
694	C20	Sc28	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	59.96030463
	19.64406076		0.295402301	26.74737871	17.31056311	13.26088315		
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
695	C21	Sc28	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.029325069	63.68161457	89.96292202
	0.313735822		79.75400352	58.45841461	36.47467781			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5

696	C22	Sc28	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
				0.380141173	0.550948219	0.745334431	44.998239	0.032643252
				0.541997001	0	0	-19.00288766	1
				162.9692144	814.8460722	0.061356464	0.122712929	0.613564643
				0.255171744	0.482159781	0.476288524	0.435601111	0.271758123
				3	2	1	5	2
697	C23	Sc28	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
				0.21017401	0.752755554	0.066536481	46.98159204	0.214061164
				41.4875192	0.210299277	15.58311099	11.30259806	7.21255982
				108.1536002	216.3072004	1081.536002	0.081437743	0.162875486
				0.188706502	0.135993177	0.31838757	0.379056788	0.311830131
				0.563103781	3	2	1	5
				3	2	1	5	3
698	C24	Sc28	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
				0.92480797	0.26329677	0.065961091	43.29336424	0.048265458
				38.46617124	0.647452013	19.45536051	13.32935429	10.03885165
				0	0	0.195074589	0.194999729	0.172101157
				0.377206528	0.204296641	0.204256539	0.188603264	1
				2	3	5	2	3
699	C25	Sc28	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
				0.234362086	0.616778357	0.949016321	46.89347587	0.063579986
				14.23314753	0.691705108	54.93115148	33.38990418	24.50163823
				27.82492015	55.64984029	278.2492015	0.020951671	0.041903343
				0.234608961	0.294051043	0.476529471	0.414828361	0.460608863
				0.335062789	2	3	1	5
				2	3	1	5	5
700	C01	Sc29	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
				0.092338595	0.186260211	0.345560727	44.010279	0.217997451
				22.2596509	0.033847058	65.65109098	51.43704855	32.74395291
				42.86420713	85.72841425	428.6420713	0.027107795	0.05421559
				0.105685808	0.089720661	0.310543058	0.275436802	0.263338126
				0.267208038	2	3	1	1
				2	3	1	1	1
701	C02	Sc29	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
				0.027387593	0.67046751	44.92377119	0.012963116	25.74805725
				0.172396809	34.05808047	23.05032938	19.17571394	34.9928391
				0	0.257404041	0.194814404	0.208494062	0.445364891
				0.222682445	0.189169138	0.193388639	1	3
				1	2	1	2	1
				1	2	1	2	2
702	C03	Sc29	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
				0.968261576	0.313424178	0.692322616	45.9990459	0.274831239
				55.36183542	0.421304567	46.36858098	30.68420932	18.92109046
				75.65355704	151.3071141	756.5355704	0.04784414	0.095688279
				0.237553697	0.192031501	0.413221665	0.397937162	0.354009513
				0.416225455	3	2	1	3
				3	2	1	3	3
703	C04	Sc29	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
				0.878142503	0.098346834	0.421107625	46.08943358	0.217661196
				85.97992038	0.018222255	97.67372182	68.1690959	43.4042486
				0	0	0.214732899	0.18442312	0.126095549
				0.3266149	0.203942249	0.189644971	0.16330745	1
				1	2	3	1	4
704	C05	Sc29	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
				0.834625672	0.018288277	0.750144315	46.44082811	0.210183901
								17.90360765
								25.26080431

	50.3295197	0.124450664	71.31132816	44.61137973	28.53722046			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	5
705	C06 Sc29	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	11.25617792	7.109863301	
	57.96001621	0.035027674	76.69792376	48.85187251	32.23564249			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	1
706	C07 Sc29	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	33.74358253	36.53268887	
	2.665127499	0.179983081	18.33233601	14.46606799	10.10068013			
	0	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	
	0.339465132	0.168102684	0.166496609	0.169732566	2	3	1	2
707	C08 Sc29	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	8.390011708	78.84076537	
	58.18750434	0.388419366	87.40712142	60.10005914	36.43353834			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2
708	C09 Sc29	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	3.879128793	37.21620286	
	111.3518603	0.183350502	96.96133191	62.87738664	41.99387716	1	175.6578623	
	146.3815519	292.7631038	1463.815519	0.0925733	0.185146599	0.925732997	0.178780994	
	0.232017403	0.229727169	0.392146196	0.44667726	0.432078559	0.242359748	0.315911929	
	0.678905778	3	2	1	2	4		
709	C10 Sc29	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	45.92716747	69.4442434	
	100.7044175	0.342126169	0	-2.40497487			0	
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542	0.206429195	0.192206618	2	1	3	2	5
710	C11 Sc29	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	27.7047949	9.30900598	
	86.56844337	0.045862038	42.7798935	25.99502286	15.75170457	1	112.3632927	
	93.63607728	187.2721546	936.3607728	0.059216483	0.118432965	0.592164827	0.316867923	
	0.266455347	0.264174875	0.486389832	0.435666719	0.417511021	0.272803157	0.277049842	
	0.504837924	3	2	1	3	1		
711	C12 Sc29	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	4.249414046	102.6475506	
	13.89093305	0.505706614	98.80545886	65.74518198	40.75831539	1	65.74518198	
	54.78765165	109.5753033	547.8765165	0.034648312	0.069296624	0.346483121	0.220522508	
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.223738995	0.241588256	
	0.359833968	3	2	1	3	2		
712	C13 Sc29	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	35.3814082	16.75770835	
	105.7477489	0.082559047	17.79728864	11.67610597	8.52013921			
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	
	0.373298543	0.193600456	0.194835395	0.186649271	2	1	3	3

713	C14	Sc29	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	8.135060816	22.00870416
	101.4483754		0.108428766	94.76487598	60.77179459	37.83219942	1	60.77179459
	50.64316216		101.2863243	506.4316216	0.032027291	0.064054583	0.320272915	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.235562557	0.26584843
	0.345596707		3	2	1	3	4	
714	C15	Sc29	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	12.56976515	59.18869803
	20.48338339		0.29160088	71.76100106	44.28470418	31.27530836		
	0		0	0	0.251517278	0.292575574	0.225051384	0.421654228
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
								3
								5
715	C16	Sc29	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	14.65631006	102.2141214
	75.14665628		0.503571269	69.54418298	50.05735266	29.29169422		
	0		0	0	0.198021052	0.185581091	0.191572754	0.409469615
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
								4
								1
716	C17	Sc29	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	34.12435122	89.95873932
	3.56627786		0.443193522	31.83490119	22.00823429	12.71324059		
	0		0	0	0.154114011	0.183917483	0.218846089	0.390156452
	0.424898731		0.195078226	0.211045796	0.212449365	3	2	1
								4
								2
717	C18	Sc29	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	22.9036356	114.7069548
	14.82699307		0.56511885	55.33673428	37.90321646	23.72145029	1	49.57932244
	41.31610203		82.63220406	413.1610203	0.026128756	0.052257513	0.261287563	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.196227938	0.239913033
	0.294153591		3	2	1	4	3	
								3
718	C19	Sc29	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	10.86892611	90.00070565
	38.18171179		0.443400275	79.24738946	59.23782899	34.26558922		
	0		0	0	0.19335296	0.154863434	0.16721044	0.416396653
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
								4
								4
719	C20	Sc29	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	22.06151067	46.12331125
	19.64406076		0.227232539	45.81810536	29.6528947	22.7158163		
	0		0	0	0.266503103	0.213730709	0.290225506	0.462800059
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
								4
								5
720	C21	Sc29	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	6.320527548	48.98585736	89.96292202
	0.241335248		85.67694678	62.7998377	39.18347533			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
								1
721	C22	Sc29	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	44.80078867	84.62593646
	96.89993412		0.41692077	0.403606039	0.253494939	0.19745033	1	135.1189196
	112.5990997		225.1981993	1125.990997	0.071208906	0.142417812	0.712089062	0.273632139

	0.256849416	0.255171744	0.482159781	0.476288524	0.435601111	0.276684344	0.309353168
	0.573845087	3	2	1	5	2	
722	C23 Sc29	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	27.83832255	32.83555671
	41.4875192	0.161768675	41.36003036	29.99887503	19.14326949	1	189.7500282
	158.1250235	316.2500471	1581.250235	0.1	0.2	1	0.126338191
	0.135993177	0.31838757	0.379056788	0.311830131	0.209193785	0.289528394	0.655915066
	3	2	5	3			
723	C24 Sc29	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	23.27815882	101.091395
	38.46617124	0.49804001	38.78959972	26.57572534	20.01520542		
	0	0	0	0	0	0	0
	0.377206528	0.204296641	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079
	0	0	0	0	0	0	0
724	C25 Sc29	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	15.67428635	108.0009528
	14.23314753	0.532080852	69.99148435	42.54432854	31.21918952	1	42.54432854
	35.45360711	70.90721423	354.5360711	0.02242125	0.0448425	0.224212502	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.249475361	0.229835431
	0.342410683	2	3	1	5	5	
725	C01 Sc30	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	12.87580124	6.870223806
	22.2596509	0.033847058	62.42411959	48.90874503	31.13447776	1	48.90874503
	40.75728752	81.51457505	407.5728752	0.028731427	0.057462854	0.287314272	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169637243	0.166449828
	0.275326199	2	3	1	1	1	
726	C02 Sc30	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	29.42635114	34.9928391	3.448308502
	0.172396809	27.52504448	18.62880505	15.49742005			0
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277
	0.222682445	0.189169138	0.193388639	1	3	2	1
727	C03 Sc30	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	30.94623479	85.51575292
	55.36183542	0.421304567	36.88886179	24.41104586	15.05281111	1	82.53396202
	68.77830169	137.5566034	687.7830169	0.048484551	0.096969101	0.484845506	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.230853108	0.247453132
	0.41942751	3	2	1	1	3	
728	C04 Sc30	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.068782832	3.698785078
	85.97992038	0.01822255	96.81050148	67.5666314	43.02065075		
	0	0	0	0	0	0	0
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
729	C05 Sc30	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	20.46126588	25.26080431
	50.3295197	0.124450664	64.92002577	40.61306943	25.97956223		
	0	0	0	0	0	0	0
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3

730	C06	Sc30	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	12.86420333	7.109863301	
	57.96001621		0.035027674	72.87196588	46.41497204	30.62761708			
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2	2
731	C07	Sc30	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	38.56409432	36.53268887	
	2.665127499		0.179983081	9.58329726	7.562191182	5.28016834			
	0		0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	
	0.339465132		0.168102684	0.166496609	0.169732566	2	3	1	2
732	C08	Sc30	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	9.588584809	78.84076537	
	58.18750434		0.388419366	84.53164379	58.12291616	35.23496524			
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1	2
733	C09	Sc30	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	4.433290049	37.21620286	
	111.3518603		0.183350502	95.68180696	62.04764159	41.4397159	1	170.2273424	
	141.8561187		283.7122374	1418.561187	0.1	0.2	1	0.178780994	0.232017403
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4				
734	C10	Sc30	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	52.4881914	69.4442434	
	100.7044175		0.342126169	0	-8.9659988			0	
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542		0.206429195	0.192206618	2	1	3	2	5
735	C11	Sc30	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	31.66262274	9.30900598	
	86.56844337		0.045862038	32.03086931	19.46342339	11.79387673	1	92.06939166	
	76.72449305		153.4489861	767.2449305	0.054086136	0.108172272	0.540861358	0.316867923	
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.270237984	0.271919496	
	0.47918619		3	2	1	3	1		
736	C12	Sc30	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	4.856473196	102.6475506	
	13.89093305		0.505706614	97.33383872	64.76596549	40.15125624	1	64.76596549	
	53.97163791		107.9432758	539.7163791	0.038046747	0.076093493	0.380467465	0.220522508	
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.225438212	0.24498669	
	0.376826141		3	2	1	3	2		
737	C13	Sc30	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	40.43589509	16.75770835	
	105.7477489		0.082559047	7.239226161	4.749373545	3.46565232			
	0		0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	
	0.373298543		0.193600456	0.194835395	0.186649271	2	1	3	3
738	C14	Sc30	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	9.297212361	22.00870416	
	101.4483754		0.108428766	91.8538333	58.9049712	36.67004788	1	58.9049712	
	49.087476	98.174952	490.87476	0.034603707	0.069207414	0.346037072	0.254748757	0.280125362	

	0.188733628	0.439097823	0.467642276	0.3709205	0.236850765	0.268424845	0.358478786	3
	2	1	3	4				
739	C15 Sc30	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	14.36544588	59.18869803	
	20.48338339	0.29160088	67.64082276	41.74208529	29.47962763			
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982	
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3	5
740	C16 Sc30	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	16.75006864	102.2141214	
	75.14665628	0.503571269	64.57319262	46.47927312	27.19793564			
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715	
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
741	C17 Sc30	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	38.99925854	89.95873932	
	3.56627786	0.443193522	19.62777022	13.56915051	7.83833327			
	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	
	0.424898731	0.195078226	0.211045796	0.212449365	3	2	1	4
742	C18 Sc30	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	26.17558355	114.7069548	
	14.82699307	0.56511885	47.70402582	32.67514862	20.44950234	1	37.42452217	
	31.18710181	62.37420361	311.8710181	0.021985024	0.043970048	0.21985024	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.194156072	0.235769301	
	0.27343493	3	2	1	4	3		
743	C19 Sc30	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	12.42162984	90.00070565	
	38.18171179	0.443400275	75.65638985	56.55353842	32.71288549			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
744	C20 Sc30	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	25.21315506	46.12331125	
	19.64406076	0.227232539	39.46119646	25.53878416	19.56417191			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
745	C21 Sc30	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	7.223460055	48.98585736	89.96292202	
	0.241335248	83.70263236	61.35269667	38.28054283			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
746	C22 Sc30	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	51.20090133	84.62593646	
	96.89993412	0.41692077	0	-6.20266233	1	121.4011203	101.1676003	
	202.3352005	1011.676003	0.071317051	0.142634102	0.713170508	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.276738416	0.309461313	0.57438581	
	3	2	1	5	2			
747	C23 Sc30	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	31.81522577	32.83555671	
	41.4875192	0.161768675	32.76772391	23.76678271	15.16636627	1	169.7614589	

	141.4678824	282.9357649	1414.678824	0.099726317	0.199452634	0.997263169	0.126338191
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.209056943	0.289254711
	0.65454665	3	2	1	5	3	
748	C24 Sc30	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	26.60361007	101.091395
	38.46617124	0.49804001	32.34485333	22.16026833	16.68975417		
	0	0	0	0.195074589	0.194999729	0.172101157	0.408593283
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3
749	C25 Sc30	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	17.91347011	108.0009528
	14.23314753	0.532080852	64.9713734	39.49285375	28.98000576	1	39.49285375
	32.91071146	65.82142292	329.1071146	0.023200065	0.04640013	0.232000648	0.297089204
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.249864768	0.230614245
	0.346304756	2	3	1	5	5	
750	C01 Sc31	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	14.4852764	6.870223806
	22.2596509	0.033847058	59.19714817	46.38044149	29.5250026	1	46.38044149
	38.65036791	77.30073582	386.5036791	0.028144014	0.056288029	0.281440144	0.125908042
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169343536	0.165862415
	0.272389135	2	3	1	1		
751	C02 Sc31	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593	0.67046751	44.92377119	0.012963116	33.10464503	34.9928391	0.878117436
	0.172396809	20.99200849	14.20728072	11.81912616			3.448308502
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0
	0.222682445	0.189169138	0.193388639	1	3	2	0.386777277
752	C03 Sc31	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	34.81451414	85.51575292
	55.36183542	0.421304567	27.4091426	18.1378824	11.18453176	1	74.28365559
	61.90304633	123.8060927	619.0304633	0.045075903	0.090151806	0.450759028	0.25038454
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.229148784	0.244044484
	0.402384271	3	2	1	3		
753	C04 Sc31	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.452380686	3.698785078
	85.97992038	0.01822255	95.94728114	66.9641669	42.63705289		
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3
754	C05 Sc31	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	23.01892412	25.26080431
	50.3295197	0.124450664	58.52872335	36.61475912	23.42190399		
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3
755	C06 Sc31	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	14.47222875	7.109863301
	57.96001621	0.035027674	69.04600798	43.97807155	29.01959166		
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2
						2	1

756	C07	Sc31	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	43.38460611	36.53268887
	2.665127499		0.179983081	0.834258507	0.658314373	0.45965655		
	0		0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219
	0.339465132		0.168102684	0.166496609	0.169732566	2	3	1
								2
757	C08	Sc31	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	10.78715791	78.84076537
	58.18750434		0.388419366	81.65616615	56.14577319	34.03639214		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
								2
758	C09	Sc31	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	4.987451305	37.21620286
	111.3518603		0.183350502	94.40228201	61.21789654	40.88555465	1	164.7968226
	137.3306855		274.6613709	1373.306855	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403
	3		1	2	4			0.716039279
	2							
759	C10	Sc31	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	59.04921532	69.4442434
	100.7044175		0.342126169	0	0	-15.52702272		0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
								5
760	C11	Sc31	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	35.62045058	9.30900598
	86.56844337		0.045862038	21.28184512	12.93182392	7.83604889	1	71.77549057
	59.81290881		119.6258176	598.1290881	0.043553929	0.087107857	0.435539287	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.26497188	0.261387288
	0.426525154		2	3	1	3		
761	C12	Sc31	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	5.463532345	102.6475506
	13.89093305		0.505706614	95.86221858	63.78674901	39.5441971	1	63.78674901
	53.15562418		106.3112484	531.5562418	0.038706298	0.077412596	0.387062979	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.225767988	0.245646242
	0.380123897		3	2	1	3	2	
762	C13	Sc31	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	45.49038198	16.75770835
	105.7477489		0.082559047	0	0	-1.58883457		0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
763	C14	Sc31	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	10.45936391	22.00870416
	101.4483754		0.108428766	88.94279062	57.0381478	35.50789633	1	57.0381478
	47.53178983		95.06357966	475.3178983	0.034611194	0.069222388	0.346111939	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236854508	0.268432332
	0.35851622		3	2	1	3	4	
764	C15	Sc31	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	16.16112662	59.18869803
	20.48338339		0.29160088	63.52064444	39.19946638	27.68394689		

	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
765	0.38826343 C16 Sc31	0.210827114 C16	0.019880134 0.552821979	0.230986491 0.842030892	0.194131715 0.026210987	2 0.028306488	1 0.246211068	3 0.860027949
	0.538831064 75.14665628	0.552821979 0.503571269	0.842030892 59.60220225	43.94800428 42.90119359	0.392667574 25.10417706	0.392667574 25.10417706	18.84382722 0.409469615	102.2141214 0.400700715
766	0.376351488 C17 Sc31	0.204734808 C17	0.124173315 0.800632673	0.279183679 0.232974274	0.585759271 46.83759181	0.969595748 0.426987646	0.561030219 43.87416586	0.561030219 89.95873932
	0.018647289 3.56627786	0.800632673 0.443193522	0.232974274 7.420639264	46.83759181 5.130066733	0.426987646 2.96342595	0.426987646 2.96342595	43.87416586 0.390156452	89.95873932 0.422091592
767	0.424898731 C18 Sc31	0.195078226 C18	0.211045796 0.807105196	0.212449365 0.387860644	0.212449365 0.863541855	3 0.747121643	2 0.556240234	1 0.556240234
	0.136455226 14.82699307	0.05991769 0.56511885	0.121343456 40.07131739	46.62508589 27.4470808	0.247118419 17.1775544	0.247118419 17.1775544	29.44753149 1	114.7069548 27.4470808
768	22.87256733 0.230647918	45.74513466 0.139241534	228.7256733 0.36632712	0.016655103 0.427568554	0.033310206 0.327019619	0.033310206 0.327019619	0.166551032 0.191491112	0.168545737 0.23043938
	0.246785326 C19 Sc31	3 C19	2 0.044551879	1 0.107494129	4 0.225709339	3 0.71298898	3 0.559716982	3 0.559716982
	0.01255598 38.18171179	0.07197428 0.443400275	0.96727633 72.06539025	45.13451533 53.86924785	0.423280743 31.16018176	0.423280743 31.16018176	13.97433357 0.416396653	90.00070565 0.388253269
769	0.385127801 C20 Sc31	0.208198327 C20	0.194126634 0.568100462	0.192563901 0.203293235	0.192563901 0.252325745	1 0.743825854	2 0.195429481	3 0.195429481
	0.581358927 19.64406076	0.970019989 0.227232539	0.846828801 33.10428759	44.77732697 21.42467364	0.039822739 16.41252753	0.039822739 16.41252753	28.36479944 0.462800059	46.12331125 0.417820608
770	0.473734591 C21 Sc31	0.23140003 C21	0.208910304 0.239847759	0.236867296 0.493769714	2 0.619955718	3 0.8289809	1 0.156791395	4 0.018576202
	0.070022144 0.241335248	0.486345111 81.72831794	45.50400288 59.90555564	0.252623045 37.37761032	8.126392562 0.158385453	8.126392562 0.368886507	48.98585736 0.35464928	89.96292202 0.331493863
771	0.184443254 C22 Sc31	0.17732464 C22	0.165746932 0.606329462	1 0.568851437	2 0.317362409	3 0.988616154	5 0.579745219	1 0.579745219
	0.380141173 0.41692077	0.550948219 0	0.745334431 -12.602775	44.998239 1	0.032643252 107.936816	0.032643252 89.94734663	57.601014 179.8946933	84.62593646 96.89993412
772	899.4734663 0.482159781	0.065496904 0.476288524	0.130993807 0.435601111	0.654969036 0.273828342	0.273632139 0.303641166	0.273632139 0.303641166	0.256849416 0.545285074	0.255171744 3
	1 C23 Sc31	5 C23	2 0.669232893	1 0.264919558	5 0.066334834	1 0.370084198	2 0.629717507	2 0.629717507
	0.21017401 41.4875192	0.752755554 0.161768675	0.066536481 24.17541744	46.98159204 17.53469038	0.214061164 11.18946304	0.214061164 11.18946304	35.792129 1	32.83555671 149.7728896
773	124.8107413 0.188706502	249.6214826 0.135993177	1248.107413 0.31838757	0.09088336 0.379056788	0.18176672 0.311830131	0.18176672 0.311830131	0.9088336 0.204635465	0.126338191 0.280411754
	0.610331866 C24 Sc31	3 C24	2 0.260315099	1 0.804754564	5 0.193434283	3 0.639460881	3 0.524670309	3 0.524670309
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	29.92906133	101.091395	

	38.46617124	0.49804001	25.90010692	17.74481131	13.36430291			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
774	C25 Sc31	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	4
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	20.15265387	108.0009528	
	14.23314753	0.532080852	59.95126245	36.44137897	26.7408221	36.44137897	30.36781581	
	60.73563162	303.6781581	0.022112914	0.044225827	0.221129136	0.297089204	0.234608961	
	0.294051043	0.476529471	0.414828361	0.460608863	0.249321192	0.229527094	0.340869	2
	3	1	5	5				
775	C01 Sc32	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	16.09475155	6.870223806	
	22.2596509	0.033847058	55.97017677	43.85213797	27.91552745	1	43.85213797	
	36.54344831	73.08689662	365.4344831	0.027516569	0.055033137	0.275165686	0.125908042	
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.169029813	0.165234969	
	0.269251906	2	3	1	1			
776	C02 Sc32	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	36.78293892	34.9928391	3.448308502	
	0.172396809	14.4589725	9.78575639	8.14083227			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	2
777	C03 Sc32	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	38.68279349	85.51575292	
	55.36183542	0.421304567	17.92942341	11.86471894	7.31625241	1	66.03334916	
	55.02779097	110.0555819	550.2779097	0.041434951	0.082869902	0.414349508	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.227328308	0.240403532	
	0.384179511	3	2	1	3			
778	C04 Sc32	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	3.83597854	3.698785078	
	85.97992038	0.01822255	95.08406081	66.3617024	42.25345504			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
779	C05 Sc32	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	25.57658235	25.26080431	
	50.3295197	0.124450664	52.13742096	32.61644881	20.86424576			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
780	C06 Sc32	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	16.08025417	7.109863301	
	57.96001621	0.035027674	65.22005008	41.54117107	27.41156624			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
781	C07 Sc32	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	48.2051179	36.53268887	
	2.665127499	0.179983081	0	-4.36085524			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2

782	C08	Sc32	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	11.98573101	78.84076537
	58.18750434		0.388419366	78.78068852	54.16863022	32.83781904		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
783	C09	Sc32	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	5.541612561	37.21620286
	111.3518603		0.183350502	93.12275706	60.3881515	40.33139339	1	159.3663027
	132.8052523		265.6105045	1328.052523	0.1	0.2	1	0.178780994
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	2	1	2	4			
784	C10	Sc32	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	65.61023925	69.4442434
	100.7044175		0.342126169	0	-22.08804665			0
	0		0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
785	C11	Sc32	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	39.57827842	9.30900598
	86.56844337		0.045862038	10.53282093	6.400224457	3.87822105	1	57.72715192
	48.10595993		96.21191986	481.0595993	0.036222935	0.07244587	0.362229348	0.316867923
	0.266455347		0.264174875	0.486389832	0.435666719	0.417511021	0.261306383	0.254056294
	0.389870185		2	3	1	3	1	
786	C12	Sc32	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.070591495	102.6475506
	13.89093305		0.505706614	94.39059844	62.80753253	38.93713794	1	62.80753253
	52.33961044		104.6792209	523.3961044	0.039410799	0.078821597	0.394107986	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226120238	0.246350742
	0.383646401		3	2	1	3	2	
787	C13	Sc32	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	50.54486886	16.75770835
	105.7477489		0.082559047	0	-6.64332145			0
	0		0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
788	C14	Sc32	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	11.62151545	22.00870416
	101.4483754		0.108428766	86.03174795	55.17132441	34.34574479	1	55.17132441
	45.97610368		91.95220735	459.7610368	0.034619191	0.069238382	0.346191908	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236858507	0.268440329
	0.358556204		3	2	1	3	4	
789	C15	Sc32	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	17.95680735	59.18869803
	20.48338339		0.29160088	59.40046614	36.65684749	25.88826616		
	0		0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
790	C16	Sc32	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	20.9375858	102.2141214
	75.14665628		0.503571269	54.63121188	39.32311405	23.01041848		

	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3	4
791	C17 Sc32	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	48.74907317	89.95873932	
	3.56627786	0.443193522	0	-1.91148136			0	
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731	
	0.195078226	0.211045796	0.212449365	3	2	1	4	2
792	C18 Sc32	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	32.71947943	114.7069548	
	14.82699307	0.56511885	32.43860895	22.21901297	13.90560646	1	22.21901297	
	18.51584414	37.03168829	185.1584414	0.013942102	0.027884205	0.139421023	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.190134611	0.227726379	
	0.233220321	3	2	1	4	3		
793	C19 Sc32	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	15.52703729	90.00070565	
	38.18171179	0.443400275	68.47439068	51.1849573	29.60747804			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
794	C20 Sc32	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	31.51644382	46.12331125	
	19.64406076	0.227232539	26.74737871	17.31056311	13.26088315			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
795	C21 Sc32	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	9.029325069	48.98585736	89.96292202	
	0.241335248	79.75400352	58.45841461	36.47467781			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
796	C22 Sc32	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	64.00112666	84.62593646	
	96.89993412	0.41692077	0	-19.00288766	1	97.78152866	81.48460722	
	162.9692144	814.8460722	0.061356464	0.122712929	0.613564643	0.273632139	0.256849416	
	0.255171744	0.482159781	0.476288524	0.435601111	0.271758123	0.299500727	0.524582877	
	3	2	1	5	2			
797	C23 Sc32	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	39.76903222	32.83555671	
	41.4875192	0.161768675	15.58311099	11.30259806	7.21255982	1	129.7843202	
	108.1536002	216.3072004	1081.536002	0.081437743	0.162875486	0.814377431	0.126338191	
	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131	0.199912657	0.270966137	
	0.563103781	3	2	1	5	3		
798	C24 Sc32	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	33.25451259	101.091395	
	38.46617124	0.49804001	19.45536051	13.32935429	10.03885165			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
799	C25 Sc32	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	22.39183764	108.0009528	

	14.23314753	0.532080852	54.93115148	33.38990418	24.50163823	1	33.38990418	
	27.82492015	55.64984029	278.2492015	0.020951671	0.041903343	0.209516715	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.248740571	0.228365852	
	0.335062789	2	3	1	5	5		
800	C01 Sc33	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	17.70422671	6.870223806	
	22.2596509	0.033847058	52.74320535	41.32383444	26.30605229	1	41.32383444	
	34.4365287	68.87305739	344.365287	0.026844853	0.053689706	0.268448529	0.125908042	
	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.168693956	0.164563254	
	0.265893328	2	3	1	1	1		
801	C02 Sc33	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	40.46123282	34.9928391	3.448308502	
	0.172396809	7.925936493	5.364232049	4.46253837			0	
	0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	
	0.222682445	0.189169138	0.193388639	1	3	2	1	2
802	C03 Sc33	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	42.55107284	85.51575292	
	55.36183542	0.421304567	8.449704227	5.591555482	3.44797306	1	57.78304274	
	48.15253561	96.30507123	481.5253561	0.037537109	0.075074218	0.375371091	0.25038454	
	0.237553697	0.192031501	0.413221665	0.397937162	0.354009513	0.225379387	0.23650569	
	0.364690302	3	2	1	1	3		
803	C04 Sc33	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	4.219576394	3.698785078	
	85.97992038	0.01822255	94.22084047	65.7592379	41.86985719			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
804	C05 Sc33	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	28.13424059	25.26080431	
	50.3295197	0.124450664	45.74611854	28.6181385	18.30658752			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	1
805	C06 Sc33	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	17.68827958	7.109863301	
	57.96001621	0.035027674	61.3940922	39.1042706	25.80354083			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	2
806	C07 Sc33	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	53.02562969	36.53268887	
	2.665127499	0.179983081	0	-9.18136703			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	2
807	C08 Sc33	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	13.18430411	78.84076537	
	58.18750434	0.388419366	75.90521089	52.19148725	31.63924594			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	2

808	C09	Sc33	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	6.095773817	37.21620286	
	111.3518603		0.183350502	91.84323212	59.55840645	39.77723213	1	153.9357828	
	128.279819		256.5596381	1282.79819	0.1	0.2	1	0.178780994	0.232017403
	0.229727169		0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279	
	3	2	1	2	4				
809	C10	Sc33	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586		0.750812103	0.725997985	43.5221926	0.133413638	72.17126317	69.4442434	
	100.7044175		0.342126169	0	-28.64907057			0	
	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237	
	0.19878542		0.206429195	0.192206618	2	1	3	2	5
810	C11	Sc33	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	43.53610626	9.30900598	
	86.56844337		0.045862038	0	-0.07960679	1	44.46850265	37.05708554	
	74.11417108		370.5708554	0.028887697	0.057775394	0.288876971	0.316867923	0.266455347	
	0.264174875		0.486389832	0.435666719	0.417511021	0.257638765	0.246721057	0.353193996	
	2	3	1	3	1				
811	C12	Sc33	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	6.677650644	102.6475506	
	13.89093305		0.505706614	92.9189783	61.82831605	38.3300788	1	61.82831605	
	51.5235967		103.0471934	515.235967	0.040165006	0.080330012	0.401650058	0.220522508	
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.226497342	0.247104949	
	0.387417437		3	2	1	3	2		
812	C13	Sc33	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	55.59935575	16.75770835	
	105.7477489		0.082559047	0	-11.69780834			0	
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543	
	0.193600456		0.194835395	0.186649271	2	1	3	3	
813	C14	Sc33	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	12.783667	22.00870416	
	101.4483754		0.108428766	83.12070527	53.30450101	33.18359324	1	53.30450101	
	44.42041751		88.84083501	444.2041751	0.034627752	0.069255504	0.346277519	0.254748757	
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236862787	0.26844889	
	0.35859901		3	2	1	3	4		
814	C15	Sc33	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	19.75248809	59.18869803	
	20.48338339		0.29160088	55.28028782	34.11422858	24.09258542			
	0	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3	3
815	C16	Sc33	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	23.03134438	102.2141214	
	75.14665628		0.503571269	49.66022151	35.74503452	20.9166599			
	0	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3	4
816	C17	Sc33	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	53.62398049	89.95873932	
	3.56627786		0.443193522	0	0	-6.78638868		0	

	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
817	C18	Sc33	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	35.99142738	114.7069548
	14.82699307		0.56511885	24.80590049	16.99094513	10.63365851	1	16.99094513
	14.15912094		28.31824188	141.5912094	0.011037684	0.022075368	0.110376839	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.188682402	0.224821961
	0.218698229		3	1	2	4	3	
818	C19	Sc33	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	17.07974102	90.00070565
	38.18171179		0.443400275	64.88339108	48.50066673	28.05477431		
	0		0	0	0.154863434	0.16721044	0.416396653	0.388253269
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3
819	C20	Sc33	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	34.6680882	46.12331125
	19.64406076		0.227232539	20.39046984	13.19645259	10.10923877		
	0		0	0	0.213730709	0.290225506	0.462800059	0.417820608
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1
820	C21	Sc33	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395
	0.070022144		0.486345111	45.50400288	0.252623045	9.932257576	48.98585736	89.96292202
	0.241335248		77.7796891	57.01127357	35.5717453			0
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863
	0.184443254		0.17732464	0.165746932	1	2	3	5
821	C22	Sc33	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	70.40123933	84.62593646
	96.89993412		0.41692077	0	-25.40300033	1	92.75630809	77.29692341
	154.5938468		772.9692341	0.060256496	0.120512991	0.602564955	0.273632139	0.256849416
	0.255171744		0.482159781	0.476288524	0.435601111	0.271208138	0.298400758	0.519083033
	3	2	1	5	2			
822	C23	Sc33	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	43.74593544	32.83555671
	41.4875192		0.161768675	6.990804538	5.070505748	3.2356566	109.7957509	91.49645909
	182.9929182		914.9645909	0.071325685	0.142651369	0.713256846	0.126338191	0.188706502
	0.135993177		0.31838757	0.379056788	0.311830131	0.194856627	0.260854078	0.512543489
	3	2	1	5	3			
823	C24	Sc33	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	36.57996385	101.091395
	38.46617124		0.49804001	13.0106141	8.913897266	6.71340039		
	0		0	0	0.195074589	0.194999729	0.408593283	0.408513079
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3
824	C25	Sc33	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	24.6310214	108.0009528
	14.23314753		0.532080852	49.91104053	30.33842939	22.26245447	1	30.33842939
	25.28202449		50.56404899	252.8202449	0.019708497	0.039416994	0.197084972	0.297089204
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.248118984	0.227122678
	0.328846918		2	3	1	5	5	

825	C01	Sc34	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891
	0.092338595		0.186260211	0.345560727	44.010279	0.217997451	19.31370186	6.870223806
	22.2596509		0.033847058	49.51623395	38.79553091	24.69657714	1	38.79553091
	32.3296091		64.65921819	323.296091	0.026124011	0.052248022	0.261240108	0.125908042
	0.105685808		0.089720661	0.310543058	0.275436802	0.263338126	0.168333535	0.163842412
	0.262289117		2	3	1	1		
826	C02	Sc34	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225
	0.027387593		0.67046751	44.92377119	0.012963116	44.13952671	34.9928391	0.878117436
	0.172396809		0.172396809	0.94270772	0.78424448			3.448308502
	0		0	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276
	0.222682445		0.189169138	0.193388639	1	3	2	0.386777277
827	C03	Sc34	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569
	0.968261576		0.313424178	0.692322616	45.9990459	0.274831239	46.41935219	85.51575292
	55.36183542		0.421304567	0	-0.42030629	1	50.21434428	41.8452869
	83.69057381		418.452869	0.033813175	0.06762635	0.338131749	0.25038454	0.237553697
	0.192031501		0.413221665	0.397937162	0.354009513	0.22351742	0.232781756	0.346070631
	3		1	3				
828	C04	Sc34	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042
	0.878142503		0.098346834	0.421107625	46.08943358	0.217661196	4.603174248	3.698785078
	85.97992038		0.01822255	93.35762014	65.1567734	41.48625933		
	0		0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	1
829	C05	Sc34	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928
	0.834625672		0.018288277	0.750144315	46.44082811	0.210183901	30.69189882	25.26080431
	50.3295197		0.124450664	39.35481615	24.6198282	15.74892929		
	0		0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602
	0.365064068		0.222546725	0.225752801	0.182532034	2	1	3
830	C06	Sc34	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007
	0.447893526		0.908595503	0.293614148	43.49182041	0.165167411	19.296305	7.109863301
	57.96001621		0.035027674	57.5681343	36.66737012	24.19551541		
	0		0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035
	0.410044838		0.212181782	0.203205018	0.205022419	1	3	2
831	C07	Sc34	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116
	0.265546659		0.491573159	0.053362545	43.84426266	0.102324317	57.84614148	36.53268887
	2.665127499		0.179983081	0	-14.00187882			0
	0		0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132
	0.168102684		0.166496609	0.169732566	2	3	1	2
832	C08	Sc34	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429
	0.414055988		0.694400158	0.41417927	44.82355005	0.309635483	14.38287721	78.84076537
	58.18750434		0.388419366	73.02973326	50.21434428	30.44067284		
	0		0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003
	0.396290772		0.189261003	0.182744501	0.198145386	2	3	1
833	C09	Sc34	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756
	0.586555041		0.903401915	0.137474704	45.87300595	0.149827337	6.649935073	37.21620286
	111.3518603		0.183350502	90.56370717	58.7286614	39.22307088	1	148.505263
	123.7543858		247.5087717	1237.543858	0.1	0.2	1	0.232017403

	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.716039279
	3	1	4				
834	C10 Sc34	C10 0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	78.7322871	69.4442434
	100.7044175	0.342126169	0	-35.2100945			0
	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542	0.206429195	0.192206618	2	1	3	2
835	C11 Sc34	C11 0.883306091	0.623672207	0.750942434	0.348898342	0.269927892	
	0.895886218	0.42809119	0.964840047	43.45649947	0.310566916	47.49393411	9.30900598
	86.56844337	0.045862038	0	-4.03743464	1	37.61007784	31.34173153
	62.68346306	313.4173153	0.025325754	0.050651508	0.253257542	0.316867923	0.266455347
	0.264174875	0.486389832	0.435666719	0.417511021	0.255857793	0.243159114	0.335384281
	2	3	1				
836	C12 Sc34	C12 0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698	45.00772944	0.264571047	7.284709793	102.6475506
	13.89093305	0.505706614	91.44735816	60.84909956	37.72301965	1	60.84909956
	50.70758297	101.4151659	507.0758297	0.040974372	0.081948745	0.409743724	0.220522508
	0.224798251	0.197499161	0.412829677	0.413879887	0.373184816	0.226902025	0.247914316
	0.39146427	3	2	1	3	2	
837	C13 Sc34	C13 0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976	43.90154741	0.067289973	60.65384264	16.75770835
	105.7477489	0.082559047	0	-16.75229523			0
	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456	0.194835395	0.186649271	2	1	3	3
838	C14 Sc34	C14 0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575	45.96726024	0.256789061	13.94581854	22.00870416
	101.4483754	0.108428766	80.2096626	51.43767762	32.0214417	1	51.43767762
	42.86473135	85.7294627	428.6473135	0.034636939	0.069273878	0.346369392	0.254748757
	0.280125362	0.188733628	0.439097823	0.467642276	0.3709205	0.236867381	0.268458077
	0.358644946	3	2	1	3	4	
839	C15 Sc34	C15 0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962	43.84507351	0.092219933	21.54816882	59.18869803
	20.48338339	0.29160088	51.16010952	31.57160969	22.29690469		
	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343	0.210827114	0.230986491	0.194131715	2	1	3
840	C16 Sc34	C16 0.019880134	0.026210987	0.028306488	0.246211068	0.860027949	
	0.538831064	0.552821979	0.842030892	43.94800428	0.392667574	25.12510296	102.2141214
	75.14665628	0.503571269	44.68923115	32.16695499	18.82290132		
	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488	0.204734808	0.200350357	0.188175744	1	2	3
841	C17 Sc34	C17 0.124173315	0.279183679	0.585759271	0.969595748	0.561030219	
	0.018647289	0.800632673	0.232974274	46.83759181	0.426987646	58.49888781	89.95873932
	3.56627786	0.443193522	0	-11.661296			0
	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226	0.211045796	0.212449365	3	2	1	4
842	C18 Sc34	C18 0.807105196	0.387860644	0.863541855	0.747121643	0.556240234	
	0.136455226	0.05991769	0.121343456	46.62508589	0.247118419	39.26337532	114.7069548

	14.82699307	0.56511885	17.17319206	11.76287731	7.36171057	1	11.76287731	
	9.802397755	19.60479551	98.02397755	0.007920849	0.015841698	0.079208488	0.168545737	
	0.230647918	0.139241534	0.36632712	0.427568554	0.327019619	0.187123984	0.221705126	
	0.203114054	3	1	2	4	3		
843	C19 Sc34	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598	0.07197428	0.96727633	45.13451533	0.423280743	18.63244475	90.00070565	
	38.18171179	0.443400275	61.29239148	45.81637616	26.50207058			
	0	0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801	0.208198327	0.194126634	0.192563901	1	2	3	4
844	C20 Sc34	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927	0.970019989	0.846828801	44.77732697	0.039822739	37.81973259	46.12331125	
	19.64406076	0.227232539	14.03356094	9.082342047	6.95759438			
	0	0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591	0.23140003	0.208910304	0.236867296	2	3	1	4
845	C21 Sc34	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144	0.486345111	45.50400288	0.252623045	10.83519008	48.98585736	89.96292202	
	0.241335248	75.80537469	55.56413255	34.6688128			0	
	0	0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254	0.17732464	0.165746932	1	2	3	5	1
846	C22 Sc34	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173	0.550948219	0.745334431	44.998239	0.032643252	76.801352	84.62593646	96.89993412
	0.41692077	0	-31.803113	1	87.73108753	73.10923961	146.2184792	
	731.0923961	0.05907608	0.118152159	0.590760797	0.273632139	0.256849416	0.255171744	
	0.482159781	0.476288524	0.435601111	0.27061793	0.297220342	0.513180954	3	2
	1	5	2					
847	C23 Sc34	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401	0.752755554	0.066536481	46.98159204	0.214061164	47.72283866	32.83555671	
	41.4875192	0.161768675	0	-0.74124662	1	90.96876813	75.80730678	
	151.6146136	758.0730678	0.061256259	0.122512517	0.612562587	0.126338191	0.188706502	
	0.135993177	0.31838757	0.379056788	0.311830131	0.189821914	0.250784653	0.462196359	
	3	2	1	5	3			
848	C24 Sc34	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797	0.26329677	0.065961091	43.29336424	0.048265458	39.90541511	101.091395	
	38.46617124	0.49804001	6.565867693	4.498440244	3.38794913			
	0	0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528	0.204296641	0.204256539	0.188603264	1	2	3	5
849	C25 Sc34	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086	0.616778357	0.949016321	46.89347587	0.063579986	26.87020516	108.0009528	
	14.23314753	0.532080852	44.89092959	27.28695461	20.02327071	1	27.28695461	
	22.73912884	45.47825769	227.3912884	0.018374402	0.036748805	0.183744024	0.297089204	
	0.234608961	0.294051043	0.476529471	0.414828361	0.460608863	0.247451937	0.225788583	
	0.322176444	2	3	1	5	5		
850	C01 Sc35	C01	0.417022005	0.720324493	0.000114375	0.302332573	0.146755891	
	0.092338595	0.186260211	0.345560727	44.010279	0.217997451	20.92317702	6.870223806	
	22.2596509	0.033847058	46.28926253	36.26722738	23.08710198	1	36.26722738	
	30.22268948	60.44537896	302.2268948	0.025348448	0.050696897	0.253484484	0.125908042	

	0.105685808	0.089720661	0.310543058	0.275436802	0.263338126	0.167945753	0.163066849	
	0.258411305	2	3	1	1	1		
851	C02 Sc35	C02	0.396767474	0.538816734	0.419194514	0.6852195	0.20445225	0.878117436
	0.027387593	0.67046751	44.92377119	0.012963116	47.8178206	34.9928391	3.448308502	
	0.172396809	0	-2.89404941			0	0	
	0.257404041	0.194814404	0.208494062	0.445364891	0.378338276	0.386777277	0.222682445	
	0.189169138	0.193388639	1	3	2	1	2	
852	C03 Sc35	C03	0.417304802	0.558689828	0.140386939	0.198101489	0.800744569	
	0.968261576	0.313424178	0.692322616	45.9990459	0.274831239	50.28763154	85.51575292	
	55.36183542	0.421304567	0	-4.28858564	1	48.23720131	40.19766776	
	80.39533552	401.9766776	0.033714687	0.067429373	0.337146866	0.25038454	0.237553697	
	0.192031501	0.413221665	0.397937162	0.354009513	0.223468176	0.232683268	0.34557819	
	3	2	1	3				
853	C04 Sc35	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042	
	0.878142503	0.098346834	0.421107625	46.08943358	0.217661196	4.986772102	3.698785078	
	85.97992038	0.01822255	92.4943998	64.5543089	41.10266148			
	0	0	0.214732899	0.18442312	0.126095549	0.407884499	0.379289941	
	0.3266149	0.203942249	0.189644971	0.16330745	1	2	3	
854	C05 Sc35	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928	
	0.834625672	0.018288277	0.750144315	46.44082811	0.210183901	33.24955706	25.26080431	
	50.3295197	0.124450664	32.96351374	20.62151788	13.19127105			
	0	0	0.286047241	0.291180307	0.19489221	0.44509345	0.451505602	
	0.365064068	0.222546725	0.225752801	0.182532034	2	1	3	
855	C06 Sc35	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007	
	0.447893526	0.908595503	0.293614148	43.49182041	0.165167411	20.90433042	7.109863301	
	57.96001621	0.035027674	53.7421764	34.23046963	22.58748999			
	0	0	0.231167154	0.224930393	0.238148451	0.424363564	0.406410035	
	0.410044838	0.212181782	0.203205018	0.205022419	1	3	2	
856	C07 Sc35	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116	
	0.265546659	0.491573159	0.053362545	43.84426266	0.102324317	62.66665327	36.53268887	
	2.665127499	0.179983081	0	-18.82239061			0	
	0	0.108835421	0.116048175	0.133699741	0.336205368	0.332993219	0.339465132	
	0.168102684	0.166496609	0.169732566	2	3	1	2	
857	C08 Sc35	C08	0.574117605	0.146728575	0.589305537	0.69975836	0.102334429	
	0.414055988	0.694400158	0.41417927	44.82355005	0.309635483	15.58145031	78.84076537	
	58.18750434	0.388419366	70.15425563	48.23720131	29.24209974			
	0	0	0.195954796	0.182760584	0.225479264	0.378522006	0.365489003	
	0.396290772	0.189261003	0.182744501	0.198145386	2	3	1	
858	C09 Sc35	C09	0.049953459	0.535896406	0.663794645	0.514889112	0.944594756	
	0.586555041	0.903401915	0.137474704	45.87300595	0.149827337	7.204096329	37.21620286	
	111.3518603	0.183350502	89.28418222	57.89891636	38.66890962	1	143.0747431	
	119.2289526	238.4579052	1192.289526	0.1	0.2	1	0.178780994	
	0.229727169	0.392146196	0.44667726	0.432078559	0.246073098	0.32333863	0.232017403	
	3	2	1	4			0.716039279	
859	C10 Sc35	C10	0.139276347	0.807391289	0.397676837	0.165354197	0.92750858	
	0.34776586	0.750812103	0.725997985	43.5221926	0.133413638	85.29331103	69.4442434	
	100.7044175	0.342126169	0	-41.77111843			0	

	0	0	0.212063257	0.22017735	0.208648434	0.397570841	0.412858391	0.384413237
	0.19878542		0.206429195	0.192206618	2	1	3	2
860	C11	Sc35	C11	0.883306091	0.623672207	0.750942434	0.348898342	0.269927892
	0.895886218		0.42809119	0.964840047	43.45649947	0.310566916	51.45176195	9.30900598
	86.56844337		0.045862038	0	-7.99526248	1	34.23046963	28.52539136
	57.05078272		285.2539136	0.023924886	0.047849773	0.239248863	0.316867923	0.266455347
	0.264174875		0.486389832	0.435666719	0.417511021	0.255157359	0.241758246	0.328379942
	2	3	1	3	1			
861	C12	Sc35	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133
	0.578389614		0.408136803	0.23702698	45.00772944	0.264571047	7.891768944	102.6475506
	13.89093305		0.505706614	89.97573802	59.86988308	37.1159605	1	59.86988308
	49.89156923		99.78313846	498.9156923	0.041845179	0.083690359	0.418451795	0.220522508
	0.224798251		0.197499161	0.412829677	0.413879887	0.373184816	0.227337428	0.248785123
	0.395818305		3	2	1	3	2	
862	C13	Sc35	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902
	0.527058102		0.885942099	0.35726976	43.90154741	0.067289973	65.70832952	16.75770835
	105.7477489		0.082559047	0	-21.80678211			0
	0	0	0.221712208	0.223609096	0.217157743	0.387200912	0.389670791	0.373298543
	0.193600456		0.194835395	0.186649271	2	1	3	3
863	C14	Sc35	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918
	0.99732285		0.172340508	0.13713575	45.96726024	0.256789061	15.10797009	22.00870416
	101.4483754		0.108428766	77.29861992	49.57085422	30.85929015	1	49.57085422
	41.30904518		82.61809036	413.0904518	0.034646824	0.069293648	0.346468238	0.254748757
	0.280125362		0.188733628	0.439097823	0.467642276	0.3709205	0.236872323	0.268467962
	0.358694369		3	2	1	3	4	
864	C15	Sc35	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188
	0.923024536		0.711524759	0.124270962	43.84507351	0.092219933	23.34384956	59.18869803
	20.48338339		0.29160088	47.0399312	29.02899078	20.50122395		
	0	0	0	0.251517278	0.292575574	0.225051384	0.421654228	0.461972982
	0.38826343		0.210827114	0.230986491	0.194131715	2	1	3
865	C16	Sc35	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949
	0.538831064		0.552821979	0.842030892	43.94800428	0.392667574	27.21886154	102.2141214
	75.14665628		0.503571269	39.71824078	28.58887545	16.72914274		
	0	0	0	0.198021052	0.185581091	0.191572754	0.409469615	0.400700715
	0.376351488		0.204734808	0.200350357	0.188175744	1	2	3
866	C17	Sc35	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219
	0.018647289		0.800632673	0.232974274	46.83759181	0.426987646	63.37379512	89.95873932
	3.56627786		0.443193522	0	-16.53620331			0
	0	0	0.154114011	0.183917483	0.218846089	0.390156452	0.422091592	0.424898731
	0.195078226		0.211045796	0.212449365	3	2	1	4
867	C18	Sc35	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234
	0.136455226		0.05991769	0.121343456	46.62508589	0.247118419	42.53532326	114.7069548
	14.82699307		0.56511885	9.54048362	6.534809481	4.08976263	1	6.534809481
	5.445674567		10.89134913	54.45674567	0.00456741	0.009134819	0.045674095	0.168545737
	0.230647918		0.139241534	0.36632712	0.427568554	0.327019619	0.185447265	0.218351687
	0.186346857		3	1	2	4	3	

868	C19	Sc35	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982	
	0.01255598		0.07197428	0.96727633	45.13451533	0.423280743	20.18514848	90.00070565	
	38.18171179		0.443400275	57.70139188	43.13208559	24.94936685			
	0		0	0.19335296	0.154863434	0.16721044	0.416396653	0.388253269	
	0.385127801		0.208198327	0.194126634	0.192563901	1	2	3	4
869	C20	Sc35	C20	0.568100462	0.203293235	0.252325745	0.743825854	0.195429481	
	0.581358927		0.970019989	0.846828801	44.77732697	0.039822739	40.97137697	46.12331125	
	19.64406076		0.227232539	7.676652064	4.968231522	3.80595			
	0		0	0.266503103	0.213730709	0.290225506	0.462800059	0.417820608	
	0.473734591		0.23140003	0.208910304	0.236867296	2	3	1	4
870	C21	Sc35	C21	0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202
	0.070022144		0.486345111	45.50400288	0.252623045	11.73812259	48.98585736	89.96292202	
	0.241335248		73.83106026	54.11699151	33.76588029			0	
	0		0.167087112	0.139838178	0.158385453	0.368886507	0.35464928	0.331493863	
	0.184443254		0.17732464	0.165746932	1	2	3	5	1
871	C22	Sc35	C22	0.606329462	0.568851437	0.317362409	0.988616154	0.579745219	
	0.380141173		0.550948219	0.745334431	44.998239	0.032643252	83.20146466	84.62593646	
	96.89993412		0.41692077	0	-38.20322566	1	82.70586696	68.9215558	
	137.8431116		689.215558	0.057806057	0.115612113	0.578060566	0.273632139	0.256849416	
	0.255171744		0.482159781	0.476288524	0.435601111	0.269982919	0.295950319	0.506830839	
	3	2	1	5	2				
872	C23	Sc35	C23	0.669232893	0.264919558	0.066334834	0.370084198	0.629717507	
	0.21017401		0.752755554	0.066536481	46.98159204	0.214061164	51.69974189	32.83555671	
	41.4875192		0.161768675	0	-4.71814985	1	77.21229111	64.34357592	
	128.6871518		643.4357592	0.053966402	0.107932804	0.53966402	0.126338191	0.188706502	
	0.135993177		0.31838757	0.379056788	0.311830131	0.186176986	0.243494796	0.425747076	
	3	2	1	5	3				
873	C24	Sc35	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309	
	0.92480797		0.26329677	0.065961091	43.29336424	0.048265458	43.23086637	101.091395	
	38.46617124		0.49804001	0.121121283	0.082983222	0.06249787			
	0		0	0.195074589	0.194999729	0.172101157	0.408593283	0.408513079	
	0.377206528		0.204296641	0.204256539	0.188603264	1	2	3	5
									4
874	C25	Sc35	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573	
	0.234362086		0.616778357	0.949016321	46.89347587	0.063579986	29.10938893	108.0009528	
	14.23314753		0.532080852	39.87081862	24.23547982	17.78408694	1	24.23547982	
	20.19623318		40.39246636	201.9623318	0.016939034	0.033878069	0.169390343	0.297089204	
	0.234608961		0.294051043	0.476529471	0.414828361	0.460608863	0.246734253	0.224353215	
	0.314999603		2	3	1	5	5		

	0.147223623	0.165895397	0.338774094	3	2	1	0.109223903	0.132746573			
	0.336597605	3	2	1	0.071224183	0.099597749	0.334421116	3	2	1	
	0.033224463	0.066448926	0.332244628	3	2	1	3				
3	C04	sc01	C04	0.876389152	0.894606664	0.085044211	0.039054783	0.16983042			
	0.878142503	0.098346834	0.421107625	35.08943358	0.217661196	3.83597854	3.698785078				
	85.97992038	0.435322393	0.789220736	0.05560195	0.03161625	0.734933929	49.08551219				
	31.25345504	0	0	0	0	0.214732899	0.18442312				
	0.126095549	0.407884499	0.379289941	0.3266149	0.367096049	0.341360947	0.29395341	1			
	2	3	0.326307599	0.303431953	0.26129192	1	2	3	0.285519149		
	0.265502959	0.22863043	1	2	3	0.244730699	0.227573965	0.19596894	1		
	2	3	0.203942249	0.189644971	0.16330745	1	2	3	0.1631538	0.151715977	
	0.13064596	1	2	3	0.12236535	0.113786982	0.09798447	1	2	3	
	0.0815769	0.075857988	0.06532298	1	2	3	0.04078845	0.037928994	0.03266149		
	1	2	3	0	0	1	2	3	1	4	
4	C05	sc01	C05	0.95788953	0.533165285	0.691877114	0.315515631	0.686500928			
	0.834625672	0.018288277	0.750144315	35.44082811	0.210183901	25.57658235	25.26080431				
	50.3295197	0.420367802	0.870562062	0.370728835	0.215922765	0.430203605	15.42047916				
	9.86424576	0	0	0	0	0.286047241	0.291180307				
	0.19489221	0.44509345	0.451505602	0.365064068	0.400584105	0.406355042	0.328557661				
	2	1	3	0.35607476	0.361204481	0.292051254	2	1	3	0.311565415	
	0.316053921	0.255544848	2	1	3	0.26705607	0.270903361	0.219038441	2		
	1	3	0.222546725	0.225752801	0.182532034	2	1	3	0.17803738		
	0.180602241	0.146025627	2	1	3	0.133528035	0.135451681	0.10951922	2		
	1	3	0.08901869	0.09030112	0.073012814	2	1	3	0.044509345		
	0.04515056	0.036506407	2	1	3	0	0	1	2	3	1
	5										
5	C06	sc01	C06	0.988861089	0.748165654	0.280443992	0.789279328	0.103226007			
	0.447893526	0.908595503	0.293614148	32.49182041	0.165167411	16.08025417	7.109863301				
	57.96001621	0.330334821	0.187921392	0.233080942	0.060773257	0.495427098	24.87109546				
	16.41156624	0	0	0	0	0.231167154	0.224930393				
	0.238148451	0.424363564	0.406410035	0.410044838	0.381927208	0.365769032	0.369040354				
	1	3	2	0.339490851	0.325128028	0.32803587	1	3	2	0.297054495	
	0.284487025	0.287031387	1	3	2	0.254618139	0.243846021	0.246026903	1		
	3	2	0.212181782	0.203205018	0.205022419	1	3	2	0.169745426		
	0.162564014	0.164017935	1	3	2	0.127309069	0.121923011	0.123013451	1		
	3	2	0.084872713	0.081282007	0.082008968	1	3	2	0.042436356		
	0.040641004	0.041004484	1	3	2	0	0	1	2	3	2
	1										
6	C07	sc01	C07	0.287775339	0.130028572	0.019366958	0.678835533	0.211628116			
	0.265546659	0.491573159	0.053362545	32.84426266	0.102324317	48.2051179	36.53268887				
	2.665127499	0.204648634	0.269505246	0.698726162	0.312271894	0.022780815	0				
15.36085524	0	0	0	0	0	0.108835421	0.116048175				
	0.133699741	0.336205368	0.332993219	0.339465132	0.302584831	0.299693897	0.305518619				
	2	3	1	0.268964294	0.266394575	0.271572106	2	3	1	0.235343757	
	0.233095253	0.237625592	2	3	1	0.201723221	0.199795931	0.203679079	2		
	3	1	0.168102684	0.166496609	0.169732566	2	3	1	0.134482147		
	0.133197288	0.135786053	2	3	1	0.10086161	0.099897966	0.10183954	2		

	3	1	0.067241074	0.066598644	0.067893026	2	3	1	0.033620537		
	0.033299322		0.033946513	2	3	1	0	0	1	2	3
	2										2
7	C08	sc01	C08	0.574117605	0.146728575	0.589305537	0.69975836		0.102334429		
	0.414055988		0.694400158	0.41417927	33.82355005	0.309635483	11.98573101		78.84076537		
	58.18750434		0.619270966	0.496192141	0.173731425	0.673910295	0.497371607		36.02324329		
	21.83781904		0	0	0	0	0.195954796		0.182760584		
	0.225479264		0.378522006	0.365489003	0.396290772	0.340669805	0.328940102		0.356661695		
	2	3	1	0.302817605	0.292391202	0.317032617	2	3	1		0.264965404
	0.255842302		0.27740354	2	3	1	0.227113203	0.219293402	0.237774463		2
	3	1	0.189261003	0.182744501	0.198145386	2	3	1	0.151408802		
	0.146195601		0.158516309	2	3	1	0.113556602	0.109646701	0.118887232		2
	3	1	0.075704401	0.073097801	0.079258154	2	3	1	0.037852201		
	0.0365489	0.039629077	2	3	1	0	0	1	2	3	2
8	C09	sc01	C09	0.049953459	0.535896406	0.663794645	0.514889112		0.944594756		
	0.586555041		0.903401915	0.137474704	34.87300595	0.149827337	5.541612561		37.21620286		
	111.3518603		0.299654674	0.739121747	0.080324867	0.318114393	0.951806652		43.91786345		
	29.33139339		1	108.4238548	90.35321233	180.7064247	903.5321233	0.1	0.2		1
	0.178780994		0.232017403	0.229727169	0.392146196	0.44667726	0.432078559		0.362931577		
	0.422009534		0.488870703	3	2	1	0.333716957	0.397341808	0.545662847		3
	2	1	0.304502338	0.372674082	0.602454991	3	2	1	0.275287718		
	0.348006356		0.659247135	3	2	1	0.246073098	0.32333863	0.716039279		3
	2	1	0.216858479	0.298670904	0.772831424	3	2	1	0.187643859		
	0.274003178		0.829623568	3	2	1	0.158429239	0.249335452	0.886415712		3
	2	1	0.12921462	0.224667726	0.943207856	3	2	1	0.1	0.2	1
	3	2	1	2	4						
9	C10	sc01	C10	0.139276347	0.807391289	0.397676837	0.165354197		0.92750858		
	0.34776586		0.750812103	0.725997985	32.5221926	0.133413638	65.61023925		69.4442434		
	100.7044175		0.266827275	0.194951992	0.95101086	0.593591276	0.860795089		0		-
33.08804665			0	0	0	0	0.212063257		0.22017735		
	0.208648434		0.397570841	0.412858391	0.384413237	0.357813757	0.371572552		0.345971913		
	2	1	3	0.318056672	0.330286713	0.307530589	2	1	3		0.278299588
	0.289000874		0.269089266	2	1	3	0.238542504	0.247715034	0.230647942		2
	1	3	0.19878542	0.206429195	0.192206618	2	1	3	0.159028336		
	0.165143356		0.153765295	2	1	3	0.119271252	0.123857517	0.115323971		2
	1	3	0.079514168	0.082571678	0.076882647	2	1	3	0.039757084		
	0.041285839		0.038441324	2	1	3	0	0	1	2	3
	5										
10	C11	sc01	C11	0.883306091	0.623672207	0.750942434	0.348898342		0.269927892		
	0.895886218		0.42809119	0.964840047	32.45649947	0.310566916	39.57827842		9.30900598		
	86.56844337		0.621133833	0.179745247	0.57368138	0.079570955	0.73996447		0		-
7.12177895	1		24.87109546	20.72591288	41.45182577	207.2591288	0.022938767		0.045877534		
	0.22938767		0.316867923	0.266455347	0.264174875	0.486389832	0.435666719		0.417511021		
	0.440044726		0.396687801	0.398698686	1	3	2	0.393699619	0.357708882		
	0.379886351		1	3	2	0.347354513	0.318729964	0.361074016	2	3	1
	0.301009406		0.279751045	0.342261681	2	3	1	0.2546643	0.240772127		0.323449346
	2	3	1	0.208319193	0.201793208	0.304637011	2	3	1		0.161974087

	0.16281429	0.285824676	3	2	1	0.11562898	0.123835371	0.26701234	3
	2	0.069283874	0.084856453			0.248200005	3	2	1
	0.045877534	0.22938767	3	2	1	3	1		0.022938767
11	C12	sc01	C12	0.663441498	0.62169572	0.114745973	0.949489259	0.449912133	
	0.578389614	0.408136803	0.23702698		34.00772944	0.264571047	6.070591495	102.6475506	
	13.89093305	0.529142094	0.538826259		0.087992339	0.877404484	0.118736072	45.06398757	
	27.93713794	1	45.06398757	37.55332297	75.10664594	375.5332297	0.041562798		
	0.083125596	0.415627978	0.220522508		0.224798251	0.197499161	0.412829677	0.413879887	
	0.373184816	0.375702989	0.380804458		0.377429132	3	1	2	0.338576301
	0.347729029	0.381673448	3	2	1	0.301449614	0.3146536	0.385917765	3
	1	0.264322926	0.281578171	0.390162081	3	2	1	0.227196238	0.248502742
	0.394406397	3	2	1	0.19006955	0.215427312	0.398650713	3	2
	0.152942862	0.182351883	0.40289503	3	2	1	0.115816174	0.149276454	1
	0.407139346	3	2	1	0.078689486	0.116201025	0.411383662	3	2
	0.041562798	0.083125596	0.415627978	3	2	1	3	2	1
12	C13	sc01	C13	0.903379521	0.573679487	0.002870327	0.617144914	0.326644902	
	0.527058102	0.885942099	0.35726976		32.90154741	0.067289973	50.54486886	16.75770835	
	105.7477489	0.134579945	0.282765605		0.732640511	0.143240519	0.90390417	0	-
17.64332145		0	0	0	0	0	0.221712208	0.223609096	
	0.217157743	0.387200912	0.389670791		0.373298543	0.348480821	0.350703712	0.335968689	
	2	3	0.309760729	0.311736633	0.298638834	2	1	3	0.271040638
	0.272769554	0.26130898	2	1	3	0.232320547	0.233802474	0.223979126	2
	1	3	0.193600456	0.194835395	0.186649271	2	1	3	0.154880365
	0.155868316	0.149319417	2	1	3	0.116160274	0.116901237	0.111989563	2
	1	3	0.077440182	0.077934158	0.074659709	2	1	3	0.038720091
	0.038967079	0.037329854	2	1	3	0	0	1	2
	3							3	3
13	C14	sc01	C14	0.908535151	0.623360116	0.015821243	0.929437234	0.690896918	
	0.99732285	0.172340508	0.13713575		34.96726024	0.256789061	11.62151545	22.00870416	
	101.4483754	0.513578121	0.760939869		0.168452174	0.188124662	0.867154247	37.50146247	
	23.34574479	1	37.50146247	31.25121873	62.50243746	312.5121873	0.034587834		
	0.069175667	0.345878336	0.254748757		0.280125362	0.188733628	0.439097823	0.467642276	
	0.3709205	0.398646824	0.427795615	0.368416284	2	1	3	0.358195825	0.387948954
	0.365912067	3	1	2	0.317744826	0.348102294	0.363407851	3	2
	0.277293827	0.308255633	0.360903634	3	2	1	0.236842828	0.268408972	1
	0.358399418	3	2	1	0.196391829	0.228562311	0.355895202	3	2
	0.15594083	0.18871565	0.353390985	3	2	1	0.115489831	0.148868989	1
	0.350886769	3	2	1	0.075038832	0.109022328	0.348382552	3	2
	0.034587834	0.069175667	0.345878336	3	2	1	3	4	1
14	C15	sc01	C15	0.932595463	0.696818161	0.066000173	0.755463053	0.753876188	
	0.923024536	0.711524759	0.124270962		32.84507351	0.092219933	17.95680735	59.18869803	
	20.48338339	0.184439866	0.269692942		0.260281307	0.50592955	0.175086618	21.08124579	
	14.88826616		0	0	0	0	0.251517278	0.292575574	
	0.225051384	0.421654228	0.461972982		0.38826343	0.379488805	0.415775684	0.349437087	
	2	1	3	0.337323382	0.369578386	0.310610744	2	1	3
	0.323381088	0.271784401	2	1	3	0.252992537	0.277183789	0.232958058	2
	1	3	0.210827114	0.230986491	0.194131715	2	1	3	0.168661691

	0.184789193		0.155305372	2	1	3	0.126496268	0.138591895	0.116479029	2
	1 3		0.084330846	0.092394596		0.077652686	2	1 3	0.042165423	
	0.046197298		0.038826343	2	1	3	0	0	1	2 3 3
	5									
15	C16 sc01	C16	0.019880134	0.026210987	0.028306488	0.246211068	0.860027949			
	0.538831064		0.552821979	0.842030892	32.94800428	0.392667574	20.9375858	102.2141214		
	75.14665628		0.785335148	0.293519509	0.303487256	0.873699645	0.642334014	20.52492249		
	12.01041848		0	0	0	0	0.198021052	0.185581091		
	0.191572754		0.409469615	0.400700715	0.376351488	0.368522654	0.360630643	0.338716339		
	1 2 3		0.327575692	0.320560572	0.30108119	1	2 3	0.286628731		
	0.2804905	0.263446041	1	2 3	0.245681769	0.240420429	0.225810893	1 2		
	3	0.204734808	0.200350357	0.188175744	1	2 3	0.163787846	0.160280286		
	0.150540595		1 2 3	0.122840885	0.120210214	0.112905446	1	2 3		
	0.081893923		0.080140143	0.075270298	1	2 3	0.040946962	0.040070071		
	0.037635149		1 2 3	0	0	1 2 3	4	1		
16	C17 sc01	C17	0.124173315	0.279183679	0.585759271	0.969595748	0.561030219			
	0.018647289		0.800632673	0.232974274	35.83759181	0.426987646	48.74907317	89.95873932		
	3.56627786		0.853975293	0.962405512	0.706610714	0.768943836	0.030483613	0	-	
12.91148136			0	0	0	0	0.154114011	0.183917483		
	0.218846089		0.390156452	0.422091592	0.424898731	0.351140806	0.379882433	0.382408858		
	3 2		1	0.312125161	0.337673273	0.339918985	3 2	1	0.273109516	
	0.295464114		0.297429112	3 2	1	0.234093871	0.253254955	0.254939239	3	
	2 1		0.195078226	0.211045796	0.212449365	3 2	1	0.156062581		
	0.168836637		0.169959492	3 2	1	0.117046935	0.126627478	0.127469619	3	
	2 1		0.07803129	0.084418318	0.084979746	3 2	1	0.039015645		
	0.042209159		0.042489873	3 2	1	0	0	1 2 3	4	
	2									
17	C18 sc01	C18	0.807105196	0.387860644	0.863541855	0.747121643	0.556240234			
	0.136455226		0.05991769	0.121343456	35.62508589	0.247118419	32.71947943	114.7069548		
	14.82699307		0.494236837	0.913214326	0.474264088	0.980485125	0.126737269	4.64271068		
	2.90560646		1	4.64271068	3.868925567	7.737851134	38.68925567	0.004282001		
	0.008564002		0.042820011	0.168545737	0.230647918	0.139241534	0.36632712	0.427568554		
	0.327019619		0.330122608	0.385668099	0.298599659	2 1 3	0.293918096			
	0.343767644		0.270179698	2 1	3	0.257713584	0.301867188	0.241759737	2	
	1 3		0.221509072	0.259966733	0.213339776	2 1 3	0.185304561			
	0.218066278		0.184919815	2 1	3	0.149100049	0.176165823	0.156499855	3	
	1 2		0.112895537	0.134265368	0.128079894	3 1	2	0.076691025		
	0.092364913		0.099659933	3 2	1	0.040486513	0.050464457	0.071239972	3	
	2 1		0.004282001	0.008564002	0.042820011	3 2	1	4 3		
18	C19 sc01	C19	0.044551879	0.107494129	0.225709339	0.71298898	0.559716982			
	0.01255598		0.07197428	0.96727633	34.13451533	0.423280743	15.52703729	90.00070565		
	38.18171179		0.846561485	0.568174845	0.225062144	0.769302553	0.326367312	32.16832476		
	18.60747804		0	0	0	0	0.19335296	0.154863434		
	0.16721044		0.416396653	0.388253269	0.385127801	0.374756988	0.349427942	0.346615021		
	1 2		3	0.333117323	0.310602615	0.308102241	1 2	3	0.291477657	
	0.271777288		0.269589461	1 2	3	0.249837992	0.232951961	0.231076681	1	
	2 3		0.208198327	0.194126634	0.192563901	1 2	3	0.166558661		

	0.155301307	0.15405112	1	2	3	0.124918996	0.116475981	0.11553834	1
	2	0.083279331	0.077650654	0.07702556	1	2	3	0.041639665	
	0.038825327	0.03851278	1	2	3	0	0	1	2
	4							1	2
19	C20 sc01	C20 0.568100462	0.203293235	0.252325745	0.743825854	0.195429481			
	0.581358927	0.970019989	0.846828801	33.77732697	0.039822739	31.51644382	46.12331125		
	19.64406076	0.079645477	0.485492354	0.456826262	0.394250032	0.167912307	2.951323831		
	2.26088315	0	0	0	0	0.266503103	0.213730709		
	0.290225506	0.462800059	0.417820608	0.473734591	0.416520053	0.376038547	0.426361132		
	2	3	1	0.370240047	0.334256486	0.378987673	2	3	1
	0.292474425	0.331614214	2	3	1	0.277680035	0.250692365	0.284240755	2
	3	1	0.23140003	0.208910304	0.236867296	2	3	1	0.185120024
	0.167128243	0.189493836	2	3	1	0.138840018	0.125346182	0.142120377	2
	3	1	0.092560012	0.083564122	0.094746918	2	3	1	0.046280006
	0.041782061	0.047373459	2	3	1	0	0	1	2
	5							1	2
20	C21 sc01	C21 0.239847759	0.493769714	0.619955718	0.8289809	0.156791395	0.018576202		
	0.070022144	0.486345111	34.50400288	0.252623045	9.029325069	48.98585736	89.96292202		
	0.50524609	0.653704371	0.130878752	0.418718329	0.768979588	40.82857935	25.47467781		
		0	0	0	0	0.167087112	0.139838178	0.158385453	
	0.368886507	0.35464928	0.331493863	0.331997857	0.319184352	0.298344477	1	2	
	3	0.295109206	0.283719424	0.265195091	1	2	3	0.258220555	0.248254496
	0.232045704	1	2	3	0.221331904	0.212789568	0.198896318	1	2
	0.184443254	0.17732464	0.165746932	1	2	3	0.147554603	0.141859712	
	0.132597545	1	2	3	0.110665952	0.106394784	0.099448159	1	2
	0.073777301	0.070929856	0.066298773	1	2	3	0.036888651	0.035464928	3
	0.033149386	1	2	3	0	0	1	2	3
21	C22 sc01	C22 0.606329462	0.568851437	0.317362409	0.988616154	0.579745219			
	0.380141173	0.550948219	0.745334431	33.998239	0.032643252	64.00112666	84.62593646		
	96.89993412	0.065286504	0.536629399	0.927687008	0.723360428	0.828275358	0		-
30.00288766	1	61.35350184	51.1279182	102.2558364	511.279182	0.056586719	0.113173438		
	0.565867188	0.273632139	0.256849416	0.255171744	0.482159781	0.476288524	0.435601111		
	0.439602475	0.439977016	0.448627719	3	2	1	0.397045168	0.403665507	
	0.461654327	3	2	1	0.354487862	0.367353998	0.474680934	3	2
	0.311930556	0.33104249	0.487707542	3	2	1	0.26937325	0.294730981	1
	0.50073415	3	2	1	0.226815944	0.258419472	0.513760757	3	2
	0.184258637	0.222107964	0.526787365	3	2	1	0.141701331	0.185796455	
	0.539813973	3	2	1	0.099144025	0.149484946	0.55284058	3	2
	0.056586719	0.113173438	0.565867188	3	2	1	5	2	1
22	C23 sc01	C23 0.669232893	0.264919558	0.066334834	0.370084198	0.629717507			
	0.21017401	0.752755554	0.066536481	35.98159204	0.214061164	39.76903222	32.83555671		
	41.4875192	0.428122328	0.995738897	0.576446329	0.280669773	0.354624491	0		-
3.78744018	1	56.20089438	46.83407865	93.6681573	468.3407865	0.051834437	0.103668873		
	0.518344367	0.126338191	0.188706502	0.135993177	0.31838757	0.379056788	0.311830131		
	0.291732257	0.351517996	0.332481555	3	1	2	0.265076943	0.323979205	
	0.353132978	3	2	1	0.23842163	0.296440413	0.373784402	3	2
	0.211766317	0.268901622	0.394435826	3	2	1	0.185111003	0.24136283	1

	0.415087249	3	2	1	0.15845569	0.213824039	0.435738673	3	2	1
	0.131800377	0.186285248			0.456390096	3	2	1	0.105145063	0.158746456
	0.47704152	3	2	1	0.07848975	0.131207665	0.497692943	3	2	1
	0.051834437	0.103668873			0.518344367	3	2	1	5	3
23	C24	sc01	C24	0.260315099	0.804754564	0.193434283	0.639460881	0.524670309		
	0.92480797	0.26329677	0.065961091	32.29336424	0.048265458	33.25451259	101.091395			
	38.46617124	0.096530916	0.141982464	0.482019316	0.864102872	0.328798797	0	-		
0.96114835		0	0	0	0	0.195074589	0.194999729			
	0.172101157	0.408593283	0.408513079	0.377206528	0.367733954	0.367661771	0.339485876			
	1	2	3	0.326874626	0.326810463	0.301765223	1	2	3	0.286015298
	0.285959155	0.26404457	1	2	3	0.24515597	0.245107847	0.226323917	1	
	2	3	0.204296641	0.204256539	0.188603264	1	2	3	0.163437313	
	0.163405231	0.150882611	1	2	3	0.122577985	0.122553924	0.113161959	1	
	2	3	0.081718657	0.081702616	0.075441306	1	2	3	0.040859328	
	0.040851308	0.037720653	1	2	3	0	0	0	1	2
	4								2	3
										5
24	C25	sc01	C25	0.735065963	0.77217803	0.907815853	0.931972069	0.013951573		
	0.234362086	0.616778357	0.949016321	35.89347587	0.063579986	22.39183764	108.0009528			
	14.23314753	0.127159972	0.975341637	0.324566425	0.92316397	0.121661232	18.39952098			
	13.50163823	1	18.39952098	15.33293415	30.6658683	153.3293415	0.016969993			
	0.033939987	0.169699934	0.297089204	0.234608961	0.294051043	0.476529471	0.414828361			
	0.460608863	0.430573523	0.376739524	0.43151797	2	3	1	0.384617575		
	0.338650686	0.402427077	2	3	1	0.338661628	0.300561849	0.373336185	2	
	3	1	0.29270568	0.262473011	0.344245292	2	3	1	0.246749732	
	0.224384174	0.315154399	2	3	1	0.200793784	0.186295337	0.286063506	2	
	3	1	0.154837837	0.148206499	0.256972613	2	3	1	0.108881889	
	0.110117662	0.22788172	3	2	1	0.062925941	0.072028824	0.198790827	3	
	2	1	0.016969993	0.033939987	0.169699934	3	2	1	5	5

3. *The three selected LID data*

	sc_id	lid_id	lid_bnf1	lid_bnf2	lid_bnf3	lid_bnf4	lid_bnf5	lid_bnf6	lid_bnf7	lid_bnf8	cost
lid01	sc01	lid01	0.417022	0.302333	0.18626	0.538817	0.204452	0.670468	0.140387	0.968262	1.2
lid02	sc01	lid02	0.720324	0.146756	0.345561	0.419195	0.878117	0.417305	0.198101	0.313424	0.6
lid03	sc01	lid03	0.000114	0.092339	0.396767	0.68522	0.027388	0.55869	0.800745	0.692323	0.12

APPENDIX F: IT DESIGN PARAMETERS USED IN CHAPTER 4

Table F 1. Design parameters for IT (used in PCSWMM)

Parameters					
SURFACE	Berm height (mm)	Vegetative Cover (fraction)	Surface roughness (Manning's n)	Surface slope (percent)	
	150	0	0.013	5	
STORAGE	Storage Height (mm)	Storage Void Ratio (voids / solids)	Seepage Rate (mm/hr)	Storage Clogging Factor	
	750	0.4	210	0	
DRAIN	Drain coefficient (mm/hr)	Drain exponent	Drain offset height (mm)	Open level (mm)	Closed level (mm)
	0	0.5	0	0	0